

RULES

AND
REGULATIONS

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LLOYD'S REGISTER

OF

BRITISH AND FOREIGN SHIPPING.

RULES AND REGULATIONS.

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GREENOCK AND PORT GLASGOW, with Campbeltown and Rothesay Ship Surveyors (Office, Commercial Bank Buildings, 14, Cross- shore Street, Greenock) Ship and Engineer Surveyors (GRIMSBY AND BOSTON Ship and Engineer Surveyors Ship and Engineer Surveyors (C. Martell W. H. Roberts Ship and Engineer Surveyors (Address, Point House, Llanstadwell, Neyland) N. G. Turnbull W. Morrison J. Kerr Ship and Engineer Surveyors A. L. Whittell D. M. Chapman G. F. Silley MILFORD HAVEN, with Pembroke and Tenby, and a district extending as far as New Quay inclusive Quay inclusive Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) † Not an exclusive Officer of Lloyd's Register.					J. R. Dippie
GREENOCK AND PORT GLASGOW, with Campbeltown and Rothesay Ship Surveyors (Office, Commercial Bank Buildings, 14, Cross- shore Street, Greenock) Ship and Engineer Surveyors GRIMSBY AND BOSTON Ship and Engineer Surveyors Ship and Engineer Surveyors Ship and Engineer Surveyors C. Martell W. H. Roberts R. Cheetham (Office, Bank Chambers, 2, Freeman Street, Great W. Morrison J. Kerr A. L. Whittell D. M. Chapman G. F. Silley MILFORD HAVEN, with Pembroke and Tenby, and a district extending as far as New Quay inclusive Quay inclusive (Address, Point House, Llanstadwell, Neyland) † J. W. Johnstone Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) † Not an exclusive Officer of Lloyd's Register.			A. Fletcher	Middlesbrough)	
Campbeltown and Rothesay Ship Surveyors Ship Surveyors (Office, Commercial Bank Buildings, 14, Cross- shore Street, Greenock) Ship and Engineer Surveyors Ship and Engineer Surveyors W. R. Austin J. Harbottle Ship and Engineer Surveyors Ship and Engineer Surveyor (A. I. Whittell D. M. Chapman G. F. Silley MILFORD HAVEN, with Pembroke and Tenby, and a district extending as far as New Quay inclusive Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) † Not an exclusive Officer of Lloyd's Register.	_		Jervis Dale	Abanime Surveyed J. G. Madallop	
Ship Surveyors J. Craig (Office, Commercial Bank Buildings, 14, Cross-shore Street, Greenock) Ship and Engineer Surveyors { W. R. Austin J. Harbottle Ship and Engineer Surveyors { W. H. Roberts Ship Surveyor Coffice, Bank Chambers, 2, Freeman Street, Great Ship Surveyors { C. Martell W. H. Roberts R. Cheetham (Office, Bank Chambers, 2, Freeman Street, Great Ship Surveyor street, Great J. Craig R. Bennett A. P. W. MacNab MILFORD HAVEN, with Pembroke and Tenby, and a district extending as far as New Quay inclusive † J. W. Johnstone Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) † Not an exclusive Officer of Lloyd's Register.	GREENOCK			C1 1 F	
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Ship and Engineer Surveyors { W. R. Austin Grimsby and Engineer Surveyors { W. R. Austin Boston Ship and Engineer Surveyors { C. Martell W. H. Roberts Ship Surveyor R. Cheetham (Office, Bank Chambers, 2, Freeman Street, Great MILFORD HAVEN, with Pembroke and Tenby, and a district extending as far as New Quay inclusive Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) † Not an exclusive Officer of Lloyd's Register.		Buildings, 14, Cross-	R. Bennett A. P. W. MacNab	(deed year	
Grimsby and Boston Ship and Engineer Surveyors { C. Martell W. H. Roberts Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) (Office, Bank Chambers, 2, Freeman Street, Great C. Martell Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) The property of the control of the property of the control of the c		shore street, dreehock)			
Grimsby and Boston Ship and Engineer Surveyors { C. Martell W. H. Roberts Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) (Office, Bank Chambers, 2, Freeman Street, Great C. Martell Ship and Engineer Surveyor (Address, Point House, Llanstadwell, Neyland) The property of the control of the property of the control of the c		Ship and Engineer Surveyors {	J. Harbottle	tending as far as New	+ I W Johnstone
Ship Surveyor R. Cheetham (Office, Bank Chambers, 2, Freeman Street, Great (Address, Point House, Llanstadwell, Neyland) † Not an exclusive Officer of Lloyd's Register.		O Shin and Fraimon Summers	C. Martell		J. W. Johnstone
(Office, Bank Chambers, 2, Freeman Street, Great † Not an exclusive Officer of Lloyd's Register.	BOSTON			(Address, Point House,	
Treeman Street, Great		(Office, Bank Chambers, 2,			's Register.

Newcastle-on-Tyne, with North and South Shields; also Blyth and Warkworth Harbour Ship Surveyors (Office, Collingwood Buildings, Collingwood Street, Newcastle) (Telegrams, Register.)	George Harrison Principal Surveyor E. J. Milton A. R. Sneddon A. Munro G. L. Brown T. Shaw John Macdonald L. G. G. Demarest M. Macleod B. C. Laws, B.Sc. J. S. Butler W. A. Brydon J. A. Whitford	QUEENSTOWN, with Cork, Kinsale, Crook- haven, Castletown, Bantry, Valentia, Tralee, River Shannon and Limerick, as well as all intermediate Ports
Ship and Engineer Surveyors	R. W. Coomber C. Cooper G. Murdoch T. Field L. G. Shallcross C. J. Hudson J. E. Sellex R. Lee Annear, B.Sc. J. Houston W. Cowie	SOUTHAMPTON, and South Coast from Littlehampton to Bridport, inclusive, also the Isle of Wight
Inspector of Forgings	William Campbell	SUNDERLAND AND SEAHAM (F. R. Noton Principal Surveyor A 1
Newport, Mon., with Chepstow and Lydney Ship and Engineer Surveyors Ship Surveyor (Office, Bank Chambers, Newport, Mon.)	S. Townend	Ship Surveyors J. Allan T. S. Leathard T. S. Shute Sunderland T. S. Shute R. M. McLaren (J. T. Findlay
ORKNEYS (residing at Stromness) †Not an exclusive Officer of Lloyd's Regist		Ship and Engineer Surveyors \{\text{W. Butler} \ \L. C. Davis} \] Inspector of Forgings M. Robertson
PLYMOUTH Ship and Engineer Surveyors (Office, 13, Exchange) PORTMADOC AND BARMOUTH, with a district extending as far as, but not including, New Quay (Address, Eifion House, Portmadoc)	J. C. Larg	SWANSEA, with Llanelly, Neath and Port Talbot G. C. Vaux Ship and Engineer Surveyors (Office, Lancaster Chambers, 17, Wind Street, Swansea) WATERFORD Ship and Engineer Surveyor †Andrew Horn † Not an exclusive Officer of Lloyd's Register.

LIST OF FOREIGN AND COLONIAL SURVEYORSHIPS OF LLOYD'S REGISTER,

The Surveyors at the following Ports do not hold appointments as the exclusive Officers of the Society, excepting in the cases marked* RUSSIA. GERMANY—continued. *J. Meijer ODESSA, with Nikolaieff, Kertch, and DÜSSELDORF, Ship and Engineer Surveyors for Steel Testing duties and *R. Hauss In an extremal for the strong in Novorossisk Inspection of Forgings, &c., *Hans Kolbow Ship and Engineer Surveyor \ *G. Robson (Office, Khersonskaya 54, Kv. 8, Odessa) in Germany *M. Berg *Exclusively an Officer of Lloyd's Register. Düsseldorf, 109) (TELEGRAMS, Meijer Herderstrasse 70) RIGA, with Windau and Libau * Exclusively Officers of Lloyd's Register. Ship and Engineer Surveyor Eduard Buchholz (Address, Muckenholm Strasse No. 37, Riga.) (TELEGRAMS, Surveyor) HAMBURG, with the River Elbe, Lubeck, Rostock, and ports in Schleswig-Holstein and Mecklenburg *Geo. Dykes Ship Surveyors ... *C. H. F. Priess NORWAY. Ship and Engineer Surveyor S. A. Eide (TELEGRAMS, Surveyor) BERGEN (Office, Steinhöft No. 3, Hamburg, 11) (TELEGRAMS, Dykes, Steinhöft) * Exclusively Officers of Lloyd's Register. Christiania, with a district extending from $\underbrace{ \begin{array}{c} \textit{Engineer Surveyor for the} \\ \textit{Hamburg District} \dots & \cdots \end{array}}_{\text{(Office, Steinhöft No. 3, Hamburg, 11)}} \mathbf{M. \ Berendt}_{\text{(Telegrams, Ingbert)}}$ Fredrikshald to Lindesnæs Ship and Engineer Surveyor Assistant Engineer Surveyor J. Köhler SWEDEN Swinemunde Emil Herzberg Ship and Engineer Surveyor (Telegrams, Herzberg, STETTIN, with Swinemunde GOTHENBURG, with a district extending from Strömstad to Halm-(Office, Bollwerk, 1, Stettin) Lloydssurveyor) stad, and from Vestervik to *V. C. Bülow Sölvesborg; also Frederik-... *G. W. Jörgensen HOLLAND. Ship and Engineer Surveyors (TELEGRAMS, Surveyer) (Office, Hertzia, Packhus-AMSTERDAM, with Veendam, Nieuwediep, platsen, 2) and neighbouring Ports ... *J. B. Slebe Ship and Engineer Surveyors *H. P. Burgdorffer *Exclusively Officers of Lloyd's Register. (Office, Binnenkant, No. 27, (TELEGRAMS, Lloyd's Register) STOCKHOLM, with a district including Gefle Amsterdam) and Norrköping, with intermediate Ports, and *Exclusively Officers of Lloyd's Register. also Wisby Albert Isakson (TELEGRAMS, Lloyd's Register) Ship and Engineer Surveyor ROTTERDAM, with Dordrecht, Schiedam, and (Address, Drottgården, 14 & 16, surrounding places, also Stadsgården) *R. Leeuwenburg Zeeland Ship Surveyors *A. Schouwenaar DENMARK. Ship and Engineer Surveyors (Office, Veerhaven, W.Z. 19b, Rotterdam) *F. N. Bernoski *J. J. Schoo (Telegrams, Lloyd's Register) Ship and Engineer Surveyors *H. J. Sonne COPENHAGEN (Office, Amaliegade, 361, *A. F. Örbech *A. T. Poulsen Copenhagen, K.) ... *J. A. A. C. von Rosen Ship Surveyor *Exclusively Officers of Lloyd's Register. (TELEGRAMS, Engineer) *Exclusively Officers of Lloyd's Register. BELGIUM. GERMANY. Bremen, with Bremerhaven, Emden and

surrounding Ports *G. H. C. Bahr Ship and Engineer Surveyor (Telegrams, Bahr, Rolandhaus, Bremen)

Ship and Engineer Surveyor (Address, Pommersche Strasse, 38, Carl Schirnick

(Óffice, Rolandhaus, Bremen) *Exclusively an Officer of Lloyd's Register.

Zoppot, near Danzig)

DANZIG

Dillore	
Antwerp, including all places in Belgium, and the Dutch Port Ter- neuzen	*T. W. Fish Principal Surveyor
Ship Surveyor Ship and Engineer Surveyors (Office, Maritime Buildings, Quai Taverniers, 4, Antwerp)	*N. E. McClelland *A. E. Farminer *J. E. J. Wilvers (TELEGRAMS, Register)
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FOREIGN AND COLONIAL SURVEYORSHIPS-continued.

FOREIGN	AND COLONIAL SURV	EYORSHIPS—continued
	FRANCE.	
BORDEAUX	Engineer Surveyor	Albert Vandercruyce Arthur Donzelle (TELEGRAMS FOR THE SUR-
	(Office, 16, rue Esprit des Lois)	VEYORS, Vandercruyce, 16, rue Esprit des Lois)
DUNKIRK, with	Calais Ship and Engineer Surveyor (Office, rue des Pierres No.22, Dunkirk)	
	District including Boulogne, Barfleur, and Rouen Ship Surveyor Engineer Surveyor and Assistant Ship Surveyor (Office, 61, rue de la Bourse, Hâvre) ely Officers of Lloyd's Register	*M. G. Boyer *A. Cartier (TELEGRAMS, Lloy d's Register)
MARSEILLES	Ship and Engineer Surveyor) * . D T
	(Office, 16, rue Beauvau) ely an Officer of Lloyd's Register.	*A. P. Jones
NANTES	Ship and Engineer Surveyor (Office, 2, rue Racine)	William Kerr (Telegrams, Kerr, rue Racine)
	SPAIN AND PORTUG	AL.
BARCELONA	Ship and Engineer Surveyor (Office, Calle de Mallorca 259)	G. E. A. Muston (TELEGRAMS, Muston, Mallorca 259)
	Ship and Engineer Surveyors (Office, Aurora Building, Calle de la Estacion, 5) ly Officers of Lloyd's Register.	*J. Pollock
CADIZ	Ship and Engineer Surveyor	William West
	(Address, Isaac Peral, 8)	(TELEGRAMS, West)
LISBON	Ship and Engineer Surveyor (Address, 7, T. do Caes do Tojo)	
SEVILLE	Ship and Engineer Surveyor (Office, Laraña, 12)	José Pina (Telegrams, Pina)
	GIBRALTAR.	
GIBRALTAR	Ship and Engineer Surveyor (Address, H.M. Naval Yard)	W. H. Beckett (Telegrams, Yard)
	ITALY.	
GENOA *Exclusiv	Ship and Engineer Surveyor Ship Surveyor (Office, Piazza S. Giorgio No. 32, 1 ^a Scala) rely Officers of Lloyd's Register.	(TELEGRAMS, Surveyors)
LEGHORN	(Address, Piazza Micheli)	Amerigo Gori (TELEGRAMS, A. Gori)
Naples, with	Messina and other Ports in	1
	Ship and Engineer Surveyor (Torre Annunziata, nea Naples; also at Viale Elena No. 16, Naples)	T Ducoster, TorreAnnunziata)
	AUSTRIA-HUNGAI	RY.
FIUME, with	the coast South of Pola, and the Dalmatian Islands Ship Surveyor Engineer Surveyor (Office, Governo Marittimo Fiume)	Arturo Duimich Matteo Petrich

AUSTRIA-HUNGARY—continued.

TRIESTE, with Pola and the coast North of
Pola; also Venice ...
Ship Surveyor
Ship and Engineer Surveyor
(Office, Via San Giorgio, No. 5,
Trieste)
*Bernard J. Ives
*G. D. Ritchie
(Telegrams, Lloydregister,
Sangiorgio, Trieste)

*Exclusively Officers of Lloyd's Register

VIENNA Ship and Engineer Surveyors
for Steel Testing duties and
Inspection of Forgings, &c.,
in Austria-Hungary and
Upper Silesia
(Address, Schelleingasse 52^{IX},
Vienna IV/2)

*Exclusively Officers of Lloyd's Register.

*M. Koch
*J. Rolland
(Telegrams, Surveyor)

MALTA.

MALTA Ship and Engineer Surveyor C. H. Wright (Office, 21, Strada Zaccaria, Valetta.) (Telegrams, Register)

GREECE, TURKEY, AND ROUMANIA.

CONSTANTINOPLE, including the Bosphorus,

Sea of Marmora, and the

Dardanelles

Ship and Engineer Surveyor

(Office, Ferménédjiler YeniHan, Galata; Postal Address,
P.O. 27, c/o British Post Office)

* Exclusively an Officer of Lloyd's Register.

GALATZ AND

BRAILA

BRAILA

as far as the mouth of the Danube and including Sulina (residing at Braila)

PIRÆUS Ship and Engineer Surveyor *W. W. Barnes
(TELEGRAMS, Barnes)

* Exclusively an Officer of Lloyd's Register.

Syra Ship and Engineer Surveyor Edward Eyssartier
(Telegrams Eyssartier)

CANADA.

PRINCIPAL SURVEYOR FOR THE UNITED STATES AND CANADA "James H. Mancor (Office, 17, Battery Place, New York)

*Exclusively an Officer of Lloyd's Register.

HALIFAX, N.S. Ship and Engineer Surveyor John L. G. Cooke (Address, Room 37, Furness Withy Building)

MONTREAL ... (Address, Port Warden's Office) Archibald Reid (Telegrams, Portwarden)

PRINCE EDWARD ISLAND H. P. Welsh (Office, 296, Grafton Street, Charlottetown) (TELEGRAMS, Register, Charlottetown)

QUEBEC, and the River St. Lawrence ... Ship and Engineer Surveyor (Office, 40, Dalhousie Street) Joseph Samson (Telegrams, Samson)

St. John, N.B. Ship and Engineer Surveyor C. E. Dalton (Telegrams, Dalton)

FOREIGN A	ND COLONIAL SURVEYORSHIPS—continued.
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TORONTO, ONT	Lake Ontario and Colling- wood, Ont Ship and Engineer Surveyor (Residing at Barrie, Ont.)
VANCOUVER CITY, B.C.	including Victoria, Van- couver Island, and all Ports in British Columbia Ship and Engineer Surveyor (Office, 426, Winch Building, Hastings Street, (P.O. Box 642), Vancouver City)
	NEWFOUNDLAND.
ST. JOHN'S	Ship and Engineer Surveyor (Office, Fisheries and Marine Department, Custom House) *J. Black (TELEGRAMS, Surveyor)
Exclusiv	vely an Officer of Lloyd's Register.
1	UNITED STATES OF AMERICA.
New York	Principal Surveyor for the \Interpolation \text{James H. Mancor} \Interpolation \text{States and Canada} \text{*James H. C. Farrar}
	C*A. W. Murray
	Ship and Engineer Surveyors *A. W. Murray *J. S. Blackett *E. Bennett *F. W. Dawkins
* Exclusiv	(Office, 17, Battery Place, New York.) ely Officers of Lloyd's Register.
Baltimore, MD	Ship and Engineer Surveyor Ship Surveyor
	ely Officers of Lloyd's Register.
BOSTON, MASS.	Ship and Engineer Surveyor (Office, Fiske Building, 89, State Street) *B. Stewart Murphy (TELEGRAMS, Register)
	ely an Officer of Lloyd's Register.
	Ship Surveyor *James French (Office, 1517, Rockefeller Building) Engineer Surveyor for Cleveland District (residing at Pittsburg, Pa.) *J. S. Heck
	y Officers of Lloyd's Register.
GALVESTON, TEXAS	Ship and Engineer Surveyor *C. J. M. Mancor
* Exclusiv	ely an Officer of Lloyd's Register.
LA.	Ship and Engineer Surveyor * J. M. Buchanan (Office, 810, Hennen Building) \((Telegrams, Retsiger) \)
* Exclusivel	y an Officer of Lloyd's Register.
NEWPORT NEWS, VA.	Ship and Engineer Surveyor (Office, 2711, Washington (Telegrams, Marsden Avenue) ely an Officer of Lloyd's Register.
	Ship and Engineer Surveyor) *R. Haig
Pa.	Ship Surveyor

(Office, 324, Bourse)

* Exclusively Officers of Lloyd's Register.

(TELEGRAMS, Haio)

UNITED STATES OF AMERICA—continued. PITTSBURG, PA. Ship and Engineer Surveyor) for Steel Testing Duties ... *J. S. Heck (Office, 5,630, Rural Street) * Exclusively an Officer of Lloyd's Register PORTLAND, OREGON, including both shores of the Columbia River and all Ports in Oregon... Lyddon Veysey (Office, Room 208, Commercial) (TELEGRAMS, Register) Club Building, Fifth and Oak Streets) San Francisco, Ship Surveyor (John Metcalfe Engineer Surveyor W. H. Stewart (Office, 454, California Street) (TELEGRAMS, Freeboard) CAL. SEATTLE, WASH., with Tacoma, Port Townsend and all Ports in Washington Territory; not including the Washington shore of the Columbia River Ship and Engineer Surveyor James Fowler (Office, 503, Maynard Building, (TELEGRAMS, Llouds) First Avenue, Corner Washington Street, Seattle) MEXICO. Ship and Engineer Surveyor \ G. Howard VERA CRUZ (Office, Naval Military College) (TELEGRAMS, Inamecon) BRITISH WEST INDIES. J. B. Saunders TRINIDAD ... (TELEGRAMS, Harbour DANISH WEST INDIES. T. V. C. Kruse ST. THOMAS (TELEGRAMS, Kruse) SOUTH AMERICA. Bahia Blanca Ship and Engineer Surveyor J. H. Brewer (Address, La Usina Electrica, (Telegrams, Brewer, clo Bumodus) Calle Donado) BUENOS AYRES Ship and Engineer Surveyors *P. I. Adie AND ROSARIO, (Office, Calle San Martin, *J. C. G. Williamson 264, Buenos Ayres) *A. Moffat (TELEGRAMS, Adie) * Exclusively Officers of Lloyd's Register. (Address, Harbour Master's L. H. J. Tinney Office, 15, Water Street, L. H. J. Tinney DEMERARA (TELEGRAMS, Heliostat) Georgetown) $\begin{array}{c} \textit{Ship and Engineer Surveyor} \\ \texttt{(Address, Caixa do Correio, No. 100)} \end{array} \} \begin{array}{c} \texttt{Bruce Thompson} \\ \texttt{(Telegrams, Bruce)} \end{array}$ MANAOS MONTE VIDEO PARA Ship and Engineer Surveyor Punta Arenas, Ship and Engineer Surveyor J. J. Dickson (Address, Apostadero Naval) (TELEGRAMS, Maestranza) CHILI RIO DE JANEIRO Ship and Engineer Surveyor | Robert Vance (Address, Caixa 636) (TELEGRAMS, Register) TALCAHUANO Ship and Engineer Surveyor (A. F. Smith VALPARAISO (TELEGRAMS, Smith, Pacific, Valparaiso) (Address, Casilla 934) EGYPT AND RED SEA. Ship and Engineer Surveyor T. W. Twaddle (Address, Hedjuff) (Telegrams, Twaddle) ADEN

(Address, Hedjuff)

(Address, The Arsenal)

ALEXANDRIA

Ship and Engineer Surveyor \ J. E. Roberts

(TELEGRAMS, Roberts)

FOREIGN A	ND COLONIAL SURVEYORSHIPS—continued	7.		
	SOUTH AFRICA.	CHINA.		
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East London	(Address, The Shipping Office) William Hildyard (Telegrams, Register)	* Exclusively an Officer of Lloyd's Register. TIENTSIN Ship and Engineer Surveyor \ W. Wilson		
PORTELIZABE	THShip and Engineer Surveyor H. McG. Richardson (Telegrams, Richardson, Harbour, Port Elizabet)	$(Address, Victoria Road)$ $\int (TELEGRAMS, Dumbarton)$		
PORT NATAL	(Address, 3, Castle Buildings,) Frederick Airth	GAFAN.		
TORT TRAILE	Durban) (TELEGRAMS, Airth, Durban	KOBÉ Ship and Engineer Surveyor *A. L. Jones (Office, 16A, Harima Machi) (Telegrams, Register) * Exclusively an Officer of Lloyd's Register.		
	MAURITIUS.	NAGASAKI Ship and Engineer Surveyor *A. C. Heron		
MAURITIUS	(residing at Port Louis) M. S. McDonald (TELEGRAMS, McDonald, Port Louis, Mauritius)	Ship Surveyor *G. D. Aitken (Office, 42c, Sagarimatsu) *(Telegrams, Register) * Exclusively Officers of Lloyd's Register.		
TNIDIA (TEVIAN DIIDMAU SIAM AND STRAITS	YOKOHAMA Ship and Engineer Surveyor) *A. S. Williamson		
INDIA, C	EEYLON, BURMAH, SIAM, AND STRAITS SETTLEMENTS.	(Office, 23, Water Street; P.O.) (TELEGRAMS, Register) Box 48) * Exclusively an Officer of Lloyd's Register.		
BANGKOK	Ship and Engineer Surveyor	HAKODATE Assistant Ship and Engineer) Gosaku Horiuchi		
Вомвач	Ship and Engineer Surveyor A. T. Graham (Office, Gool Mansions,	Surveyor (Address, 43, Ohmachi) (GOSAKU HOFIUCHI (TELEGRAMS, Horiuchi, Ohmachi, Hakodate)		
* Exclusive	Wellington Lines, Mayo Road) (TELEGRAMS, Surveyor) ely an Officer of Lloyd's Register.	AUSTRALIA AND NEW ZEALAND.		
CALCUTTA	Ship and Engineer Surveyor \ *J. H. Mackirdy	ADELAIDE, S. A. (Office, Lipson Street, Port J. H. Gibbon Adelaide) (Telegrams, Gibbon)		
(Office, 2, Hare Street)) (TELEGRAMS, Freeboards) * Exclusively an Officer of Lloyd's Register.		Auckland, N.Z M. T. Clayton		
Согомво	Ship and Engineer Surveyor H. B. Ratsey (Telegrams Ratsey)	BRISBANE, QUEENSLAND		
KARACHI	Ship and Engineer Surveyor (Address, Persian Gulf Telegraphs, Manora, Karachi)	*Christohurch& Lyttelton,N.Z.		
PENANG	Ship and Engineer Surveyor H. Muir (Telegrams, Muir)	Dunedin, N.Z. Ship and Engineer Surveyor A. Morrison (Address, 123, High Street) (Telegrams, Cellular)		
RANGOON	(Address, Lower Poozoon- R. P. Taylor doung) (Telegrams, Orion)	FREMANTLE, W.A D. E. A. 11		
SINGAPORE	Ship and Engineer Surveyor \ *Andrew Couper	(Address, Dalgety's Buildings, R. E. Arundel (Telegrams, Arundel)		
* Exclusi	(Office, 6A, Flint Street) (TELEGRAMS, Couper) vely an Officer of Lloyd's Register.	VICTORIA Ship and Engineer Surveyor (Office, New Zealand Chambers, 483, Collins Street) Alexander McCowan (Telegrams, Reports)		
	EAST INDIAN ARCHIPELAGO.	NAPIER, N.Z John C. Tonkin		
BATAVIA	H. van Taalingen (Telegrams, Taalingen)	(TELEGRAMS, Tonkin, Surveyor) NEWCASTLE, N.S.W. Ship Surveyor J. W. Vellacott (Office, Carrington Chambers, Watt Street) (TELEGRAMS, Backstay)		
Manila, P.I.,	and Ports in the Philippine	Engineer Surveyor $\langle F. A. Spence \rangle$		
	Ship and Engineer Surveyor (Telegrams, Turbine)	(Office, 1, Bolton Street) (TELEGRAMS, Spence, clo Barambio)		
	(Address, Anloague No. 10, Binondo; P.O. Box 307)	PORT PIRIE, S.A., with Port Germein and Wallaroo Alfred M. Mars (Address, Institute Building, (Telegrams, Mars)		
Sourabaya	Ship and Engineer Surveyor B. N. Powell (Telegrams, Powell)	Alexandra Street, Port Pirie)		
	(IDDEGRAMO, TOWER)	Sydney, N.S.W. Ship and Engineer Surveyor *R. Pollock		
	HONG KONG.	(Office, 17, Bridge Street) (TELEGRAMS, Miramar)		
Hong Kong	Ship and Engineer Surveyor *John Lambert	* Exclusively Officers of Lloyd's Register.		
	(Office, 5, Alexandra Buildings; P.O. Box 463)	TIMARU, N.Z James Tait Wellington, N.Z		
* Exclusi	vely an Officer of Lloyd's Register.	TI AMAZINIA AND THE STATE OF TH		

71, Fenchurch Street, London, 1st January, 1912.

LIST OF SURVEYORSHIPS OF LLOYD'S REGISTER.

(ALPHABETICALLY ARRANGED.)

THE SURVEYORS AT THE PORTS MARKED * ARE EXCLUSIVELY THE OFFICERS OF THE SOCIETY, AND ARE NOT PERMITTED TO ENGAGE IN ANY OTHER BUSINESS OR EMPLOYMENT WHATSOEVER.

	S. J. P. THEARLE, D.Sc., Chief Ship Surveyor of	Principal Surveyor for London	AUCKLAND, N.Z		M. T. Clayton (TELEGRAMS, Replento)
	Lloyd's Register.	Ship Surveyors:	Bahia Blanca	Ship and Engineer Surveyor (Address, La Usina Electrica,	(TELEGRAMS, Brewer,
	Assistants to Chief Ship Surveyor:	D. Nicholas R. Howie	*Baltimore, M	Calle Donado) [D.Ship and Engineer Sur-	c o Bumodus)
	C. Buchanan E. C. Champness C. Fowling	G. F. Robson W. H. Watson R. B. Watt J. W. Grier			H. A. Stewart A. Allen (Telegrams, Surveyor)
idouisellija Situatus stantas Situatus stantas	Principal Surveyors on the Chief Ship Surveyor's Staff: G. R. Mares T. S. Warren	J. Montgomerie, B.Sc. C. C. Gearing	BANGKOK	Ship and Engineer Surveyor	Tanana Tanan
.03	JAMES T. MILTON,	R. D. Cairns J. F. Isherwood A. Chisholm, B.Sc.	BARCELONA	Ship and Engineer Surveyor (Office, Calle de Mallorca 259)	G. E. A. Muston (TELEGRAMS, Muston, Mallorca 259)
*LONDON	M.Inst.C.E., Chief Engineer Surveyor of Lloyd's Register.	H. J. Cox W. Thomson, B.Sc.	*Barrow	Ship and Engineer Surveyor (Office, Ramsden Square)	J. Easthope
(Telegrams (Committee)	Assistant to Chief Engineer Surveyor: H. A. Ruck-Keene,	R. J. L. Ward, B.Sc. R. Balfour T. R. Blackie	*Barry	Ship and Engineer Surveyors (Office, Dock Chambers, Barry Dock) Ship Surveyor	Wm. J. Darling J. G. Mackillop G. O. Common H. C. T. Ireland
	M.INST.C.E.	J. W. Dimmock H. H. Ashton H. P. Cornish	BATAVIA		H. van Taalingen
Shipand Engineer Surve	Shipand Engineer Surveyors	J. B. A. Common	*Belfast	Ship and Engineer Surveyors Ship Surveyors	R. J. Beveridge A. T. Thomas S. O. Kendall
	and the second of the second o			(Office, 97 & 98, Scottish Provident Institution Build- ings, Donegall Square West)	J. McIlvenna
		A. Lawrance, B.Sc. H. L. Fletcher	BERGEN	Ship and Engineer Surveyor	S. A. Eide (TELEGRAMS, Surveyor)
	Draughtsman	David S. Hunter	*Bideford	(Address, Odun Road, Appledore, Devon)	J. Hand
*ABERDEEN	Ship and Engineer Surveyor Ship Surveyor		*BILBAO	Ship and Engineer Surveyors (Office, Aurora Building, Calle de la Estacion, 5)	J. Pollock I. de Mutiozabal (Telegrams, Register)
ADELAIDE, S.A.	(Office, Lipson Street, Port	J. H. Gibbon (Telegrams, Gibbon)	*Вомвач	Ship and Engineer Surveyor (Office, Gool Mansions, Wellington Lines, Mayo Road)	A. T. Graham (TELEGRAMS, Surveyor)
ADEN	Ship and Engineer Surveyor (Address, Hedjuff)	T. W. Twaddle (TELEGRAMS, Twaddle)	BORDEAUX		Albert Vandercruyce Arthur Donzelle (TELEGRAMS FOR THE SUR-
ALEXANDRIA, EGYPT	Ship and Engineer Surveyor (Address, The Arsenal)	J. E. Roberts (TELEGRAMS, Roberts)	*Boston, Mass	Lois) s. Ship and Engineer Surveyor	VEYORS, Vandercruyce, 16, rue Esprit des Lois)
*AMSTERDAM	Ship and Engineer Surveyors (Office, Binnenkant, No. 27)	J. B. Slebe H. P. Burgdorffer	Dobton, Billion	(Office, Fiske Building, 89, State Street)	(B. Stewart Murphy (TELEGRAMS, Register)
*Antwerp		(TELEGRAMS, Lloyd's Register) T. W. Fish	BRAILA AND GALATZ	(residing at Braila)	(TELEGRAMS, Archbold)
ANTHERI	Ship Surveyor	N. E. McClelland	*Bremen	Ship and Engineer Surveyor (Office, Rolandhaus)	G. H. C. Bahr (TELEGRAMS, Bahr, Rolandhaus)
	Ship and Engineer Surveyors (Office, Maritime Buildings, Quai Taverniers, 4)	A. E. Farminer J. E. J. Wilvers (TELEGRAMS, Register)	Brisbane, Queenslani	(Office, Parbury's Buildings, Eagle Street)	R. S. Taylor (TELEGRAMS, Surveyor)

LIST OF SURVEYORSHIPS (ALPHABETICALLY ARRANGED)—continued.

LIST O	F SURVEYORSHIPS (ALPHABETICALLY ARRANGED)—continued.	
*Bristol	Ship and Engineer Surveyor G. A. D. Toyne (Office, 53, Queen Square)	DEMERARA	(Address, Harbour Master's Office, 15, Water Street, Georgetown) (TELEGRAMS, Heliostat)
*BuenosAyr	EESShip and Engineer Surveyors P. I. Adie 10 (Office, Calle San Martin, 264, J. C. G. Williamson Buenos Ayres) (A. Moffat	DOVER	John Iron (TELEGRAMS, Harbour Master)
CADIZ	Ship and Engineer Surveyor William West	*Dublin	Ship and Engineer Surveyor (Office, 115, Philipsburgh Avenue) (Tellegrams, Macwilliam, 115, Philipsburgh Avenue)
*CALCUTTA	(Address, Isaac Peral, 8) (Telegrams, West) Ship and Engineer Surveyor; J. H. Mackirdy	*Dundee	Ship and Engineer Surveyor E. M. Salmon Ship Surveyor M. Blackwood
CAPE TOWN	(Office, 2, Hare Street) (TELEGRAMS, Freeboards) (Address, Dock Office) W. Stephen		(Office, Maritime Buildings, East Dock Street)
	(TELEGRAMS, Navigation)	Dunedin, N.Z.	. Ship and Engineer Surveyor A. Morrison (Address, 123, High Street) (TELEGRAMS, Cellular)
*CARDIFF	Henry Hand Principal Surveyor Ship Surveyors (J. Petree	DUNKIRK	Ship and Engineer Surveyor F. C. Morel (Office, rue des Pierres, (TELEGRAMS, Morc!, Lloyd's) No. 22)
	(Office, Merchants' Exchange, A. B. R. Harris Bute Docks) E. 1. Evans (TELEGRAMS, Register)	*Düsseldorf	for Steel Testing duties and R. Hauss P. F. J. Abel
	Ship and Engineer Surveyors Ship and Engineer Surveyors W. Lane		Inspection of Forgings, &c., In Germany (Office, Herderstrasse 70, Düsseldorf, 109) Hans Kolbow M. Berg (Telegrams, Meijer, Herderstrasse, 70)
*CHANNEL	J. F. Robson	East London, S. Africa	(Address, The Shipping Office) William Hildyard (TELEGRAMS, Register)
ISLANDS *CHRISTCHUI	(Office, 15, Mulcaster Street, St. Helier's, Jersey) J. F. Picot	*FALMOUTH	Ship Surveyor (Office, Pendennis House, Lansdowne Road)
& Lyttelto N.Z.			Ship and Engineer Surveyor F. Davis
CHRISTIANIA	$Ship\ and\ Engineer\ Surveyor$	FIUME	Ship Surveyor Arturo Duimich Engineer Surveyor Matteo Petrich (Office, Governo Marittimo) Arturo Duimich (Matteo Petrich (TELEGRAMS FOR THE SURVEYORS, Duimich, Porto, Fiume)
*CLEVELAND OHIO	, Ship Surveyor James French (Office, 1,517,Rockefeller Building)	FREMANTLE, W	(Address, Dalgety's Buildings, R. E. Arundel Cliff Street)
	Engineer Surveyor for Cleveland District J. S. Heck	GALATZ	(See Braila)
Collingwood	(residing at Pittsburg, Pa.) O, ONT. (See TORONTO, ONT.)	*Galveston, Texas	Ship and Engineer Surveyor C. J. M. Mancor
COLOMBO *CONSTANTI-	Ship and Engineer Surveyor H. B. Ratsey (TELEGRAMS, Ratsey) Ship and Engineer Surveyor)	*GENOA	Ship and Engineer Surveyor Ship Surveyor
NOPLE	(Office, Ferménédjiler, Yeni- Han, Galata; Postal Address, P.O. 27, c/o British Post (TELEGRAMS, Mumford Yeni-Han, Galata)	GIBRALTAR	Ship and Engineer Surveyor W. H. Beckett (Address, H.M. Naval Yard) (TRLEGRAMS, Fard)
*Copenhage	Office) N Ship and Engineer Surveyors (Office, Amaliegade, 361, Copenhagen, K.) H. J. Sonne (A. F. Örbech A. T. Poulsen		T. J. Dodd Principal Surveyor J. D. Mares R. Wright G. M. Shaw
Danzig	Ship Surveyor \{J.A.A.C. von Rosen \{\text{TELEGRAMS}, Engineer}\}	*GLASGOW	Ship Surveyors (Office, 342, Argyle Street) (Telegrams, Register) W. Watt
MANDIG	Ship and Engineer Surveyor (Address, Pommersche Strasse, 38, Carl Schirnick Zoppot, near Danzig)		G. Nicol W. A. Grier A. Scullard
*DARLINGTON	Inspector of Forgings F. Cook (Office, 9, Granville Terrace)		A. Pickworth, B.Sc. J. S. Gardiner

LIST OF SURVEYORSHIPS (ALPHABETICALLY ARRANGED)--continued.

DIOI OI	SORVETORSHITS (AM)		-communea.	EUROPE DE L'ANDRE DE L	
		John H. Heck	KARACHI	Ship and Engineer Surveyor) E II I
		H. Clarke A. McKeand		(Address, Persian Gulf	F. H. Jones
		P. McGregor	*Кове́	Telegraphs, Manora, Karachi)	
		H. Gardner-Smith	HOBE	Ship and Engineer Surveyor	1
		W. G. Minchin	LEGHORN	(Office, 16A, Harima Machi)	(TELEGRAMS, Register)
**	nelli ili pagemakeenineli ki	C. H. L. Pilditch		(Address, Piazza Micheli)	Amerigo Gori (Telegrams, A. Gori)
*GLASGOW	Ship and Engineer Surveyors	H. C. Forster P. T. Brown	*LEITH	Ship and Engineer Surveyors	
(Cont.)		A. Smellie		(Office, Royal Bank Buildings,	W. D. Heck, B.Sc.
		G. E. Bench		28, Constitution Street)	
		T. W. C. Napier	1 rapus	Ship Surveyor	J. R. Henderson
		J. Davey	LISBON	Ship and Engineer Surveyor	George Payne
		F. A. Ferguson		(Address 7, T. do Caes do Tojo)	(TELEGRAMS, Enyap)
		J. Blellock			(R. Williamson
	Inspectors of Forgings for		*LIVERPOOL	Ship Surveyors	J. Bradley
	the Clyde District	(Jervis Dale		(Office, 201, Tower Building)	S. A. G. Nash
*GOTHENBURG	Ship and Engineer Surveyors	(V. C. Bülow		(TELEGRAMS, Register)	W. R. M. Aspinall
	(Office, Hertzia, Packhus-	G. W. Jörgensen	,	1001 . Shake the same of the same of	W. G. Haig
	platsen, 2)	(TELEGRAMS, Surveyor)			J. Dykes
*Greenock &	1 0	(E. J. Tierney			W. Sibun
PORT GLASGOW	Office, Commercial Bank Buildings, 14, Cross-shore			01: 17 : 0	B. G. Oxford
	Street, Greenock)	R. Bennett		Ship and Engineer Surveyors	1
		A. P. W. McNab			R. D. Shilston
		(W. R. Austin		In I . Well-state of the state	A. J. Barrett W. G. McKinlay
	$Ship and Engineer Sur {\it {\bf v}} eyors$	J. Harbottle	*LYTTELTON, 1	N.Z. (See Christchurch.)	G. Molelliay
*GRIMSBY &		(C. Martell	MALTA	Ship and Engineer Surveyor	0
BOSTON	Ship and Engineer Surveyors	(W. H. Roberts		(Office, 21, Strada Zaccaria,	C. H. Wright
	Ship Surveyor	R. Cheetham	35	Valetta)	(TELEGRAMS, Register)
	(Office, Bank Chambers, 2, Freeman St., Great Grimsby)		Manaos	Ship and Engineer Surveyor	Bruce Thompson
				(Address, Caixa do Correio, No. 100)	(TELEGRAMS, Bruce)
HAKODATE	(See Yоконама.)		*MANCHESTER	Ship and Engineer Surveyors	F. W. Pitt
HALIFAX, N.S.	Ship and Engineer Surveyor	(John J. G. Cooks		(Office, 162, Trafford Road,	
TO SEE SEE SEE SEE SEE	(Address, Room 57, Furness	(TELEGRAMS, Lloyd)		Salford, Manchester)	(TELEGRAMS, Lloyd's Register, Trafford Road, Salford)
	Withy Building)		MANILA, P.I.	Ship and Engineer Surveyor	Traffora Roaa, Saifora)
*HAMBURG		Geo. Dykes	Promely	(Address, Anloague No. 10,	William Swann
	(Office, Steinhöft, No. 3, Hamburg, 11)	C. H. F. Preiss (TELEGRAMS, Dykes, Steinhöft)	***	Binondo; P.O. Box 307)	(TELEGRAMS, Turbine)
	Engineer Surveyor		*MARSEILLES	Ship and Engineer Surveyor	A. P. Jones
	(Office, Steinhöft No. 3, Ham-	(TELEGRAMS, Ingbert)	Marromarra	(Office, 16, rue Beauvau)) .
tongalf ,h	burg, 11)	+I Vählen	MAURITIUS	(residing at Port Louis)	M. S. McDonald (TELEGRAMS, McDonald,
+ Not or als	Assistant Engineer Surveyor usively Officers of Lloyd's Regist	er.			Port Louis, Mauritius)
	ca : a	D. McAuslan	MELBOURNE,	Ship and Engineer Surveyor	
*HARTLEPOOL	Ship Surveyors (Office, Central Buildings, West	Principal Surveyor	VICTORIA	(Office, New Zealand Chambers, 483, Collins Street)	(TELEGRAMS, Reports)
AND WEST HARTLEPOOL.	11	O. Narbeth W. M. Ward	Magazz		DY DG
THUTTEL COL	the later of the second	(James Innes	MESSINA, and o	other ports in Sicily. (See NA	PLES.)
	Ship and Engineer Surveyors		an Mandania a		(W. L. Gilmour
· Oral artist	Sittly with Diegenoor Sur Cogoro	C. O. Craven	*MIDDLES-	with Stockton	Principal Surveyor T. G. Baker
*Hâvre	Ship Surveyor	(M. G. Boyer	BROUGH	Ship Surveyors (Office, Royal Exchange,	J. R. Dippie
HAVRE	Engineer Surveyor and			Middlesbrough)	J. W. Stuart
	Assistant Ship Surveyor	A. Cartier			N. G. Turnbull
	(Office, 61, rue de la Bourse)	(TELEGRAMS, Lloyd's Register)			W. Morrison
*Hong Kong	Ship and Engineer Surveyor	John Lambert		m. 15	J. Kerr
	(Office, 5, Alexandra Build-	(TELEGRAMS, Marine)		Ship and Engineer Surveyors	
	ings; P.O. Box, 463)				D. M. Chapman G. F. Silley
*HULL	1	A. B. Wilson Principal Surveyor			(d. I. billey
	(Office, Ocean Chambers, Lowgate, Hull)	F. C. Smith	MILFORD	Ship and Engineer Surveyor	J. W. Johnstone
		(F. L. Sturgeon	HAVEN	(Address, Point House, Llanstadwell, Neyland)) The confidence
	Ship and Engineer Surveyors		MONTE VIDEO.		J. W. Postlethwaite
		T. G. Dodd		(Address, Calle Zabala, 69)	(TELEGRAMS, Amphyl)

LIST OF SURVEYORSHIPS (ALPHABETICALLY ARRANGED)—continued.

LIST O	OF SURVEYORSHIPS (ALI	PHABETICALLY ARRANGEL)—continued.		
MONTREAL	$({\tt Address, PortWarden's Office})$	(TELEGRAMS, Portwarden)	*Odessa	Ship and Engineer Surveyor (Office, Khersonskaya 54,	
*Nagasaki	Ship and Engineer Surveyor Ship Surveyor		ORKNEYS	Kv. 8) (residing at Stromness)	Geo. Gunn Baillie
	(Office, 42c, Sagarimatsu)	(TELEGRAMS, Register)	PARA	Ship and Engineer Surveyor	1
NANTES	Ship and Engineer Surveyor (Office, 2, rue Racine)	(TELEGRAMS, Kerr, rue		Simp and Engineer Surveyor	}
Napier, N.Z.		(John C. Tonkin	PENANG	Ship and Engineer Surveyor	(THE BOD LANG Martin)
Naples	Ship and Engineer Surveyor	(TELEGRAMS, Tonkin, Surveyor)		A Ship and Engineer Surveyor Ship Surveyor	R. Haig D. Millar
211111111	(Torre Annunziata, near	Francesco Ducoster	PA.	(Office, 324 Bourse)	(TELEGRAMS, Haig)
	Naples; also Viale Elena, No. 16, Naples)	(TELEGRAMS, Ducoster, Torre Annunziata)	*PIRÆUS	Ship and Engineer Surveyor	(TELEGRAMS, Barnes)
LA.	RS, Ship and Engineer Surveyor (Office, 810, Hennen Building)	(TELEGRAMS, Retsiger)	*PITTSBURG, P	A. Ship and Engineer Surveyor for Steel Testing duties (Office, 5,630, Rural Street)	J. S. Heck
*New York	Principal Surveyor for the United States and Canada.	James H. Mancor	*Ргумоптн	Ship and Engineer Surveyor (Office, 13, Exchange)	
	Ship Surveyor	H. C. Farrar	PORT	Ship and Engineer Surveyor	(H. McG. Richardson
	Shin and Franciscon Shuman	A. W. Murray J. S. Blackett	ELIZABETH	(Address, Harbour Works)	(TELEGRAMS, Richardson, Harbour, Port Elizabeth)
	Ship and Engineer Surveyors (Office, 17, Battery Place)	E. Bennett F. W. Dawkins	PORT NATAL	(Address, 3, Castle Buildings, Durban)	Frederick Airth (TELEGRAMS, Airth, Durban)
		(TELEGRAMS, Nymdible)	PORT PIRIE. S.	A. (Address, Institute Building,	
NEWCASTLE,	Ship Surveyor	(J. W. Vellacott			(TELEGRAMS, Mars)
N.S.W.	(Office, Carrington Chambers, Watt Street)	(TELEGRAMS, Backstay)	PORTLAND, OREGON	(Office, Room 208, Commercial Club Building, Fifth and Oak	Lyddon Veysey
	Engineer Surveyor (Office, 1, Bolton Street)	F. A. Spence (Telegrams, Spence, c/o Barambio)	*PORTMADOC	Streets) (Address, Eifion House, Port-	John W. James
		(George Harrison		madoc)	
		Principal Surveyor E. J. Milton A. R. Sneddon	PRINCE ED- WARD ISLANI	(Office, 296, Grafton Street,) Charlottetown)	H. P. Welsh (TELEGRAMS, Register, Charlottetown)
*Newcastle-	Ship Surveyors	A. Munro G. L. Brown	PUNTA ARENAS CHILI	s, Ship and Engineer Surveyor (Address, Apostadero Naval)	
ON-TYNE	(Office, Collingwood Build- ings, Collingwood Street) (TELEGRAMS, Register)	T. Shaw John Macdonald L. G. G. Demarest	QUEBEC	Ship and Engineer Surveyor (Office, 40, Dalhousie Street)	
	transmit Thompstelle Institute in	M. Macleod	*QUEENSTOWN	(Address, 1, Bellevue Terrace)	H. W. Dove
	(ulamin), Shapin	B. C. Laws, B.Sc. J. S. Butler	RANGOON	$({\tt Address,\!LowerPoozoondoung})$	R. P. Taylor (TELEGRAMS, Orion)
		W. A. Brydon J. A. Whitford	RIGA	Ship and Engineer Surveyor (Address, Muckenholm Strasse)	Eduard Buchholz
		R. W. Coomber		No. 37)	(TELEGRAMS, Surveyor)
		C. Cooper G. Murdoch T. Field	Rio de Janeir	(Address, Caixa 636)	Robert Vance (Telegrams, Register)
	Ship and Engineer Surveyors	L. G. Shallcross	*Rosario	(See Buenos Ayres.)	D. I
		C. J. Hudson J. E. Sellex	*Rotterdam		R. Leeuwenburg A. Schouwenaar
		R. Lee Annear, B.Sc. J. Houston W. Cowie		Ship and Engineer Surveyors (Office, Veerhaven, W.Z. 19b.)	F. N. Bernoski
		William Campbell	St. John, N.B.	Ship and Engineer Surveyor	
*NEWFOUNDLA	AND. (See St. John's, N.F.L.)	*St. John's,	Ship and Engineer Surveyor	T D11.
*Newport, Mon.	$Ship\ and\ Engineer\ Surveyors\ \Big\{$	R. F. Morton S. Townend	N.F.L.	(Office, Fisheries and Marine Department, Custom House)	J. Black (Telegrams, Surveyor)
	Ship Surveyor (Office, Bank Chambers)	R. Langlands			(TELEGRAMS, Kruse)
*Newport News, Va.	Ship and Engineer Surveyor (Office, 2711, Washington Avenue)		SanFrancisco, Cal.	Ship Surveyor Engineer Surveyor (Office, 454, California Street)	W H Storgart

LIST OF SURVEYORSHIPS (ALPHABETICALLY ARRANGED)—continued.

SEVILLE Ship and Engineer Surveyor of Cheromans, Prince) Shangand Engineer Surveyor of Schip and Engineer Surveyor of Schip and Engineer Surveyor of Schip and Engineer Surveyor of Forgings and Church Street) Ship and Engineer Surveyor of Forgings and Church Street of Ship and Engineer Surveyor of Schip and Engineer Surveyor of Cheromans, Prince of Cheromans, Prince of Schip and Engineer Surveyor of Cheromans, Comper of Schip and Engineer Surveyor of Cheromans, Comper of Cheromans, Comper of Schip and Engineer Surveyor of Cheromans, Comper of Cheromans, Comper of Schip and Engineer Surveyor of Cheromans, Comper of Cheromans, Compet of Cheromans, Comper of Cheromans, Comper of Cheromans, Comper of Cheromans, Compet of Cheromans, Compet of Cheromans, Compe	SEATTLE, WAS	H.Ship and Engineer Surveyor (Office, 503, Maynard Building, First Avenue, Corner Wash- ington Street)	*Sydney, Ship and Engineer Surveyor, R. Pollock N.S.W. (Office, 17, Bridge Street) (Telegrams, Miramar) Syra Ship and Engineer Surveyor Edward Eyssartier
*SHANGHAI Ship and Engineer Surveyor J. S. Cairns (Address, 13, Nanking Road) (Telebrams, Reptiler) *SHEFFIELD Ship and Engineer Surveyor J. C. Turpin Inspector of Forgings J. Pringle (Office, Orchard Chambers, Church Street) *SINGAPORE Ship and Engineer Surveyor (Office, 6a, Flint Street) *SURABAYA Ship and Engineer Surveyor (Office, 6a, Flint Street) *SOUTH- Ship and Engineer Surveyor (Office, 20, Canute Road) *SOUTH- AMPTON Office, 20, Canute Road) *Ship Surveyor	SEVILLE		TALCAHUANO (TELEGRAMS, Lyssartier)
*Sheffield Ship and Engineer Surveyor of Forgings J. Pringle (Office, Orchard Chambers, Church Street) *SINGAPORE Ship and Engineer Surveyor (Office, Orchard Chambers (Church Street)) *SOUTH—**SOUTH—**AMPTON** *SOUTH—**Ship and Engineer Surveyor Surveyor (Office, Orchard Engineer Surveyor (Office, Orchard Engineer Surveyor (Office, Orchard Engineer Surveyor (Office, Surveyor Surve	*Shanghai	Shin and Engineer Surveyor) J. S. Cairns	
*SUTH-AMPTON Coffice, 20, Canute Road) *STETTIN Ship and Engineer Surveyor (Office, 55, Fawcett Street) *SUNDERLAND *SUNDERLAND *SUNDERLAND *SUNDERLAND *SUNDERLAND *SWANSEA *SWANSEA *Ship and Engineer Surveyors (Office, 57, Fawcett Street) *SUNDERLAND *SWANSEA *Sing and Engineer Surveyors (Office, 10, Creating Surveyors (Office, 57, Fawcett Street) *SWANSEA *Ship and Engineer Surveyors (Office, 57, Fawcett Street) *SWANSEA *Sing and Engineer Surveyors (Office, 10, Creating Sunders) (Office, 57, Fawcett Street) *SWANSEA *SWANSEA *Sing and Engineer Surveyors (Office, 10, Creating Sunders) (Office, 10, Creating Surveyors (Office, 10, Creating Sunders) (CELEGRANS, Cooper) (Coffice, Via San Giorgio, No. 5) (Chice, Via San Giorgio, No. 5) (A. F. Smith (Caddress, Casilla, 934) VALPARAISO Ship and Engineer Surveyor (A. F. Smith (Catry, B.C. (Office, 42e, Winch Building, Hastings Street; P.O. Box 42) VERA CRUZ, (Office, 42e, Winch Building, Hastings Street; P.O. Box 42) (Office, 42e, Winch Building, MEXICO (Office, 42e, Winch Building, Mexico (Office, 42e, Winch Building, Mexico (Office, 42e, Winch Building,	**		TIMARU, N.Z James Tait
*SINGAPORE Ship and Engineer Surveyor (Office, 6a, Flint Street) (Telebrams, Comper) SOURABAYA Ship and Engineer Surveyor B. N. Powell (Telebrams, Fowell) *SOUTH- AMPTON (Office, 20, Canute Road) (M. Inst.C.E. H. Gilby Ship and Engineer Surveyor B. M. Inst.C.E. H. Gilby STETTIN Ship and Engineer Surveyor B. M. Ellicht, B.S.C., (Office, 20, Canute Road) (M. Inst.C.E. H. Gilby STETTIN Ship and Engineer Surveyor B. M. Herzberg (Office, Bollwerk 1.) (Office, Manufacture) (Office	*SHEFFIELD	Inspector of Forgings J. Pringle (Office, Orchard Chambers,	TORONTO, ONT. Ship and Engineer Surveyor (Residing at Barrie, Ont.) Hugh Calderwood
SOURABAYA Ship and Engineer Surveyors (Coffice, Via San Giorgio, No. 5) (Telegrams, Logargetyster, Sanglorgiot, No. 5) (Telegrams, Logargety No. 5) (Telegrams, Logargetyster, Sanglorgiot, No. 5) (Telegrams, Logargety No. 5) (Telegrams, Logargetyster, Sanglorgiot, No. 5) (Telegrams, Logargetyster, No. 6) (Telegrams, Lo			
*SOUTH- AMPTON Ship and Engineer Surveyors (Office, 20, Canute Road) *Ship and Engineer Surveyors (Office, 20, Canute Road) *Ship and Engineer Surveyors (Office, 20, Canute Road) *Ship and Engineer Surveyor (Telegrams, Herberg, Liogdawneepor) *Albert Isakson *Address, Drottgården, 14 & 16. *Ship and Engineer Surveyors *Albert Isakson *Address, Canute Road) *Telegrams, Register *Vancouver *Ship and Engineer Surveyor *Albert Isakson *Vera Cruz, *Ship and Engineer Surveyors *Albert Isakson *Vienna *Ship and Engineer Surveyor *Andrew Horn *Andrew Horn *Yokohama *Ship and Engineer Surveyor Office, 23, Water Street; P.O. Box 48) *Yokohama *Ship and Engineer Surveyor Office, 23, Water Street; P.O. Box 48) *Yokohama *Yokohama *Ship and Engineer Surveyor Office, 23, Water Street; P.O. Box 48) *Telegrams, Register Vancouver *Yokohama *Yokohama *Yokohama *Yokohama *Ship and Engineer Surveyor Office, 23, Water Street; P.O. Box 48) *Telegrams, Register Vancouver, B. A. F. Smith *Telegrams, Register Vancouver, B. C. *Telegrams, Register Vancouver, B. C. *Vera Cruz, *Vera Cruz, *Ship and Engineer Surveyor *Institute of the street of	*SINGAPORE		(Office, Via San Giorgio, No. 5)) (TELEGRAMS, Lloydregister,
*SUNDERLAND Ship Surveyors (Office, 55, Fawcett Street) *SUNDERLAND Ship Surveyors (Office, 55, Fawcett Street) *SUNDERLAND Ship and Engineer Surveyors (Office, 55, Fawcett Street) *SUNDERLAND Ship and Engineer Surveyors (Office, 55, Fawcett Street) *SUNDERLAND Ship and Engineer Surveyors (Office, 55, Fawcett Street) *SUNDERLAND Ship and Engineer Surveyors (Office, 55, Fawcett Street) *SUNDERLAND Ship surveyors (Office, 55, Fawcett Street) *Sunderland Engineer Surveyors (Office, 426, Winch Building, (Hastings Street; P.O. Box 642) *Vera Cruz, Ship and Engineer Surveyor (Office, Aval Military College) *Vera Cruz, Ship and Engineer Surveyor (Office, Aval Military College) *Vera Cruz, Ship and Engineer Surveyor (Telegrams, Heriberg, (Diffice, 426, Winch Building, (Hastings Street; P.O. Box 642) *Vera Cruz, Ship and Engineer Surveyor (Office, 426, Winch Building, (Hastings Street; P.O. Box 642) *Vera Cruz, Ship and Engineer Surveyor (Office, 426, Winch Building, (Hastings Street; P.O. Box 642) *Vera Cruz, Ship and Engineer Surveyor (Office, 426, Winch Building, (Hastings Street; P.O. Box 642) *Vera Cruz, Ship and Engineer Surveyor (Office, 426, Winch Building, (Hastings Street; P.O. Box 642) *Vera Cruz, Ship and Engineer S	Sourabaya		Trinidad J. B. Saunders
STETTIN Ship and Engineer Surveyor (Office, Bollwerk 1.) STOCKHOLM Ship and Engineer Surveyor (Office, Bollwerk 1.) STOCKHOLM Ship and Engineer Surveyor (Address, Drottgården, 14 & 16) STOCKHOLM Ship and Engineer Surveyor (Address, Drottgården, 14 & 16) Stadsgården) SUNDERLAND Ship Surveyors (Office, 55, Fawcett Street) Ship and Engineer Surveyor (Office, Address, Control of Ship and Engineer Surveyors) (Office, Bollwerk 1.) Ship and Engineer Surveyor (Office, Address, Drottgården, 14 & 16) F. R. Noton Principal Surveyors (Office, 55, Fawcett Street) Ship and Engineer Surveyors (Office, Address, Schelleingasse, 521x, Vienna, 1V) Waterford Waterford Waterford Waterford Ship and Engineer Surveyor Andrew Horn J. T. Findlay W. Butler L. C. Davis Insi ector of Forgings M. Robertson Ship and Engineer Surveyor (Office, 25, Winch Building, (Telegrams, Inamecon) Waterford Waterford Waterford Waterford Ship and Engineer Surveyor Andrew Horn Wellington, N.Z. *Yokohama Ship and Engineer Surveyor (Office, 25, Winch Building, (Telegrams, Inamecon) W. Koch M. Koch Upper Silesia (Address, Schelleingasse, 521x, Vienna, 1V) Waterford Ship and Engineer Surveyor Andrew Horn Wellington, N.Z. *Yokohama Ship and Engineer Surveyor A. S. Williamson (Office, 23, Water Street; P.O.) Telegrams, Register) Box 48 *Swansea Ship and Engineer Surveyor A. S. Williamson (Office, 23, Water Street; P.O.) Telegrams, Register) Waterford Water		(Office, 20, Canute Road) M.Inst.C.E.	(Address Cosillo 924) (TELEGRAMS, Smith,
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71, FENCHURCH STREET, LONDON.
1st January, 1912.

LLOYD'S REGISTER

OF

BRITISH AND FOREIGN SHIPPING.

RULES AND REGULATIONS.

- Section 1. The operations of the Societies of the two Register Books of Shipping formerly printed for the use of Merchants, Ship Owners, and Underwriters, having ceased in the year 1834, this Society was then established for the purpose of obtaining a faithful and accurate Classification of the Mercantile Shipping of the United Kingdom, and of the Foreign Vessels trading thereto, and for the government of which the following Rules and Regulations have been from time to time adopted.
- Section 2. A Register Book to be printed annually for the use of Subscribers, containing the names of the Ships with other useful information, and the Character assigned, where the vessels are classed by the Society; also the names, &c., of all Ships of 100 tons and upwards unclassed by this Society.
- Section 3. Each person subscribing the sum of Three Guineas per annum (or such other sum as the General Committee may fix) to be considered a Member of the Society, and entitled for his own use to one copy of the Register Book.
- Section 4. The subscription of Marine Insurance Companies, Public Companies or Public Establishments to be Six Guineas per annum, for a single copy of the Register Book and £3 3s. per annum for every additional copy supplied, unless the copies be periodically posted with type with additions and corrections throughout the year, in which case the subscription for each copy supplied will be Ten guineas per annum.
- Section 5. In the case of other Subscribers the subscription to be £3 3s. per annum for each copy, unless periodically posted with type with additions and corrections throughout the year, in which case the subscription will be £5 5s. per annum for each copy supplied.
- Section 6. For the convenience of Subscribers not resident in London, or whose Register Books are not posted, a Supplement, containing the additions to, and corrections made in, the Register Book, to be printed fortnightly, in such convenient form as to admit of its transmission by Post, so that such parties may be furnished, from time to time, with the latest and most complete information.

Section 7. The superintendence of the affairs of the Society to be under the direction of a Committee of Merchants, Shipowners, and Underwriters: (twenty-four to be elected in London and thirty-six at the principal Outports), and ten Shipbuilders and/or Engineers (to be elected as a temporary arrangement for two years by the General Committee). In addition, the Chairman, or, in his absence, the Deputy-Chairman of the Corporation of Lloyd's, and the Chairman, or, in his absence, the Deputy-Chairman of the General Shipowners' Society, for the time being, to be, ex-officio, Members of the Committee.

Any member (except an ex-officio member) who fails to attend any meetings of the Committee for a period of six continuous months, without leave of absence, shall cease to be a member, and his place shall be filled up in the usual way.

- Note.—Official intimation to be given in June of each year whether the Chairman or Deputy-Chairman of the Corporation of Lloyd's, and the Chairman or Deputy-Chairman of the General Shipowners' Society, are to be the *ex-officio* members for the ensuing twelve months.
- Section 8. The General Committee reserve the right of varying or withdrawing the representation of Outports, and of Shipbuilders and Engineers; also the representation of Shipbuilders, Engineers, Steel Makers, and Forgemasters on the Technical Sub-Committee hereinafter mentioned, as well as the mode of election of members.
- Section 9. Six of the Members elected in London, namely, two of each of the constituent parts of the Committee, to go out annually by rotation, but to be eligible to be re-elected. The vacancies so arising to be filled up by the election of two Underwriters and one Merchant by the Committee of Lloyd's, and two Shipowners and one Merchant by the Committee of the General Shipowners' Society.
- 2. Of the Members elected at the Outports twenty-two to retire at the end of *four* years, and six of the Members elected at Liverpool and the eight Members elected at Glasgow to retire annually. The retiring Members are eligible for re-election.
- Section 10. The Committee to appoint Sub-Committees of Classification, to be so regulated that each Member of the General Committee may, in rotation, take his turn of duty thereon throughout the year.
- Section 11. The Committee to appoint from their own body, annually, a Chairman and Deputy-Chairman; and also a Chairman or Chairmen of the Sub-Committees of Classification.
- Section 12. The Secretary, Clerks, and Servants of the Society, and the Surveyors, to be appointed by and be under the direction of the General Committee.
- Section 13. Special meetings to be convened by order of the Chairman, or Deputy-Chairman, or on the requisition of any three Members.
- Section 14. All elections and appointments to be made by ballot, excepting when in the election of Chairman, Deputy-Chairman, or Chairman or Chairmen of the Sub-Committees of Classification, only one person is nominated for each office.
- Section 15. No Member of the Committee to be permitted to be present on the decision of the classification of any ship of which he is the owner, or wherein he is directly, or indirectly interested.

- Section 16. 1. The Committee to be empowered to make such Bye-laws for their own government and proceedings as they may deem requisite, not being inconsistent with the original Rules and Regulations under which the Society was established; but no new Rule or Bye-law to be introduced, or any Rule or Bye-law altered, without special notice being given for that purpose at the Meeting of the Committee next preceding that at which such Motion is intended to be made; such notice to be inserted in the summons convening the meeting.
- 2. No new Rule, or alteration in any existing Rule materially affecting the classification of Ships, to be applied compulsorily to vessels of which the plans have been submitted and approved before the expiration of six months after the date when the change has been adopted.
- Section 17. 1. That fifteen representatives of Shipbuilders, Engineers, Steel Makers, and Forgemasters shall be admitted as members of the Technical Sub-Committee on all occasions when it is proposed to make alterations in the existing rules, or to frame new rules, for the construction of ships or machinery.
- 2. That twelve representatives of Shipbuilders and Engineers shall be elected by the following bodies, viz.:
 - (a) The Institution of Naval Architects, London;
 - (b) The North-East Coast Institution of Engineers and Shipbuilders, Newcastle-on-Tyne; and
- (c) The Institution of Engineers and Shipbuilders in Scotland, Glasgow, two shipbuilders and two engineers being elected by each body;

That two representatives of Steel Makers be elected by the Iron and Steel Institute, of whom one is to represent England and Wales, and the other Scotland; also

That one representative of Forgemasters be elected by the English and Scottish Forgemasters' Association.

- 3. That the representatives shall be elected for a term of two years, but in the event of any vacancy occurring before the expiration of this period a representative may be elected to fill the vacancy for the unexpired portion of the term.
- 4. That those only who are actually partners in firms, or managers of joint stock companies, engaged in Shipbuilding, Engineering, Steelmaking, or the Manufacture of Forgings, shall be eligible for election.
- 5. That the Chairman of the Committee of Lloyd's Register of British and Foreign Shipping, for the time being, or, in his absence, the Deputy-Chairman; or, failing him, some other member of the General Committee shall preside at the meetings of the Sub-Committee.
- 6. That the representatives of Shipbuilders, Engineers, Steel Makers, and Forgemasters shall have the same rights and powers as the other members of the Sub-Committee in speaking and voting at the meetings of the Sub-Committee at which they are entitled to be present.
- 7. That it shall be open to representatives of Shipbuilders, Engineers, Steel Makers, and Forgemasters to propose alterations in, or additions to, the Rules for the construction of ships or machinery; and that notice of all such proposals shall be sent in writing to the Secretary.

- 8. That meetings of the Sub-Committee shall be convened as often and at such times as may appear necessary to the General Committee, but there shall be at least two meetings in the year, though not necessarily one in each six months.
- 9. That every meeting shall be convened by notice from the Secretary at least one month before the date of meeting; that the meetings shall, whenever practicable, be arranged for Tuesday afternoons; that notice of matters proposed to be brought before the Sub-Committee by members shall be sent to the Secretary not less than fourteen days before the meeting, and the Secretary shall, as soon as possible thereafter, send to each member an agenda paper.
- 10. That the recommendations of the Sub-Committee shall be reported to the General Committee, who will refer them for consideration to a Special Meeting of the General Committee, as required by Section 16 of the Rules.
- 11. That in the event of eight representatives of Shipbuilders, Engineers, Steel Makers, and Forgemasters, actually voting together on any question, and nevertheless failing to obtain a majority of the Sub-Committee, it shall be open to them to present a minority report to the General Committee.
- 12. That the General Committee reserve to themselves the right of varying, adding to, or rescinding, at their discretion, any or all of the foregoing Rules.
- Section 18. All Reports of survey to be made in writing by the Surveyors according to the form prescribed, and submitted for the consideration of the General Committee, or of the Sub-Committees of Classification; but the character assigned by the latter to be subject to confirmation by the General Committee.
- Section 19. 1. The reports of the Surveyors, and all documents and proceedings relating to the classification of ships are to be carefully preserved and to be open to the inspection of the Owners, but no other person or persons are to have access to such documents except with the written consent of the Owners and under the direction of the Chairman, or Deputy-Chairman.
- 2. Copies of the original reports (if the ships be already classed, but not otherwise), so far as relates to the dimensions, scantlings, fastenings, and materials, in cases where the correctness of the reports in these particulars is certified by the builders, are granted on application.
- Section 20. Foreign ships, and ships built in the British possessions abroad where there is not a Surveyor (see also Section 52 of the Rules for Wood Vessels), to be surveyed on their arrival at a port to which a Surveyor has been appointed; but a due regard is to be had to the circumstance of such vessels having been exempted from supervision while building, and the Character to be assigned to them is to be regulated according to their intrinsic quality and from the best information the Committee can obtain.
- Section 21. In every case in which the Character assigned to a ship may be proposed, on survey, to be reduced, notice is to be given in writing to the Owner, Master, or Agent, with an intimation that if the reduction be objected to, the Committee will be ready to direct a special survey, on the Owner, Master, or Agent agreeing to pay the expenses attending the same, provided on the said survey there shall appear sufficient ground for the proposed reduction.

- Section 22. 1. When the Surveyors consider repairs to be requisite, they are respectfully to communicate the same in writing to the Owner, Master, or Agent, and if such repairs be not entered upon within a reasonable time, a corresponding report is to be made, as soon as possible, to the Committee for their decision thereon.
- 2. All repairs of Ships or Machinery required at Ports where there is a Surveyor to this Society, in order to their obtaining a Character in the Register Book, or to their retaining the Characters assigned to them therein, must be carried out under the inspection, and to the satisfaction of the Society's Surveyors. Ships or machinery repaired at Ports where there is no Surveyor to this Society must be surveyed by one of the Society's Surveyors at the earliest opportunity.
- Section 23. Parties considering the repairs suggested by the Surveyor to be unnecessary or unreasonable may appeal to the Committee, who will direct a special survey to be held; but should the opinion of the Surveyor be confirmed by the Committee, then the expense of such special survey is to be paid by the party appealing.
- Section 24. The Surveyors to the Society not to be permitted (without the especial sanction of the Committee) to receive any fee, gratuity, or reward whatsoever for their own use or benefit, for any service performed by them in their capacity of Surveyors to this Society, on pain of immediate dismissal.
- Section 25. The Surveyors will be directed to attend on Special Surveys of ships or machinery while building or under damage or repair, when required by Merchants, Shipowners, or Underwriters; the charge for which is to be regulated according to the nature and extent of the service performed. In all cases, the application for the assistance of the Surveyors must be made in writing addressed to the Secretary.
- Section 26. While the Committee use their best endeavours to ensure that the functions of the Society are properly executed, it is to be understood that neither the Committee nor the Society are under any circumstances whatever to be held responsible for any inaccuracy in any report or certificate issued by the Society or its Surveyors, or in any entry in the Register Book or other publication of the Society, or for any error of judgment, default, or negligence of the Surveyors, or other Officers or Agents of the Society.

FUNDS.

Section 27. The Funds to be under the authority and control of the Committee, and a statement of the Receipts and Expenditure to be annually printed for the information of the subscribers.

Section 28. The following Fees to be charged to the Owners of ships prior to their vessels being classed and registered in the book:—

CLASSING FEES.

For First Entry of Class in the Register Book.

For each Ship	under	200	tons			 	 	£1	0	0	
Ditto								2	0	0	
Ditto									0	0	
Ditto									0	0	
Ditto				.,	,,				0	0	

For First Entry of Notification "LMC" in the Register Book.

For each Ship	under	100	nominal HP	 	 	£1	0	0
Ditto	of	100	and under 300 HP.	 	 	2	0	0
Ditto	of	300	and above	 	 	3	0	0

SPECIAL SURVEYS.

Section 29. 1. For ships built under the special superintendence of the Surveyors (to entitle them to the distinctive mark +):—1s. per ton for the first 1,000 tons; 6d. per ton for every ton from 1,001 tons to 10,000 tons; 4d. per ton for every ton from 10,001 tons to 20,000 tons; and 2d. per ton for every ton beyond 20,000 tons. No fee to be less than £7 0s. 0d.

2. For engines and boilers built under the special superintendence of the Surveyors (to entitle them to the distinctive mark # in red):—three shillings per horse-power for the first 200 horse-power; one shilling for each horse-power from 201 to 1,000; 6d. for each horse-power from 1,001 to 3,000; and 3d. for each horse-power beyond 3,000. No fee to be less than £8 0s. 0d.

The following rule is to be used for determining the Nominal Horse power of Engines in regulating the fees for their survey, viz.:—

$$\begin{aligned} \text{NHP} &= \frac{\text{P} + 340}{1000} \left(\frac{\text{D}^2 \sqrt{\text{S}}}{100} + \frac{\text{H}}{15} \right) \text{ where the boiler pressure is below 160 lbs.} \\ &= \frac{\text{P} + 590}{1500} \left(\frac{\text{D}^2 \sqrt{\text{S}}}{100} + \frac{\text{H}}{15} \right) \text{ where the boiler pressure is 160 lbs. or above.} \end{aligned}$$

If the boilers are fitted with Forced Draught or Induced Draught appliances, then $\frac{H}{12}$ is to be taken instead of $\frac{H}{15}$.

where D = diameter of L.P. Cylinder in inches.

s = stroke in inches.

н = heating surface in square feet.

P = working pressure in lbs. per square inch.

The square feet of heating surface represented by H will comprise the surfaces of the tubes, of the back tube plate or plates, and of the furnace and combustion chamber plating down to the level of the fire bars.

- 3. For the survey and testing of each Donkey Boiler, a fee of two guineas will be charged.
- 4. No charge will be made for occasional or docking surveys, or for surveying repairs consequent on ordinary wear and tear, at ports in the United Kingdom.

For the survey of damage repairs essential to the continuation of class (whether a special damage report be required or not), for surveys with a view to the re-instatement of class, and for the survey of alterations in the structure of a vessel, a fee will be charged according to the nature and extent of the services performed.

For all surveys held at Foreign ports a fee will be chargeable according to the nature and extent of the services rendered.

SPECIAL PERIODICAL SURVEYS, Nos. 1, 2, and 3.

5.

For the special periodical surveys of Iron and Steel Vessels, when such surveys are held by the Society's exclusive Surveyors in the United Kingdom.

							,	S.S. 1	No.	1.	S.S.	No.	2.	S.S.	No. 3.
								£	S.		£	s.		£	8.
For	Vessels	under	150	tons g	ross			1	0		1	10		3	0
	,,	99	200	99				1	10		2	0		3	10
	,,	"	250	,,				2	0		2	10		4	0
	,,	,,	300	"				2	10		3	10		4	10
	,,	"	400	99				3	0		4	0		5	0
	"	"	800	"				3	10		4	10		6	0
	"	91	1,200	,,				4	0		5	0		7	0
	"	"	1,800	,,				4	10		5	10		. 8	0
	"	"	2,500	,,				5	0		6	0		9	0
	"	,,	3,500	"				5	10		6	10		. 10	0
	"	of	3,500	"	and	above		6	0		7	0	•••	. 10	0

SPECIAL PERIODICAL SURVEYS OF MACHINERY.

Held at the Special Surveys, Nos. 1, 2, and 3.

For each Ship	under	r 50	nominal HP		 	 	£2	0	0
,,	"	75	,,		 	 	2	10	0
,,	,,	100	"		 	 	3	10	0
"	"	150	"		 	 	4	0	0
"	"	200	"		 	 	4	10	0
"	"	300	"		 	 	5	0	0
"	of	300	**	and above	 	 	5	10	0

SPECIAL ANNUAL SURVEYS OF BOILERS.

To be held when and after the Boilers are six years old.

For each Ship having 1 boiler	 	£1	0	0
And for each additional boiler (including the donkey boiler)	 	0	10	0
But the fee in no case to be more than	 	3	0	0
For survey of donkey boiler of sailing vessels	 	1	0	0

- 6. For Surveys for Restoration, Continuation, or the character A in Red, and in cases where the caulking of ships is superintended and tested by the Surveyors a charge will be made according to the nature and extent of the services rendered.
- 7. All repairs which may be required on the Surveys above referred to, must be performed under the superintendence of the Society's Surveyors. (See also Section 22.)

MEM.—It is to be understood that in all cases where travelling expenses are incurred by the Surveyors in connection with the above services, they are to be defrayed by the parties interested in the same.

Section 30. The class of a vessel is liable to be withheld, or, if already granted, may be withdrawn or expunged from the Register Book in the case of non-payment of any fees or expenses chargeable on account of such vessel.

Section 31. Certificates of Classification, signed by the Chairman, Deputy-Chairman, or Chairman of the Sub-Committee of Classification, and countersigned by the Secretary, will be granted on application.

FREEBOARD.

Section 32. Fees for the Survey for, and assignment of, Freeboard.

									assed			class	
For	Vessels	under 300	tons g	ross .				 £1	1	0	£ 2	2	0
"	"	of 300	tons ar	nd under	1,000 to	ns gro	SS	 2	2	0	3	3	0
"	"	1,000	"	"	2,000	"		 3	3	0	5	5	0
"	"	2,000	,,	,,	3,000	"		 4	4	0	6	6	0
"	"	3,000	,,	,,	4,000	"		 5	5	0	8	. 8	.0
"	"	4,000	" and	d above				 6	6	0	10	10	0

Section 33. Rules for Steel Ships, 5s.; if for Wood Ships and Composite Ships, 5s.

GENERAL REGULATIONS

RELATING TO THE

CLASSIFICATION OF STEEL VESSELS.

1. Classification. 1. General.—Steel vessels built in accordance with the Society's Rules and Regulations, or with alternative arrangements equivalent thereto, will be classed 100A so long as they are found, upon careful annual and periodical survey, to be in a fit and efficient condition for the safe conveyance of dry and perishable cargoes. Vessels which do not fully satisfy the requirements for the 100A class may, if the Committee approve, be classed 90A.

Deviations from the Rules will be allowed, provided they are submitted to the Committee and considered by them to be equivalent to the requirements of the Rules. The Builder is required to obtain the Owners' sanction to such deviations, when the Committee deem it to be necessary.

2. Classes for Special Trades.—Vessels which are intended for special trades or purposes, and which are considered by the Committee to be fit for the contemplated employment, will be classed A without a numeral prefixed, provided all the details of the proposed scantlings and arrangements are submitted to the Committee and approved by them, and provided the Rules are otherwise complied with. To the class A, in such cases, will be affixed notations showing the particular trades or purposes for which the vessels are intended, thus:—A "For river purposes only"; A "For tug purposes"; A "Fishing Smack"; A "For channel purposes"; &c. In the cases of vessels intended for channel purposes, the particular channel will be defined thus: "Bristol Channel," "Irish Channel," "English Channel," "Newhaven—Dieppe," &c.

Vessels built in accordance with the "Rules for the construction of vessels intended to carry oil in bulk," or that may be classed by the Committee for that purpose, will have the following notation inserted under their class in the Register Book—"Carrying petroleum in bulk."

3. Vessels classed "with freeboard."—In the cases of awning or shelter deck steamers and channel steamers, and, in such other cases as the Committee may consider necessary, it is a condition of classification that a minimum freeboard shall be submitted to and approved by the Committee. In such cases the words "with freeboard" will be inserted under the character in the certificates of class and in the Register Book, and the freeboard must be marked on the vessel's sides in the manner shown by the diagrams printed at the end of the Rules.

Whenever the character of a vessel to which a minimum freeboard has been assigned as a condition of classification is for any reason withdrawn or expunged from the Register Book, the record of freeboard will be omitted on the next reprint of the Register Book, unless the character has been previously reinstated.

2. Submission of Plans.—In all cases in which it is intended to build vessels for classification in the Register Book, sketches of midship section and profile, with deck and other plans, showing the proposed dimensions, scantlings and arrangements, must in the first place be submitted by the builders through the local Surveyors, for the approval of the Committee.

3. Special Survey during Construction.—Vessels intended for classification in the Register Book are to be built under the Society's Special Survey, and vessels so built will be entitled to the distinctive mark # in the Register Book.

During the progress of construction, from the laying of the keel to the completion of a vessel, it is the duty of the Surveyors to examine the material and workmanship in order to ensure that the requirements of the Rules and the approved plans are satisfactorily carried out. The Surveyors are required to point out as early as possible anything that is objectionable, or that is not in accordance with the Rules or with the plans approved by the Committee for the particular vessel.

- 4. Vessels not built under Survey.—The requirements of the Committee in cases in which it may afterwards be desired that vessels which have not been built under the Society's survey should be assigned classes in the Register Book are set forth on page 58.
- 5. Engines and Boilers. 1. General.—The engines and boilers of steam vessels intended for classification, or already classed, in the Register Book, must be constructed under the Society's Special Survey. Appropriate records will be made in the Register Book in red ink, as follows, viz.:— \(\psi \text{LMC}\). 6,11 (Lloyd's Machinery Certificate, June, 1911); \(\psi \text{N.E.&B. 6,11}\) (New Engines and Boilers, June, 1911); \(\psi \text{N.E. 6,11}\); or \(\psi \text{N.B. 6,11}\). The requirements relating to the construction and survey of engines and boilers, are set forth on pages 71 to 84.
- 2. Novel Types, &c.—In cases in which the engines or boilers are of novel description, or in which experience has not sufficiently shown the safety of the principle or mode of application involved, the words "Machinery Experimental," or "Boiler Experimental," will be inserted under the class of the vessel in the Register Book; but if, in the opinion of the Committee, the engines or boilers are so far inefficient as to imperil the vessel's safety, no class will be assigned.
- 6. Equipment.—The figure 1 placed after the character assigned to a vessel, thus:— 100A1 will denote that the vessel's equipment is in good and efficient condition and otherwise in accordance with the requirements of the Rules. In cases in which the requirements of the Rules as to equipment have not been complied with, or in which the equipment is found to be insufficient in quantity or defective in quality, a line will be inserted in place of the figure 1, thus:— 100A—.
- 7. Date of Build.—In all cases of vessels built under special survey, the date of the completion of such survey will be taken as the date of build of the vessel, provided the survey be completed within six months of the date of launching for vessels under 10,000 tons gross, nine months for vessels of 10,000 tons and under 20,000 tons gross, and twelve months for vessels of 20,000 tons gross and upwards. When, however, the special survey is not completed within the period allowed, the date of build will be taken as six, nine, or twelve months after the date of launching, as the case may be.
- 8. Periodical Special Surveys. 1. General.—To entitle steel vessels to retain the characters assigned to them in the Register Book, they are required to be subjected to the Periodical Special Surveys, designated No. 1, No. 2, and No. 3 (the requirements for which are set forth at pages 13 to 18). These surveys severally become due, in the cases of vessels classed 100A or 90A at 4 years, 8 years, and 12 years respectively from the date of build, and subsequently at the expiration of like periods from the date recorded in the Register Book of the previous Special Survey No. 3. Should a vessel at any time be submitted to Special Survey No. 3 before being 12 years old, the Special Surveys

subsequently required will be Nos. 1, 2 and 3, at 4 years, 8 years, and 12 years, respectively from the date recorded in the Register Book of such Special Survey No. 3.

- 2. Vessels classed for special trades.—Vessels classed A for special purposes are required to be subjected to Special Surveys Nos. 1, 2, and 3 (the requirements for which are set forth at pages 13 to 18), at 3 years, 6 years, and 9 years, respectively, from the date of build, and at the expiration of like periods from the date recorded in the Register Book of the previous Special Survey No. 3.
- 3. Surveys held in anticipation.—In cases in which it may suit the convenience of the owners, the Special Surveys No. 1 and 2 may be held at any time within twelve months previous to the dates at which they severally become due, and the Special Survey No. 3 may be held at any time before the date at which it becomes due.
- 4. Period allowed for completion of surveys.—In cases in which it is inconvenient to owners to fulfil all the requirements of either of the Periodical Special Surveys at the prescribed time, part only of the survey need be then carried out, provided the remainder of the survey be completed within twelve months from the date at which it became due. When a special survey is only partly held, the Surveyors must give the owners or their agents written notice of the parts not surveyed, and report the facts to the Committee.
- 5. Record of Periodical Special Surveys in Register Book.—Vessels which have satisfactorily passed any of the Periodical Special Surveys will have notations made against their names in the Register Book indicating the survey and the date at which it was held thus:—ssNo.1-11, ssNo.2-11, ssNo.3-6,11, 2ndssNo.3-6,11. In cases in which Special Surveys are not completely carried out at one time, the date of Special Survey recorded in the Register Book will be the date of the survey at which the principal part of the requirements are complied with.
- 6. Engines and Boilers.—Particulars of the requirements for, and of the records made in the Register Book concerning the periodical survey of the engines and boilers of steam vessels, and of the donkey boilers of sailing vessels, are set forth at pages 83 and 84.
- 9. Occasional Surveys.—All vessels are subject to Annual, or Occasional, Surveys when practicable. The requirements in respect of such surveys are set forth at page 18.
- 10. Survey of Repairs.—All repairs of vessels, engines and boilers that may be required at ports where there is a Surveyor to the Society, in order that the vessels may retain their characters in the Register Book, must be carried out under the inspection and to the satisfaction of the Society's Surveyor. When such repairs are effected at a port where there is no Surveyor to this Society, the vessel must be surveyed by one of the Society's Surveyors at the earliest opportunity.

When the Surveyors consider repairs to be requisite, they are respectfully to communicate the same in writing to the owner, master, or agent; and, if such repairs be not entered upon within a reasonable time, a corresponding report is to be made, as soon as possible, to the Committee for their decision thereon.

11. Notice of Surveys.—Whilst the Society's Surveyors are required to attend for the purpose of holding surveys in their district, the duty of giving notice when the attendance of the Surveyors is required to carry out Periodical Special Surveys or to supervise repairs rests with the owners, master, or agents. If such notice is not given, and the requisite surveys are not carried out, the characters of vessels are liable to be expunged from the Register Book.

- 12. Appeal from Surveyor's recommendations. Interested parties considering the recommendations of the Society's Surveyors, as to the construction or repair of a vessel, to be in any case unnecessary or unreasonable, are entitled to appeal to the Committee, who will direct a special survey to be held; but should the opinion of the Surveyor be confirmed by the Committee, the expense of such special survey is to be paid by the party appealing.
- 13. Certificates of Class. 1. General. Certificates of first entry of classification, and certificates of character upon subsequent completed surveys on vessels, engines, and boilers, signed by the Chairman, the Deputy-Chairman, or the Chairman of the Sub-Committees of Classification, and countersigned by the Secretary, will be granted on application.
- 2. Provisional Certificates.—If the hull of a steamer has been built in accordance with the Rules, and a satisfactory report has been received from the Society's Surveyors, a provisional certificate will be issued, if desired, stating the class to which the vessel will be entitled when the engines and boilers have been fitted on board in accordance with the Rules, and the Committee's requirements otherwise complied with.
- 14. Reconsideration of Class.—If, upon survey of any vessel, material reduction is found to have taken place in the thickness of the plating and angles, the classification of the vessel will be reconsidered by the Committee. In every case in which the class assigned to a vessel is proposed to be reduced, notice is to be given in writing to the owner, master, or agent, with an intimation that if the reduction be objected to, the Committee will be ready to direct a special survey, if the owner, master, or agent agrees to pay the expenses attending the same, provided on the said special survey there shall appear sufficient ground for the proposed reduction.
- 15. Withdrawal of Class. 1. Non-compliance with Rules. When the Rules as regards surveys on the hull, engines or boilers of a steam vessel, or on the hull, masts, spars, or rigging of a sailing vessel have not been complied with, so that the vessel is not entitled to retain her class in the Register Book, the character will be expunged with a red line, under which the date of such withdrawal of class will be recorded.
- 2. Reported defects.—When it is found from reported defects in the hull, engines or boilers of a steam vessel, or in the hull, masts, spars, or rigging of a sailing vessel, that the vessel is not entitled to retain her class in the Register Book, the character will be expunged with a black line, under which the date of such withdrawal of class will be recorded.
- 3. Owner's request.—When the class of a vessel is withdrawn from the Register Book by the Committee in consequence of a request from the owner, the fact will be indicated by the insertion of three dots (...) in column 7 of the Register of steam vessels and column 8 of the Register of sailing vessels.
- 4. Infringement of conditions as to minimum freeboard.—If any vessel, to which a minimum freeboard has been assigned as a condition of classification, proceeds to sea with a less freeboard than that approved by the Committee, or if the freeboard mark is placed higher on the vessel's sides than the position assigned by the Committee, the vessel's class will be liable to be expunged from the Register Book.

PERIODICAL SPECIAL SURVEYS

OF

STEEL VESSELS.

SPECIAL SURVEY No. 1.

- 1. The vessel is to be placed on blocks of sufficient height in a dry dock or on a slipway; proper stages are to be made; and the holds and peaks are to be cleared for examination.
- 2. The limber boards and ceiling equal to not less than two strakes fore and aft on each side are to be removed, one such strake being taken from the bilges. Where the ceiling in the flat of bottom is fitted in hatches, the whole of the hatches and one strake of ceiling at the bilges are to be removed. At second and subsequent Special Surveys No. 1, additional ceiling is to be lifted at other parts of the vessel where deemed necessary by the Surveyor to enable him to satisfy himself as to the condition of the vessel.
- 3. The coal bunkers of steam vessels are to be cleared for examination, and ceiling is to be removed as in the holds. The bilges and limbers in the engine and boiler spaces are to be cleaned out, so as to allow of these parts being properly examined.
- 4. The framing and both surfaces of outside plating are to be exposed, and cleaned and coated where necessary.
- 5. In cases in which the inner surface of the bottom plating is coated with cement or asphalt, the removal of this coating may be dispensed with provided it be carefully inspected, tested by beating or chipping, and found sound and adhering satisfactorily to the steel.
- 6. If the vessel has a double bottom, the ceiling is to be removed therefrom and the efficiency of the tanks tested by a head of water to the height of the light water-line. Where peak tanks or other deep water ballast tanks are fitted, their watertightness is to be tested by a head of water not less than 8 feet above the crown of the tank. All water ballast tanks are to be cleaned out, to admit of their being properly examined inside.
- 7. When a deck originally required to be 4 inches thick is worn to 3 inches, $3\frac{1}{2}$ inches to $2\frac{3}{4}$ inches, 3 inches to $2\frac{1}{2}$ inches, it is to be renewed. If, however, such deck is found on survey to be in good condition, the case will, upon application, receive the consideration of the Committee.

- 8. The anchors are to be examined and placed in good condition, and when a vessel is undergoing Special Survey No. 1, after having passed Special Survey No. 3, the chain cables are also to be ranged for inspection; any length of chain cable which is found to be reduced in mean diameter at its most worn part to the extent indicated on the backs of Tables 30 and 31, is to be renewed; the windlass, if of wood, is to be unhung, where necessary, and its wood linings are to be sufficiently stripped for examination, unless this requirement was carried out at the previous Periodical Special Survey.
- 9. The masts, spars, and general equipment of steam and sailing vessels must be examined and found, or placed, in good and efficient condition. At second and subsequent Special Surveys No. 1, the mast and bowsprit wedging is to be removed, unless the plating of iron or steel masts and bowsprits is doubled in way of the same.
- 10. The hatches are to be examined in position at the hatchways, and, if defective, are to be renewed or made good.
- 11. The steam steering engine and its connections, the steering rods, chains, blocks, rudder quadrant, tillers, steering gear, windlass, pumps, sluice valves, watertight doors, and air and sounding pipes are to be carefully examined, and the condition of the same is to be stated on the Surveyor's report. The Surveyor must see that doubling plates are fitted under all sounding pipes.
- 12. Where holds are insulated for the purpose of carrying frozen or chilled meat, and the vessel in way of the insulation was examined by the Society's Surveyors at the time such insulation was fitted, it will be sufficient at the first Special Survey No. 1 if the limbers and hatches are removed and the vessel is examined in way of the same. At all subsequent Special Surveys No. 1, in addition to the above, sufficient lining is to be removed in each of the chambers to admit of the framing and plating being exposed to satisfy the Surveyor of their general condition, subject to such modifications as may be accepted by the Committee, upon application in each particular instance.
- 13. The engines and boilers of steam vessels and the donkey boilers of sailing vessels must be examined and favourably reported on by the Society's Engineer Surveyors. For Periodical Surveys of engines and boilers, see pages 83 and 84.

SPECIAL SURVEY No. 2.

- 1. The vessel is to be placed on blocks of sufficient height in a dry dock or on a slipway, proper stages are to be made; and the holds and peaks are to be cleared for examination.
- 2. The limber boards and ceiling equal to not less than three strakes fore and aft on each side are to be removed, one such strake being taken from the bilges. Where the ceiling in the flat of bottom is fitted in hatches, the whole of the hatches and one strake of ceiling at the bilges are to be removed. At second and subsequent Special Surveys No. 2, additional ceiling is to be lifted at other parts of the vessel where deemed necessary by the Surveyor to enable him to satisfy himself as to the condition of the vessel.
- 3. The coal bunkers of steam vessels are to be cleared for examination, and ceiling is to be removed as in the holds. The bilges and limbers in the engine and boiler spaces are to be cleaned out, so as to allow of these parts being properly examined.
- 4. The framing and both surfaces of outside plating are to be exposed, and cleaned and coated where necessary.

- 5. In cases in which the inner surface of the bottom plating is coated with cement or asphalt, the removal of this coating may be dispensed with provided it be carefully inspected, tested by beating or chipping, and found sound and adhering satisfactorily to the steel.
- 6. If the vessel has a double bottom, the ceiling is to be removed therefrom, and the efficiency of the tanks tested by a head of water to the height of the light water-line. Where peak tanks or other deep water ballast tanks are fitted, their watertightness is to be tested by a head of water not less than 8 feet above the crown of the tank. All water ballast tanks are to be cleaned out, to admit of their being properly examined inside.
- 7. When a deck originally required to be 4 inches thick is worn to 3 inches, $3\frac{1}{2}$ inches to $2\frac{3}{4}$ inches, 3 inches to $2\frac{1}{2}$ inches, it is to be renewed. If, however, such deck is found on survey to be in good condition, the case will, upon application, receive the consideration of the Committee.
- 8. The chain cables are to be ranged for inspection, and the anchors examined and put in good working condition; any length of chain cable which is found to be reduced in mean diameter at its most worn part to the extent indicated on the backs of Tables 30 and 31, is to be renewed. The windlass, if of wood, is to be unhung, where necessary, and its wood linings are to be sufficiently stripped for examination, unless this requirement was carried out at the previous Periodical Special Survey.
- 9. The masts, spars, and general equipment of steam and sailing vessels must be examined and found, or placed, in good and efficient condition. At second and subsequent Special Surveys No. 2, the mast and bowsprit wedging is to be removed, unless the plating of iron or steel masts and bowsprits is doubled in way of the same.
- 10. The hatches are to be examined in position at the hatchways, and, if defective, are to be renewed or made good.
- 11. The steam steering engine and its connections, the steering rods, chains, blocks, rudder quadrant, tillers, steering gear, windlass, pumps, sluice valves, water-tight doors, and air and sounding pipes are to be carefully examined, and the condition of the same is to be stated on the Surveyor's report. The Surveyor must see that doubling plates are fitted under all sounding pipes.
- 12. Where holds are insulated for the purpose of carrying frozen or chilled meat, and the vessel in way of the insulation was examined by the Society's Surveyors at the time such insulation was fitted, it will be sufficient at the first Special Survey No. 2 if the limbers and hatches are removed and the vessel is examined in way of the same. At all subsequent Special Surveys No. 2, in addition to the above, sufficient lining is to be removed in each of the chambers to admit of the framing and plating being exposed to satisfy the Surveyor of their general condition, subject to such modifications as may be accepted by the Committee upon application in each particular instance.
- 13. The engines and boilers of steam vessels and the donkey boilers of sailing vessels must be examined and favourably reported on by the Society's Engineer Surveyors. For periodical Surveys of engines and boilers, see pages 83 and 84.

SPECIAL SURVEY No. 3.

TO BE HELD BY TWO SURVEYORS, ONE AT LEAST TO BE AN OFFICER OF THE SOCIETY.

1. The vessel is to be placed on blocks of sufficient height in a dry dock or on a slipway; proper stages are to be made; and the holds and peaks are to be cleared for examination.

- 2. All close ceiling is to be removed, so that the flat of bottom may be thoroughly examined. The whole of the frames, stringers, hooks, floor-plates, keelsons, engine and boiler bearers, ends of beams, water-tight bulkheads, rivets and inner surfaces of the outside plating are to be exposed. Where side lights are fitted, the condition of the plating in way of the same is to be ascertained. In iron and steel steam trawlers and other fishing vessels in which close ceiling is fitted at the sides of the holds above the bilges, provided a strake of this close ceiling be removed at the upper turn of bilge and another at the upper part of the side of the vessel, right fore and aft of the holds on both sides, and the condition of the iron or steel work of the shell plating, frames, reverse frames, &c., is found to be satisfactory, the removal of the remainder of the close ceiling above the bilges may be dispensed with. Whenever the close ceiling of these vessels is renewed, the Surveyor should report upon the condition of the iron or steel work in way of same.
- 3. The coal bunkers of steam vessels are to be cleared for examination and all ceiling is to be removed as in the holds. The bilges and limbers in the engine and boiler spaces are to be cleaned out, so as to allow of these parts being properly examined.
- 4. All rust is to be cut or beaten off the steel and iron throughout the vessel. The planksheers and waterways, if of wood, are to be scraped bright. When the vessel is thus prepared, the Surveyors are to satisfy themselves thoroughly as to the condition of the plating. If the Surveyors deem it necessary, the thickness of the plating is to be ascertained by drilling holes in parts to be indicated by them, and in such cases a detailed statement of the thicknesses is to be included in the Surveyors' report. Any parts that are found defective, or materially less in substance than is required by the Rules, are to be removed and replaced with proper materials, equal in substance and quality to that used in the original construction of the vessel. All the scaled or chipped surfaces of the iron and steel are to be recoated. The planksheers, waterways, flat of decks and their fastenings, are also to be examined and made good where necessary. Where the deterioration in thickness is widespread, and it is not deemed advisable by the owner to renew the material, a detailed report is to be made by the Surveyors, and the class of the vessel will be reconsidered by the Committee.
- 5. In cases in which the inner surface of the bottom plating is coated with cement or asphalt, the removal of this coating may be dispensed with provided it be carefully inspected, tested by beating or chipping, and found sound, and adhering satisfactorily to the steel.
- 6. If the vessel has a double bottom, the ceiling is to be removed therefrom and the efficiency of the tanks tested by a head of water to the height of the light water-line. Where peak tanks or other deep water ballast tanks are fitted, their watertightness is to be tested by a head of water not less than 8 feet above the crown of the tank. All water ballast tanks are to be cleaned out, to admit of their being properly examined inside.
- 7. When a deck originally required to be 4 inches thick is worn to 3 inches, $3\frac{1}{2}$ inches to $2\frac{3}{4}$ inches, 3 inches to $2\frac{1}{2}$ inches, it is to be renewed. If, however, such deck is found on survey to be in good condition, the case will, upon application, receive the consideration of the Committee.
- 8. The chain cables are to be ranged for inspection, and the anchors examined and put in good working condition; any length of chain cable which is found to be reduced in mean diameter at its most worn part to the extent indicated on the backs of Tables 30 and 31, is to be renewed. The windlass, if of wood, is to be unhung, where necessary, and its wood linings are to be sufficiently stripped for examination, unless this requirement was carried out at the previous Periodical Special Survey.

- 9. The masts, spars, and general equipment of steam and sailing vessels must be examined and found, or placed, in good and efficient condition. All mast and bowsprit wedging is to be removed, whether the plating of iron or steel masts and bowsprits is doubled in way of the same or not. Iron or steel masts, bowsprits, and yards are to be carefully tested by hammering; and if the plates are considered by the Surveyors to be materially wasted at any part, the thickness is to be ascertained by drilling. In sailing vessels, the standing rigging is to be lifted and the service and parcelling stripped off the nips, bends, and splices for examination; if, however, the rigging has been recently lifted, particulars of the case are to be submitted for the consideration of the Committee. The bobstay pins, the deadeyes, and rigging screws to the whole of the standing rigging, also all bolts or pins and fittings, are to be carefully examined.
- 10. The hatches are to be examined in position at the hatchways, and, it defective, are to be renewed or made good.
- 11. The steam steering engine and its connections, the steering rods, chains, blocks, rudder quadrant, tillers, steering gear, windlass, pumps, sluice valves, watertight doors, and air and sounding pipes are to be carefully examined, and the condition of the same is to be stated on the Surveyors' report. The Surveyors must see that doubling plates are fitted under all sounding pipes.
- 12. Where holds are insulated for the purpose of carrying frozen or chilled meat, and the vessel in way of the insulation was examined by the Society's Surveyors at the time such insulation was fitted, the limbers and hatches are to be lifted, and enough lining is to be removed in each of the chambers to admit of the framing and plating being exposed to satisfy the Surveyors of the general condition of the same.
- 13. The engines and boilers of steam vessels and the donkey boilers of sailing vessels must be examined and favourably reported on by the Society's Engineer Surveyors. For Periodical Surveys of engines and boilers, see pages 83 and 84.

Second and subsequent Special Surveys No 3.—Additional Requirements.

- 1. The Surveyors are to ascertain whether the scantlings of the vessel are satisfactorily maintained in all parts.
- 2. In steamers, the inside of the bunkers and the parts in way of the boilers are to receive the Surveyors' particular attention, in view of the special liability of these parts to deterioration.
- 3. The outside plating is to be drilled at such parts as the Surveyors may consider necessary to satisfy themselves as to its thickness, the number of holes drilled on each side of the vessel being in no case less than three in each strake of plating not covered with cement. All paint as well as rust is to be entirely removed before the plates are gauged, and the actual thicknesses at all parts drilled are to be correctly ascertained and stated on a sketch which is to accompany the Surveyors' report.
- 4. The plating in way of cement in the bottom need not be drilled, provided the cement be found to be adhering satisfactorily to the plating, and the Surveyors consider drilling at this part unnecessary.
- 5. In cases in which a Second Special Survey No. 3 is held on a vessel before she is 24 years old, the drilling of outside plating referred to in paragraph 3 may be postponed until she reaches that age; but, until the requirements as to drilling have been fully complied with, the survey, in such cases, will be described in the Register Book as Special Survey No. 3.

- 6. In cases in which the requirements of the Second Special Survey No. 3 are fully complied with before a vessel is 24 years old, the fact will be noted in the Register Book. Such notation, however, will not exempt a vessel from compliance with the requirements of the survey as regards drilling when she is 24 years old, or at the first Special Survey held after that time, unless the drilling has been done at the previous Special Survey.
- 7. Where holds are insulated for the purpose of carrying frozen or chilled meat, the whole of the insulating lining is to be removed.

ANNUAL OR OCCASIONAL SURVEYS OF STEEL VESSELS.

At annual, or occasional, surveys vessels should be examined generally, as far as possible.

When a vessel is placed in dry dock or on a slipway the Society's Surveyors at the port are to avail themselves of the opportunity to examine the bottom of the vessel, and to examine the vessel throughout as far as practicable in order to satisfy themselves generally as to her condition.

Whenever the engines or boilers are taken out, the bearers, with the floor plates, keelsons, rivets, etc., under them, are to be surveyed; and whenever the bottom plating is to be cemented, a survey is to be held prior to the cement being laid. The masts and spars are to be subject to examination by the Surveyors when deemed necessary by them on other occasions besides Special Surveys.

The requirements for the survey of engines and boilers are set forth at pages 83 and 84.

RULES FOR THE BUILDING OF STEEL VESSELS.

Section 1. 1. When it is proposed to build ships of steel for classification in the Register Book, a sketch of midship section with longitudinal, deck, and other plans showing the details of the scantlings and arrangements, must in the first place be submitted through the local Surveyors for the approval of the Committee. Such vessels must be built under special survey to the plans approved and otherwise in accordance with the following Rules, subject to such modifications as may be deemed necessary by the Committee. All important plans should be submitted on tracing cloth.

Section 2. The measurements for regulating the Scantling Numbers are to be taken as follows (See Sketch on page 21):—

LENGTH.

1. The Length (L) to be measured from the fore part of the stem to the after part of the stern-post on the range of the upper deck beams, except in awning or shelter deck vessels, in which cases the length is to be measured on the range of the deck beams next below the awning or shelter deck.

In vessels where the stem forms a cutwater the length (\mathbb{L}) is to be measured from the place where the upper deck beam line would intersect the fore edge of stem if it were produced in the same direction as the part below the cutwater.

BREADTH.

2. The Breadth (B) is in all cases to be the greatest moulded breadth of the vessel.

DEPTH.

3. The Depth (D) is to be measured at the middle of length, from the top of keel to the top of beam at side of uppermost continuous deck, except in awning or shelter deck vessels, where it may be taken to the deck next below the awning or shelter deck, provided the height of 'tween decks does not exceed 8 feet. Where the height of 'tween decks exceeds 8 feet the (D) is to be measured from the top of keel to a point 8 feet below the awning or shelter deck.

In addition, a depth (d) is to be measured vertically at the middle of length, from top of ordinary floor at centre, or double bottom at side, to top of the beams of the lowest deck or tier of beams at side. By a "tier of beams" is meant a range of beams fitted either at every frame or at alternate frames; or widely spaced beams not more than 24 feet apart in conjunction with a broad hold stringer. (See Section 21 for size of hold stringer.)

SCANTLING NUMBERS.

4. The scantlings of the various parts of the vessel are to be determined by numbers obtained as follows:—

B + D is to be termed the Transverse Number.

 $L \times (B + D)$ is to be termed the Longitudinal Number.

(B + D) regulates the frame spacing and scantlings of floors. (See Tables 2, 3, 4, and 5.)

and

considered in association with (d) regulates the scantlings of frames, reversed frames and web frames. (See Tables 2, 3, and 5.) For the framing and number of side stringers in way of a raised quarter deck the depth (d) is to be measured amidships and increased by the height of the raised quarter deck.

 $L \times (B + D)$ regulates the scantlings of keel, stem, stern-post, side and bottom plating, double bottom, side stringers, keelsons, lower deck stringer plates, and lower deck plating. (See Tables 1, 6, 7, 8, and 17.)

and

considered in association with the proportions of the vessel, regulates the thicknesses of side plating and deck plating, of upper, awning or shelter decks and of long erections. (See Table 18.)

- (B) regulates the number of keelsons. (See Section 14.)
- (d) regulates the number of side stringers. (See Tables 2, 3, and 5.)

The length of amidship beams considered in association with the number of rows of pillars regulates the scantlings of beams. (See Tables 11, 12, and 13.)

5. In vessels of exceptional fineness of form, intended for passenger traffic, or to carry a limited amount of cargo with a fixed freeboard, a modification in the scantlings may be admitted, subject to all particulars being submitted by the Builders, and approved by the Committee, and to the deviations from the Rules being sanctioned by the Owner.

PROPORTIONS.

- 6. The depth used in obtaining the proportions of length to depth is to be measured, at the middle of the length, from top of keel to top of beam at side of upper deck, or awning or shelter deck, except in way of a "Long" bridge where the depth is to be taken to the bridge deck. Beyond the ends of a "Long" bridge, and throughout when there is a "Short" bridge, the depth for proportions is to be taken to the upper deck.
- 7. The longitudinal strengthenings in relation to the proportions of vessels are to be as shown in Table 18.
- 8. For all vessels exceeding 14 depths in length, plans showing the proposals for affording the vessels sufficient strength longitudinally must be submitted for the approval of the Committee, and all vessels having a length of $13\frac{1}{2}$ depths and above are to have a bridge extending over the midship half length of the vessel, or such special compensation for extreme proportions as may be required by the Committee.
- 9. In all cases where structural additions may be required for a certain portion of the length of a vessel, care should be taken to avoid any abrupt termination of the additional strength so obtained, by tapering the structural additions beyond these limits, and properly shifting their terminations.

Sketch Illustrating the Method of obtaining Scantling Numbers (as per Section 2).

Dimensions 380' 0" × 51' 0" × 28' 0" Moulded Depth to Upper Deck.

36' 0" ,, Awning or Shelter Deck, or Bridge Deck.

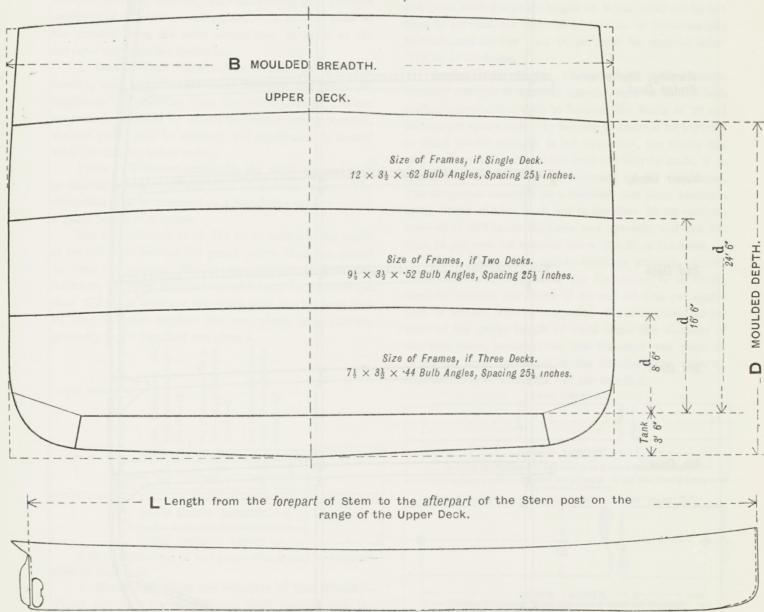
Transverse No. (B + D) and d.

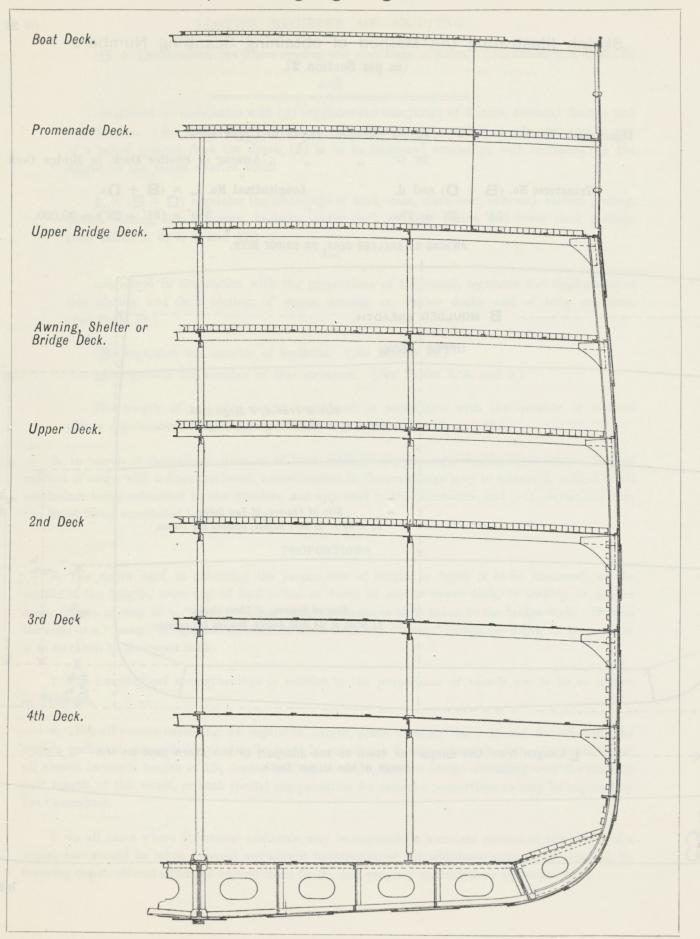
Longitudinal No. $L \times (B + D)$.

51' + 28' = 79.

 $380' \times (51' + 28') = 30,020.$

AWNING OR SHELTER DECK, OR BRIDGE DECK.





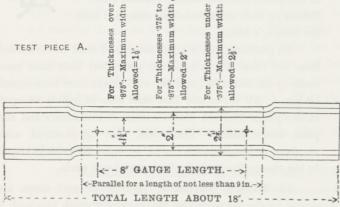
QUALITY AND TESTING OF SHIP STEEL.

Section 3. 1. Process of Manufacture.—Steel for Shipbuilding shall be made by the Open Hearth process, acid or basic.

- 2. Freedom from Defects.—The finished material shall be free from cracks, surface flaws, and lamination. It shall also have a workmanlike finish, and must not have been hammer-dressed.
- 3. Testing and Inspection.—The following tests and inspections shall be made at the place of manufacture prior to despatch; but, in the event of any of the material proving unsatisfactory in the course of being worked into vessels, such material shall be rejected, notwithstanding any previous certificate of satisfactory testing, and such further tests of the material from the same charge may be made as the Surveyor may consider desirable.
- 4. Tensile Test Pieces.—The tensile strength and ductility shall be determined from Standard test pieces cut lengthwise or crosswise from the rolled material. When material is annealed or otherwise treated before despatch, the test pieces shall be similarly and simultaneously treated with the material before testing.

Plates:—Wherever practicable the rolled surfaces shall be retained on two opposite sides of the test piece. The elongation shall be measured on a Standard test piece having a gauge length of 8 inches.

For material more than '875 in. in thickness the width of the test piece between the gauge points shall not exceed $1\frac{1}{2}$ ins.; for material '875 in. to '375 in. in thickness, inclusive, the width shall not exceed 2 ins.; for material less than '375 in. in thickness the width shall not be more than $2\frac{1}{2}$ ins. In other respects the test pieces shall conform generally to the Standard test piece A.



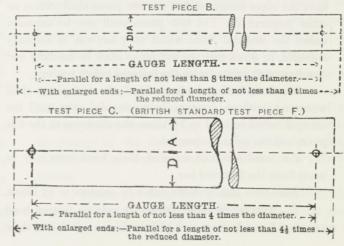
Any straightening of test pieces which may be required shall be done cold.

5. Mechanical Tests and Selection of Test Pieces.— Plates and bars for shipbuilding shall comply with the following mechanical tests. All test pieces shall be selected by the Surveyor and tested in his presence, and he shall satisfy himself that the conditions herein described are fulfilled.

6. Tensile Tests. Plates:—The tensile breaking strength of steel plates, determined from Standard test pieces, shall be between the limits of 28 and 32 tons per square inch. For plates specially intended for cold flanging and marked for identification, the tensile strength shall be between the limits of 26 and 30 tons per square inch. In the case of material for purposes in which tensile strength is not important, the tensile test may be dispensed with and the bend test only be made, if so specified by the builders and approved by the Committee. The elongation, measured on a Standard test piece having a gauge length of 8 ins., shall not be less than 20 per cent. for material of '375 in. in thickness and upwards, and not less than 16 per cent. for material below '375 in. in thickness.

Angles, Bulb Angles, Channels, etc.:—The tensile breaking strength of sectional material, such as angles, bulb angles, channels, etc., shall be between the limits of 28 and 33 tons per square inch. In the case of material for purposes in which tensile strength is not important, the tensile test may be dispensed with and the bend test only be made, if so specified by the builders and approved by the Committee. The elongation measured on a Standard test piece having a gauge length of 8 ins. shall not be less than 20 per cent. for material of '375 in. in thickness and upwards, and not less than 16 per cent. for material below '375 in. in thickness.

Rivet Bars:—The tensile breaking strength of steel rivet bars, when required by the Committee to be tested, shall be between the limits of 25 and 30 tons per square inch of section, with an elongation of not less than 25 per cent. of the gauge length of eight times the diameter of the test piece, measured on the Standard test piece B, or 30 per cent. measured on the Standard test piece C. The bars may be tested the full size as rolled.



When the Surveyor is in constant attendance at the Steel Works the following requirements are to be complied with:—

7. Number of Tensile Tests. Plates and Sectional Material:—One tensile test for plates or sectional material shall be taken from the finished material of each charge.

When the quantity of the material from one charge exceeds 25 tons, a second tensile test will be required; also additional tests shall be made for every variation in thickness of '15 of an inch in the plates or sectional bars from each charge.

Rivet Bars:—When required by the Committee to be tested, one tensile test shall be taken from each charge used for rivet bars; but when the weight of the bars, as rolled, from one charge exceeds 10 tons, an additional tensile test shall be made for each further 10 tons or portion thereof.

Should a tensile test piece break outside the middle half of its gauge length, and the elongation be less than that required by the Rules, the test may, at the Maker's option, be discarded and another test be made of the same plate or bar.

8. Bend Tests.—Cold Bends:—Test pieces shall be sheared lengthwise or crosswise from plates or bars, and shall not be less than $1\frac{1}{2}$ ins. wide, but for small bars the whole section may be used. For rivet bars bend tests are not required.

Temper Bends:—The test pieces shall be similar to those used for cold bend tests. For temper bend tests the samples shall be heated to a blood red and quenched in water at a temperature not exceeding 80 degrees Fahr. The colour shall be judged indoors in the shade.

In all cold bend tests, and in temper bend tests on samples 5 in. in thickness and above, the rough edge or arris caused by shearing may be removed by filing or grinding, and samples 1 in. in thickness and above may have the edges machined, but the test pieces shall receive no other preparation. The test pieces shall not be annealed unless the material from which they are cut is similarly annealed, in which case the test pieces shall be similarly and simultaneously treated with the material before testing.

For both cold and temper bends the test pieces shall withstand, without fracture, being doubled over until the internal radius is equal to $1\frac{1}{2}$ times the thickness of the test piece, and the sides are parallel.

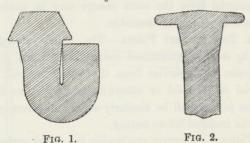
For small sectional material these bend tests may be made from the flattened bar.

Bend tests may be made either by pressure or by blows.

9. Number of Bend Tests.—A cold or temper bend test shall be made from each plate or bar as rolled, and these

tests shall be in about equal numbers from each charge; but a cold bend test shall be made from all plates which are specially marked for cold flanging.

- 10. Tests for Manufactured Rivets.—Rivets selected by the Surveyor from the bulk shall withstand the following tests:—
 - (a) The rivet shanks are to be bent cold, and hammered until the two parts of the shank touch in the manner shown in Fig. 1, without fracture on the outside of the bend.
 - (b) The rivet heads are to be flattened, while hot, in the manner shown in Fig. 2, without cracking at the edges. The heads are to be flattened until their diameter is $2\frac{1}{2}$ times the diameter of the shank.



- 11. Additional Tests before Rejection.—Should any of the test pieces first selected by the Surveyor not fulfil the test requirements, two further tests may be made from the same plate or bar, but should either of these fail, the plate or bar from which the test pieces were cut shall be rejected. In all such cases further tests shall be made before any material from the same charge can be accepted.
- 12. Branding.—Every plate and bar shall be clearly and distinctly marked by the Maker in two places with the Society's brand, thus:—indicating that the material has complied with the Society's tests.

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No plates or bars bearing this brand shall be forwarded from the Steel Works until the prescribed tests have been made by the Surveyor, and the mill sheets have been signed by him. All plates and bars shall also be legibly stamped in two places with the Maker's name or trade mark and the place where made. They shall also be stamped with numbers, or identification marks, by which they can be traced to the charge from which the material was made.

13. Maker's Certificate.—Before the mill sheets are signed by the Surveyor the Maker shall furnish him with a certificate guaranteeing that the material has been made by the Open Hearth process, and that it has been subjected to, and withstood satisfactorily, the tests above described, in the presence of the Surveyor. The following form of certificate

will be accepted if printed on each mill sheet with the name of the firm, and initialled by the Test House Manager:—

"We hereby certify that the material described below has been made by the Open Hearth process, and is that which has been satisfactorily tested in the presence of the Surveyor in accordance with the Rules of Lloyd's Register."

- 14. Rejected Material.—In the event of the material failing, in any case, to withstand the prescribed tests, the Surveyor shall see that the Society's brand stamped on the plates and bars by the Maker has been defaced by punch marks extending beyond the brand in the form of a cross, thus:—denoting that the material has been rejected.
- a system of marking the ingots, billets, slabs, plates, bars, etc., which will enable all finished material to be traced to the original charge, and the Surveyor must be given every facility for tracing all plates and bars to their respective charges, and for witnessing the required tests. When he is satisfied with the material and with the results of the tests, he shall be furnished with two copies of the advice notes of the material for his signature, one of which is to be forwarded by the Manufacturer to the Shipbuilder, and the other is to be forwarded by the Surveyors at the port where the vessel is to be built.
- 16. Steel not produced where Rolled.—Where steel is not produced in the works at which it is rolled, a certificate shall be supplied to the Surveyor stating the Open Hearth process by which it was made, the name of the Steel Maker who supplied it, also the numbers of the charges, for reference to the books of the Steel Maker. The number of the charge shall be marked on each ingot or billet for the purpose of identification, and the finished plates and bars shall also be legibly stamped in two places with the maker's name or trade mark and the place where made. They shall also be stamped with numbers or identification marks by which they can be traced to the charge from which the material was made.
- 17. Occasional Attendance at Steel Works.—When the Society's Surveyor is not in constant attendance at the Steel works, the Makers themselves may, with the written authority of the Society, comply with all the foregoing requirements, and shall furnish the Surveyor with a certificate to the effect that the Society's Rules as to the testing of steel have been complied with in the case of the material

submitted for approval. The Surveyor shall then make check tensile, cold, and temper bend tests from not less than one plate or bar in every batch of 50 or less number, provided the batch be all from one charge. If more than one charge is represented, each charge shall be tested. Additional tests shall also be made for every variation in thickness of '15 of an inch made from one charge. The test pieces shall be selected by the Surveyor from the plates or bars, and not from shearings previously detached from them, and when marked by the Surveyor for testing they shall be followed, as far as practicable, through the different stages of preparation until the tests are completed.

Should the tests be unsatisfactory, the whole of the material from the charge shall be rejected, and the Surveyor shall see that the Society's brand is satisfactorily defaced.

- 18. General.—Besides the foregoing tests, samples of all material may be subjected to additional tests at the discretion of the Surveyors.
- 19. In cases wherein it may be desired by Owners and Builders, consideration will be given by the Committee to proposals for the use of steel of other tenacity than is provided for in the foregoing Rules.

QUALITY AND TESTING OF STEEL CASTINGS.

- Section 4. 1. Process of Manufacture.—Steel for castings shall be made by the Open Hearth process, Acid or Basic, or by such other process as may be approved by the Committee.
- 2. Annealing.—All steel castings shall be thoroughly annealed in a properly constructed annealing furnace, which must permit of the whole casting being uniformly raised in temperature throughout its whole extent to the necessary intensity required for annealing purposes. The casting shall be allowed to cool down prior to removal from the annealing furnace; and if subsequently heated for any purpose it shall again be similarly annealed if required by the Surveyor.
- 3. Testing and Inspection.—The following tests and inspections shall be made, preferably at the place of manufacture prior to despatch, but in the event of any casting proving unsatisfactory in the course of preparation or fitting in the ship, such casting shall be rejected, notwithstanding any previous certificate of satisfactory testing.
- 4. Tensile and Bend Test pieces.—The tensile strength and ductility shall be determined from standard test pieces, which are to be prepared from sample pieces cast on the

casting. These sample pieces are not to be cut, or partially cut from the castings until the annealing of such castings has been completed, nor until they have been stamped by the Surveyor. The test pieces are to be stamped by the Surveyor after the annealing. All test pieces shall be selected by the Surveyor and tested in his presence, and he shall satisfy himself that the conditions herein described are fulfilled.

- 5. Number of Tests.—At least one tensile test and one cold bend test are to be taken from each casting. In castings of complex design, referred to in paragraph 12, at least two tensile and two cold bend tests are to be taken. Where a casting is made from more than one charge of steel, at least four tensile and four cold bend tests are to be taken from pieces cast as far apart as possible on the casting, some test pieces being taken from as near the top and others from as near the bottom of the casting as practicable.
- 6. Dimensions of Tensile Test pieces.—The tensile test pieces are to be turned so as to have a diameter of '564 inch with a gauge length of 2 inches, or a diameter of '798 inch with a gauge length of 3 inches, or a diameter of '977 inch with a gauge length of $3\frac{1}{2}$ inches.
- 7. Dimensions of Bend Test pieces.—The bend test pieces are to be machined to a rectangular section 1 inch wide by $\frac{3}{4}$ inch thick, with the edges rounded to a radius of $\frac{1}{16}$ th of an inch. They are to be bent over the thinner section. The bending may be performed either by pressure or blows.
- 8. Tensile Tests. The tensile breaking strength determined from test pieces of standard dimensions is to be between the limits of 26 and 35 tons per square inch, with an elongation of not less than 20 per cent. measured on the standard test piece.
- 9. Bend Tests.—The bend test pieces must withstand, without fracture, being bent cold through an angle of 120 degrees, the internal radius of the bend being not greater than one inch.
- 10. Additional Tests before Rejection.—Should either the tensile or bend test, or both, fail, and the Surveyor consider the fractured test piece or test pieces, or the results obtained therefrom, do not fairly represent the quality of the casting, a duplicate of the test or tests which failed shall be made if requested by the Maker. In such cases the quality of the casting shall be judged by the result of the duplicate test or tests and not by the original test or tests which failed.
- 11. Percussive Tests.—Stern frames cast in one piece to be let fall on hard ground (excavations being made to take bosses and other projections) after being raised through an

- angle of 45 degrees. Stern frames cast in more than one piece, rudders, steering quadrants, crossheads, tillers, etc., are to be dropped on hard ground from a height of from 7 to 10 feet according to the design, shape, and weight of the casting.
- 12. Castings of Complex Design.—Castings of complex design which would be liable to be deformed if submitted to the drop or percussive test, may have this test dispensed with provided two tensile and two cold bend tests be made upon pieces taken from positions as far apart as possible on each casting; one tensile and one bend test being taken from as near the top, and the others from as near the bottom of the casting as practicable.
- 13. Hammering Tests.—After being subjected to the percussive test, the casting in each case is to be subsequently slung up and well hammered with a sledge hammer not less in weight than 7 lbs., to satisfy the Surveyors that the casting is sound and without flaw. This hammering test is also to be applied to castings of complex design which may not have been submitted to a percussive test.
- 14. Drilling Tests. In the case of large steel castings the Surveyors are to supplement the foregoing tests by drilling small holes at such parts of the castings as experience shows cavities and contraction cracks are most likely to occur, and at positions which are to be agreed upon between the Surveyor and the Manufacturer, in order to determine the soundness or otherwise of the casting. These holes are afterwards to be tapped and properly filled up with screw plugs.
- 15. Branding.—Every casting after it has satisfactorily withstood the prescribed tests, shall be clearly and distinctly marked by the Society's Surveyor indicating that the casting has complied with the Society's requirements.

QUALITY AND TESTING OF INGOT STEEL FORGINGS.

Section 5. 1. Process of Manufacture.—Ingot steel for forgings shall be made by the Open Hearth process, Acid or Basic, or by such other process as may be approved by the Committee.

The forgings must be sound, they are to be made from sound ingots, and must be gradually and uniformly forged. The sectional area of the body of the forging (as forged) shall not exceed one-fifth of the sectional area of the original ingot, and no part of the forging (as forged) shall have more than two-thirds of the sectional area of the original ingot.

2. Annealing.—All important ingot steel forgings shall be thoroughly annealed in a properly constructed annealing furnace, which must permit of the whole forging being

uniformly raised in temperature throughout its whole extent to the necessary intensity required for annealing purposes. If the forging be subsequently heated for any further forging it shall again be similarly annealed, if required by the Surveyor.

- 3. Testing and Inspection. The following tests and inspections shall be made, preferably at the place of manufacture prior to despatch, but in the event of any forging proving unsatisfactory in the course of preparation, or fitting in the ship, such forging shall be rejected notwithstanding any previous certificate of satisfactory testing.
- 4. Tensile and Bend Test Pieces. The tensile strength and ductility shall be determined from standard test pieces, which are to be prepared from sample pieces cut lengthwise from the forging, from a part of not less sectional dimensions than the body of the forging. Such standard test pieces shall be machined from the sample pieces without forging down, and the sample pieces shall not be detached from the forging until the annealing of such forging has been completed. The test pieces are to be stamped by the Surveyor after the annealing. All test pieces shall be selected by the Surveyor and tested in his presence, and he shall satisfy himself that the conditions herein described are fulfilled.
- 5. Number of Tests.—At least one tensile and one cold bend test are to be taken from each forging. Where a number of articles are cut from one forging, one tensile and one cold bend test from this whole forging will be sufficient.
- 6. Dimensions of Tensile Test Pieces.—The tensile test pieces are to be turned so as to have a diameter of .564 inch with a gauge length of 2 inches, or a diameter of .798 inch with a gauge length of 3 inches, or a diameter of .977 inch with a gauge length of .977 inch with a gauge length of .977 inches.
- 7. Dimensions of Bend Test Pieces.—The bend test pieces are to be machined to a rectangular section 1 inch wide by $\frac{3}{4}$ inch thick, with the edges rounded to a radius of $\frac{1}{16}$ th of an inch. They are to be bent over the thinner section. The bending may be performed either by pressure or by blows.
- 8. Tensile Tests. The tensile breaking strength determined from test pieces of standard dimensions is to be between the limits of 28 and 32 tons per square inch, with an elongation on the standard test piece of not less than 29 per cent. for 28 ton steel, and 25 per cent. for 32 ton steel, and in no case must the sum of the tensile breaking strength and corresponding elongation be less than 57.

- 9. Bend Tests.—The bend test pieces must withstand without fracture being bent cold through an angle of 180 degrees, the internal radius of the bend being not greater than ¼ inch.
- 10. Additional Tests before Rejection.—Should either the tensile or bend test, or both, fail, and the Surveyor consider the fractured test piece or test pieces, or the results obtained therefrom, do not fairly represent the quality of the forging, a duplicate of the test or tests which failed shall be made if requested by the Maker. In such cases the quality of the forging shall be judged by the result of the duplicate test or tests and not by the original test or tests which failed.
- 11. Branding.—Every forging, after it has satisfactorily withstood the prescribed tests, shall be clearly and distinctly marked by the Society's Surveyor indicating that the forging has complied with the Society's requirements.
- 12. General.—The requirements as to annealing and testing are intended to apply to rudder heads and main pieces of rudder upon which arms are shrunk. They are not intended to apply to small forgings which during their last stage of manufacture are uniformly heated throughout.

(For List of Steel Manufacturers, see pages 99 to 108.)

STANDARD SECTIONS.

Section 6. The Sections of steel materials given in the following Rules are, with few exceptions, Standard Sections (see pages 109 to 113), and the thicknesses given in the Tables for the several Sections are the thicknesses of their webs.

IRON WHERE USED INSTEAD OF STEEL.

Section 7. The rivets, keel, stem, stern-frame, rudder, pillars and lining pieces, also the floors, girders and top plating of double bottom in boiler space may be of iron of the sizes given by the Rules. Deck plating and ordinary floors, also the floors, girders, and top plating of double bottoms in holds, coal bunker, and other bulkheads, shaft tunnels, casings round engines, hatchway coamings, bulwarks and deck houses may be of iron 10 per cent. in excess of the thicknesses in steel where scantlings for the same are provided for in the Rules. No other parts of the vessel are to be of iron without the special sanction of the Committee. Iron where used is to be of good malleable quality, and subjected to tests in the shipyard when considered necessary by the Surveyor.

WORKMANSHIP.

- Section 8 1. The Workmanship to be well executed, and submitted to the closest inspection, and amended where necessary before coating or painting.
- 2. It is recommended that the black oxide or "mill-scale" be removed from the surfaces before coating or painting, which should be delayed as long as practicable.
- 3. Experience has shown that, as regards durability, it is highly desirable to place steel vessels in dry dock within a reasonably short time after being launched, for the purpose of cleaning and re-coating the bottom.
- 4. It is recommended that when plates are one inch and above in thickness the edges, as well as the butts, be planed before the rivet holes are punched.

KEEL, STEM, STERN AND PROPELLER POSTS.

Section 9. 1. The keel, stem, stern, and propeller posts are to be either scarphed or welded together, and to be in size according to Table 1; if scarphed, the length of scarphs to be nine times the thickness given in the Table; and the rivet-holes required in the thin ends of them are to be drilled after the scarphs are fitted.

Where stern-frames are in more than one piece, the length of the scarphs should not be less than three times the width of the stern-posts, and the breadth one and a half times the width of the stern-posts, secured by not less than four rows of rivets.

- 2. Where Flat Plate Keels are adopted, their breadth and thickness are to be as given in Table 17, and where such keels are used, intercostal keelson plates, or vertical centreplates, must be fitted close down on the keel-plate, and connected to it by double angles of the dimensions given in Table 6, riveted all fore and aft to the keel-plate and keelson. For flat keel angles in double bottoms see Table 8.
- 3. The stem at its lower part is to be the same moulding as the keel, and attached to it by a scarph of the same length as the keel scarph; it may be gradually reduced from the height of the load-line to its head, where it may be three-fourths of the sectional area given in Table 1.
- 4. The lower portion of the stern-post forming part of the keel in sailing vessels, paddle steamers, and twin screw steamers having no aperture for propeller, is to extend sufficiently forward for the after end of its scarph to be at least once and a half the frame space forward of the stern-post, and the stern-post may be reduced from the lower part of the rudder trunk to its head where it may be three-fourths of the sectional area given in Table 1.

- 5. The lower portion of the stern-frame adjoining the keel in single screw vessels is to be tapered fairly into the keel, and to extend sufficiently forward for the after end of its scarph to be at least twice and a half the frame space forward of the propeller-post; the rudder-post may be reduced from the lower part of the rudder trunk to its head, where it may be of the size given for stems in Table 1.
- 6. Connection to Transom-plate.—The stern-post is to be extended sufficiently above the counter to be connected to the whole depth of the transom-plate by two vertical angles of the thickness of the transom-plate, which is to be fitted close against the stern-post. The transom-plate is to be of the thickness of the bottom plating at ends, and its depth not less than six times the thickness of "stern-frames with apertures." In screw steamers whose longitudinal number is 16,000 and above the foremost or propeller post should extend sufficiently above the arch of the stern-frame to be efficiently connected to plating on the beams, and to a deep transom-plate.
- 7. In single screw steamers above 350 ft. in length the after lengths of shell plating are to be connected to the portion of the stern-frame below the boss with three rows of rivets.
- 8. Rudder-braces or gudgeons are to be forged on the stern-post, and spaced as given in Table 24. The upper gudgeon should be as near as practicable to the rudder trunk. The gudgeons are not to be less in depth than seven-tenths the diameter of the rudder head, and the thickness one-half the diameter of the pintles.
- 9. When **cast steel stern-frames** are fitted they are to be tested as described in **Section 4**. Sketches of the proposed castings are to be submitted for the approval of the Committee.

RUDDERS.

Section 10. 1. For the diameters of rudder heads see Table 22.

- 2. For the scantlings of rudders, coupling bolts, quadrants, tillers, and steering chains, see Tables 23, 24 and 25.
- 3. Forged rudder heads, frames, arms, pintles, gudgeons and crossheads, and tillers are to be of the best hammered iron or steel. For quality and testing of Ingot Steel Forgings, see Section 5.
- 4. When cast steel rudders, steering quadrants, cross-heads, tillers, etc., are fitted they are to be tested as described in Section 4.

5. Couplings.—Where rudder heads are coupled the dimensions of the bolts and flanges or palms should not be less than required by Table 23, and the width of the material outside the bolt holes should not be less than two-thirds the diameter of the bolts. The nuts are to be in proportion to the size of the bolts, and locking plates, split pins, or other efficient means are to be adopted to prevent them from turning. A key or feather is to be fitted in horizontal and vertical couplings. The thickness of the tips of the palms of scarphed couplings is to be 13 of the diameter of the head. (See Sketches on page 115.)

Where the form of the coupling is modified from that contemplated by the Tables the strength is to be equivalent to that required by the Rules.

- 6. Pintles.—The pintles are to be spaced as given in Table 24, and the top pintle should be as near as practicable to the rudder trunk. The pintles should be at least the full length of the gudgeons, and it is recommended they be made independent of the frame.
- 7. Double Plate Rudders.—The frame and main piece of double plate rudders must be efficiently forged and stayed at intervals corresponding with the pintles. The main piece is to have a straight taper from below the top pintle to the heel where it is to be of the size required by Table 24. The sectional area at the top pintle is to be not less than that of the rudder head.
- 8. Single Plate Rudders.—The main piece of single plate rudders is to have a straight taper from below the top pintle to the heel where it is to be of the size required by Table 24. The sectional area at the top pintle is to be not less than that of the rudder head. The arms to be fitted alternately on opposite sides of the plate. Fillets to arms forged or cast on the main piece are not to have a less radius than one-fifth the distance between the arms. Where arms are shrunk upon and keyed to the main piece, the latter is to be increased in diameter in way of each arm to admit of an efficient key-way being cut.
- Rivets.—The rivet holes in rudder plates and arms are to be countersunk and the rivets are to have full heads and points.

FRAMES AND REVERSED FRAMES.

FRAMES.

Section 11. 1. The frames to be of the dimensions set forth in Tables 2, 3 and 5, and to extend from the keel to

the gunwale. They are to fit closely to the upper edge of the keel; and the after frames should be sufficiently apart transversely to admit of sound riveting and workmanship. At the extreme ends of the vessel the lower parts of the frames opposite to each other are to be lapped and riveted together. In raised quarter-decks, bridges, poops, or forecastles, the frames are to extend to their deck stringers respectively.

- 2. Heel Bars.—When the frames are butted on the keel they are to have not less than 3 feet lengths of corresponding angle bars, fitted back to back, to cover and support the butts and be attached to the plating for at least three-fourths the vessel's length amidships. Similar pieces of angle bar are to be fitted if the frames are butted elsewhere.
- 3. The rivet holes to be punched from the faying surfaces of the frames, and they are not to be punched at the turn of the bilge until the frames are bent to the required shape; the holes in the way of the lands of the plating are to be drilled or "beared" after the frames are faired in place, and the plate edges lined off.
- 4. Spacing.—The spacing of the frames from centre to centre to range from 20 to 33 inches, according to the size of the vessel, and to be as required by Tables 2, 3 and 5. The spacing amidships should not be exceeded around the stern of the vessel at the knuckle. In no case is the frame spacing to exceed 27 inches between the collision bulkhead and one-fifth the vessel's length from forward unless the frames are doubled to the height of the lowest tier of beams, and in the peaks the frame spacing is not to exceed 24 inches.

When a spacing of frames greater than that provided for in the Tables is adopted, the transverse framing, floors, inner bottom, beams, outside plating and deck plating, are to be proportionately increased.

5. When the height between deck stringers at the sides exceeds 8 feet at any part, additional transverse strength at such part must be submitted for approval. Where the frames are formed of frames and reversed frames, bulb angles, or channel bars without reversed frames, and the beams of the lowest tier are widely spaced, the height between the widely spaced beams and the deck above is not to exceed the depth for framing (d). Where, however, this height exceeds 9 feet, a side stringer, of the same scantlings as required to be fitted below is to be fitted midway between the widely spaced beams and the deck above, or other equivalent strengthening is to be introduced.

REVERSED ANGLES ON FRAMES.

- 6. Reversed angles on floors and frames to be in size as per Tables 2, 3 and 5.
- 7. Height of Reversed frames.—Where one tier of beams, only, is fitted and the depth (d) is 7 feet and under 9 feet, the reversed frames are all to extend to the upper turn of bilge.

When the depth (d) is 9 feet and under 11 feet, the reversed frames are to extend to upper turn of bilge and side stringer alternately.

When the depth (d) is 11 feet and under 13 feet, they are to extend to side stringer and upper deck stringer plate alternately.

When the depth (d) is 13 feet and under 27 feet, all the reversed frames are to extend to the upper deck stringer plate.

8. Where more than one tier of beams are fitted in steamers, and the height of 'tween decks does not exceed 8 feet the reversed frames are to extend to the upper deck stringer plate and deck stringer plate next below alternately.

Where the height of 'tween decks exceeds 8 feet, or where an awning or shelter deck or long bridge is fitted, the framing in the 'tween decks or the height to which the reversed frames should extend will be specially considered.

- 9. When the framing consists of channel bars with reversed frames, the latter are to extend to the lower edge of the beams at the lowest deck.
- 10. Where the beams in the lowest tier are widely spaced, the reversed frames are to extend at least to the deck above on all frames.
- Where the frames and reversed frames are connected with $\frac{5}{8}$ inch rivets the overlap of frame upon reversed frame is to be not less than $2\frac{1}{4}$ inches. Where $\frac{3}{4}$ inch rivets are used the overlap is to be not less than 3 inches, and where $\frac{7}{8}$ inch rivets are used the overlap is to be not less than $3\frac{1}{9}$ inches.
- 12. Double reversed angles are to be fitted on every floor, extending from bilge to bilge in the engine and boiler spaces of steam vessels; and where the longitudinal number is 11,000 or above, they are to extend sufficiently high to admit of the stringer at upper part of bilge being connected to them.

Short double reversed angles are to be fitted on all floors in the way of the keelsons, connected by not less than three rivets to the floor.

- 13. Additional Reversed Frames and Stringers.—In vessels where the longitudinal number is 15,000 and above, reversed angles should be fitted to every frame to the height of the upper deck, abaft the after peak bulkhead. Where such vessels have broad flat counters, a double angle stringer should be fitted to the framing in the 'tween decks for a reasonable length, connected by plate knees to the transom plate; or other additional strengthening applied, as the Surveyors may deem necessary.
- 14. In top-gallant forecastle of vessels whose longitudinal number is 14,000 and above, the alternate reversed frames are to extend to the forecastle deck, or other efficient means of strengthening the forecastle may be adopted, if approved by the Committee.

FLOOR-PLATES.

- Section 12. 1. The floor-plates to be in size at the middle line according to Table 4, excepting in the engine space in steam vessels, where they must be '04 of an inch thicker, and in the boiler space '10 of an inch thicker.
- 2. The floor-plates are to be moulded not less than one-half their midship depth at a distance of three-quarters the half breadth of the vessel set out from the middle line on the run of the frame, and not less at their extreme ends than the moulding of the frames; and they are to extend in a fair curve well up the bilges, in no case terminating lower at the outside of the frame than a perpendicular height above the top of keel of twice the midship depth of the floor as fitted. In vessels of unusually fine or full form the moulding is to be modified to the approval of the Committee.

The ends of the floors to maintain the height prescribed for one quarter of the vessel's length amidships. They may then be gradually lowered forward and aft until the upper edges of the floor-plates are level (this place to be determined by the form of the vessel), from which to the ends they are to be gradually increased in depth, so as to efficiently connect the sides.

3. A floor-plate to be fitted and riveted to every frame, and to be extended across the middle line, except where a vertical centre-plate is adopted, in which case the floor-plates are to be efficiently connected to it on each side by double

vertical angles of the thickness of the centre plate and with flanges not less than $2\frac{1}{2}$ inches for $\frac{5}{8}$ inch rivets, $\frac{3}{4}$ inch rivets, and $3\frac{1}{2}$ inches for $\frac{7}{8}$ inch rivets.

- 4. When in two lengths.—When floors are made in two lengths, the butts are to be riveted in accordance with the requirements of Table 21.
- 5. Floor-plates to which the bulkheads are attached must be deeper than the adjacent floor-plates, to admit of the bulkheads being riveted to them above the reversed angle bars.
- 6. In the after peak of steam vessels the floors are to extend well above the stern tube, and in vessels of full form where the extension of the floor-plate may not be practicable, broad cross tie-plates are to be fitted above the stern tube, stiffened with angles or flanged on both upper and lower edges. Stringer plates are also to be fitted at this part connected to the outside plating. The floors and cross-tie-plates in the after peak are to be connected to the frame angles with rivets spaced not more than five diameters apart.
- 7. Watercourses are to be formed above the frames through all the floor-plates on each side of the middle line, also at the lower turn of the bilges in vessels of full form, as well as through the vertical centre-plate, and intercostal keelsons, when such keelsons are adopted, so as to allow water to reach the pumps freely.
- 8. Transom-plates are to be fitted and connected to the frames, and to the stern-post, so as to efficiently support the counter. (See Section 9, paragraph 6.)

WEB FRAMES.

Section 13. 1. Web Frames, six frame spaces apart, in conjunction with side stringers in hold and intermediate transverse frames, may be fitted, if arranged in accordance with Table 5 and with the conditions specified below (See Sketches on pages 117 to 119):—

The depth (d) for regulating the scantlings of web frames, and the number of the side stringers required to be fitted, is to be taken from the top of the floors to the top of the beams of the lowest laid deck at side.

2. Face angles of the size given in Table 5 are to be riveted on the inner edge of the web frames and side stringers.

3. The double angles connecting the stringers to the web frames and the angles connecting the stringers and web frames to the outside plating are to be of the thickness of the web frames and with flanges—

4 inches × 4 inches for 1-inch rivets.

$$3\frac{1}{2}$$
 ,, $\times 3\frac{1}{2}$,, $\frac{7}{8}$,, 3 ,, $\times 3$,, $\frac{3}{4}$,,

Where the depth of web frame is 24 inches or above, the web frames are to be attached to the outside plating by double angles or by equivalent single angles double riveted. Where the transverse number is 111 or above, the stringer plates are to be attached to the outside plating with double angles for a length of three frame spaces on each side of the bulkheads.

- 4. Butt straps of the form shown by Sketches on pages 117 to 119, are to be fitted at the junction of web frames and side stringers, and are to be of the scantlings given in Table 5.
- 5. The deck beams are to be attached to the web frames at their head by bracket knees of the thickness of the web frames flanged on their inner edge. The breadth and depth of these knees are to be equal to the depth of the web frame, and they are to be measured from the lower edge of the beam and the inner edge of the web frame. The knees are to be double riveted in each arm.
- 6. The side stringers are to be supported by a bracket knee plate of the same thickness as the stringers fitted midway between the web frames when the depth of web frame is 16 inches and under 18 inches, and where this depth is 18 inches and above, the brackets are to be fitted to alternate frames.
- 7. The length of frame extending above a web frame is to be of the same strength as the intermediate frames.
- 8. In single deck vessels framed with web frames all the reversed frames are to extend to the upper deck striger plate.
- 9. Where more than one tier of beams are fitted in steamers having web frames and the height of 'tween decks does not exceed 8 feet the reversed frames are to extend to the upper deck stringer plate and beam stringer plate below, alternately. Where the height of 'tween decks in such vessels exceeds 8 feet or where a long bridge, awning or shelter deck is fitted, the height to which the reversed frames should extend or the framing in the 'tween decks will be specially considered.

10. The distance between stringers or between the lowest stringer and top of floors at centre in way of single bottoms, and top of margin plate in way of double bottoms, is not to exceed 8 feet at any part of the vessel.

KEELSONS.

- Section 14. 1. The scantlings and arrangements of keelsons are to be as required by Table 6 and shown by Sketches on pages 120 to 122.
- 2. When keelsons are formed of vertical plate and four angles the broader flanges of the upper angles are to be fitted horizontally, and there is to be a rider plate on the top of the same thickness as the vertical plate, and one inch broader than the sum of the horizontal flanges of the angles.
- 3. The bottom angles of keelsons are to be attached to the reversed frames and to short double reversed frames fitted in way of the keelsons connected by not less than three rivets to the floors. When these double reversed frames form butt straps for the ordinary reversed frames there should be at least three rivets on each side of the butt.
- 4. Continuity.—It is recommended that keelsons be carried fore and aft continuously through the bulkheads, the latter being made watertight around them, and, when such parts of the ship are necessarily separated the longitudinal strength is to be efficiently maintained to the satisfaction of the Surveyors. When keelsons, or other longitudinal strengthening, are required for a certain portion of the length of a vessel, care should be taken to overlap or properly shift the ends of the same so as to avoid any abrupt termination of strength.
- 5. Butt Connections.—All angle and bulb angle bars of keelsons are to be in long lengths, properly shifted, and wherever butted, to be connected with angles not less than 2 feet long, fitted in the throat of them, properly riveted to each flange. The thickness of the connecting straps is not to be less than the thickness of the angle bars they connect. The butts of the plates of keelsons are to be properly shifted and riveted as required by Table 21. The butts of the vertical plates are to be secured with double butt straps, each not less than '14 of an inch thicker than half the thickness of the plates they connect, or the butts may be overlapped.
- 6. All Middle Line Keelsons are to extend as far forward and aft as practicable; the rider plates need not, however, extend beyond $\frac{3}{4}$ the vessel's length amidships.

- 7. Middle Line Keelsons standing upon floors may be formed of double bulb angles when the longitudinal number is under 4,700, when the longitudinal number is 4,700 and under 26,000 the keelson is to be formed of a vertical plate, four angles and rider plate, and when the longitudinal number is 26,000 and above, a foundation plate 18 inches by 50 of an inch is to be fitted on the top of the floors.
- 8. When **Flat Plate Keels** are adopted, intercostal or centre through plate keelsons must be fitted.
- 9. Middle Line Keelsons with Intercostal Plates.— The intercostal plates are to be attached to the floors by double angles of the thickness of the intercostal plates, and with flanges not less than $2\frac{1}{2}$ inches for $\frac{5}{8}$ -inch rivets 3 inches for $\frac{3}{4}$ -inch rivets, and $3\frac{1}{2}$ inches for $\frac{7}{8}$ -inch rivets.
- 10. Centre Through Plate Keelsons .- The centre through plate is to be of the thickness given in Table 6, and a foundation plate not less than 24 inches in width and of the same thickness as the centre through plate is to be fitted on the top of the floors, and attached to the centre girder by continuous angles, or the centre through plate may be extended above the top of the floors, and a foundation plate fitted on each side not less than 12 inches in width. Where the longitudinal number is 10,000 and under 17,200, double bulb angles of the size given in Table 6 are to be fitted above the foundation plates and attached to the centre through plate, and where the longitudinal number is 17,200 and above, the centre through plate is to extend above the floors to the height given on Table 6, and in addition to the foundation plates, four angles of keelson size are to be fitted with a rider plate of the same thickness as the centre through plate.
- 11. Side Keelsons are to be fitted with intercostal plates attached to the outside plating by angles of the thickness of the intercostal plates, and with flanges not less than $2\frac{1}{2}$ inches for $\frac{5}{8}$ -inch rivets, 3 inches for $\frac{3}{4}$ -inch rivets, and $3\frac{1}{2}$ inches for $\frac{7}{8}$ -inch rivets.
- 12. When the breadth of the vessel is under 27 feet, a side keelson is to be fitted on each side extending as far forward and aft as practicable.
- 13. Where the breadth is 27 feet and under 50 feet two side keelsons are to be fitted on each side extending as far forward and aft as practicable. If these keelsons are formed of plate, four angles and rider plate, the depth of the vertical plate of the keelson nearest the middle line may be gradually reduced beyond three-fourths the vessel's length

amidships to the breadth of the flanges of the lower angles, and the rider plate need not extend beyond the three-fourths length. The depth of the vertical plate of the outer side keelson may be similarly reduced beyond three-fifths the vessel's length amidships.

14. When the breadth is 50 feet and under 54 feet two side keelsons are to be fitted as required in the previous paragraph, and in addition a bilge keelson formed of double angles and intercostal plates is to be fitted on each side extending as far forward and aft as practicable.

SIDE STRINGERS.

Section 15. 1. The number of side stringers is to be as required by Tables 2 and 3, and their scantlings and construction as given in Table 7, and shown by the Sketches on page 116. For side stringers in conjunction with web frames see Section 13 and Table 5.

- 2. The spacing of side stringers at ends of vessels is not to exceed that amidships.
- 3. The side stringers are to be formed of continuous angles fitted on the inside of the frames, or of the reversed frames, and when the depth of framing exceeds 3 inches by **Table 2** and 4 inches by **Table 3**, intercostal plates are to be fitted, attached to the outside plating by angles of the thickness of the intercostal plates, and with flanges not less than $2\frac{1}{2}$ inches for $\frac{5}{8}$ -inch rivets, 3 inches for $\frac{3}{4}$ -inch rivets, $3\frac{1}{2}$ inches for $\frac{7}{8}$ -inch rivets, and 4 inches for 1-inch rivets. The stringer angles are to be attached to each reversed frame, or to angle lugs on the frames with at least two rivets, and connected by brackets to the transverse watertight bulkheads, as shown by the **Sketch** on page 130.
- 4. Butt Connections.—The butts of side stringers are to be properly shifted and the angle bars are to be efficiently strapped at the butts with angles not less than 2 feet in length. The thickness of the angle straps is not to be less than the thickness of the angle bars they connect. The intercostal plates are to be in long lengths and strapped at the butts. (See Sketch on page 130.)
- 5. If it should be desired to omit one or more of the side stringers required by this section of the Rules a sketch is to be submitted showing the compensation proposed for such omission.

DOUBLE BOTTOMS AND WATER BALLAST TANKS.

Section 16. 1. Scantlings and attachments.—
The scantlings and attachments of the various parts forming the double bottom are to be as required by Tables 8 and 9.

- 2. Side keelsons and part double bottoms.—Where part double bottoms are fitted the side keelsons are to extend into, or scarph the double bottom, not less than three spaces of frames, and be connected to the longitudinal girders where practicable. Where double bottoms are fitted in the fore and after holds and not extended through the engine and boiler space, care is to be taken to provide against an abrupt termination in the longitudinal strength. The girders are either to be carried through the engine and boiler space, or connected with longitudinal engine and boiler bearers, or otherwise arranged to the satisfaction of the Surveyor.
- 3. A "Well" to be formed in the engine-room.—
 Where a double bottom extends through the engine and boiler space, a "well" should be formed between the engine-room after bulkhead and the floor immediately before the same, for the drainage of water; or open gutter ways of sufficient size should be made in the wings, so as to be always accessible.
- 4. Side girders.—Side girders in a double bottom are to be extended as far forward and aft as accessibility to all parts will admit. The girder nearest the middle line is to be extended to the collision bulkhead, except where fineness of the form of a vessel renders this unnecessary for the efficient stiffening of the bottom plating.

Where the side girders are spaced more than 6 feet apart the watertight floors in double bottom are to be stiffened by vertical angles, of the size of the frame angle on floor, fitted midway between the girders.

- 5. Double reversed frames in machinery space.— Double reversed angles are to be fitted on every floor in engine space, and on each floor in way of boiler bearers. They are to extend in all cases from the middle line to beyond the girder next outside the engine seating.
- 6. Free passage of air between divisions.—It is of importance that ample provision should be made for the free passage of air from one division to another, so that it may readily find its way to the air pipes. This should be done by fitting the liners short, setting down the angle bar from the inner bottom or top of deep tank wherever necessary, and leaving, otherwise, a sufficient number of holes as near to the inner bottom as practicable.

The air pipes should also be sufficient in number and size; and, wherever necessary, one should be fitted at each end of each tank on both sides of the vessel.

7. Tank side brackets and angles.—Bracket plates are to be fitted outside the double bottom, riveted to the margin

plate and to every frame all fore and aft, and to extend up the bilges to the height given in **Table 8**. The bracket plates are to maintain this height throughout the half length of vessel amidships and thence to fore end of double bottom; but abaft the half length amidships the height may be gradually reduced to the level of the inner bottom at the after end of double bottom.

The breadth of the bracket plate at the ship's side and its rivet attachment to the frame angle must, however, in no case be less than its breadth and attachment at the margin plate. The angle bars connecting outside bracket knees to the margin plate are to be fitted on the same side of the bracket plates as the corresponding angles connecting the floor ends or inside brackets to the margin plate.

8. Margin plates.—The margin plate is to be of the depth and thickness required by Tables 8 and 9, and is to be efficiently connected to the outside plating and frames of the main body of the vessel. The full depth of the margin plate is to be maintained throughout the midship three-fifths length of the vessel and to the fore part of double bottom, but abaft the midship three-fifths length of the vessel the depth may be gradually reduced to a depth at the after end of 15 per cent. less than the midship depth.

When gusset plates or other ties are fitted connecting the outside bracket knees to the inner bottom, the horizontal flanges of the margin plates are to be of sufficient width to admit of the gusset plates being efficiently fitted and riveted clear of the landing edge of the inner bottom, and the upper surface of the reversed frames on top of the outside bracket knees should be fair with the top of the inner bottom.

9. Manholes and covers.—Manholes, with wrought iron or steel covers, must be constructed so as to enable the inner surfaces of outside and inner bottom plating, the frames, floors, girders, and rivets to be thoroughly examined and coated when required, and where the manhole covers are attached by bolts to the inner bottom plating, doubling plates or rims are to be fitted to receive the fastenings of the covers.

Where the manhole covers in the double bottoms of cargo holds, or their fittings, project above the tank top, and the ceiling is omitted, they must be protected by fitting an angle coaming around each manhole with a hatch either of wood or of steel fitted therein.

Manholes are not to be cut in the centre girder within three-fourths the vessel's length amidships. The manholes in the floor plates, side girders, and inner bottom plating are to be no larger and not more numerous than necessary to render all parts of the double bottom readily accessible. The edges of the manholes should be smooth to enable them to be entered with facility.

10. Workmanship and Testing.—All watertight joints are to have the surfaces of steel fitted close to each other and caulked, without, as far as practicable, the use of felt, canvas, &c. The double bottom is to be caulked and made watertight, and each compartment intended for water ballast is to be tested on completion with a head of water to the height of the load water line.

Where deep water ballast tanks are fitted their watertightness is to be tested by a head of water 8 feet above the top of the tank, but not less in any case than to the height of the load water line.

A wash plate is to be fitted in the peaks when used for water ballast, and the tanks are to be tested by a head of water 8 feet above the top of tank, but not less in any case than to the height of the load water line.

11. Alternative arrangements.—Any other plan of fitting double bottoms than those hereafter referred to may be adopted, provided in the first instance it receives the approval of the Committee.

12. Peak Tanks.—Attachment where frames and reversed frames are cut at the tops of peak tanks of ordinary length:—

Trans	vers	se Numl	ber.	measur	of bracket ed from out- plating.		Number of Rivets.					
23 a	ind	under	42	15	inches.	4	of	5 8	inch.			
42	,,	,,	54	18	,,	4	"	$\frac{3}{4}$	"			
54	,,	"	63	21	"	5	,,	$\frac{3}{4}$,,			
63	"	"	75	24	,,	6	,,	$\frac{3}{4}$	"			
75	"	"	87	27	,,	7	"	$\frac{3}{4}$,,			
87	99	99	99	30	,,	7	"	7 8	"			

Brackets are to be fitted at every frame of the same thickness as the frame, and are to be attached to the tank top plating by means of single angles of the size required for lower deck stringer angles.

Where only the reversed frames are cut, and not the frames, the bracket attachments as above are to be fitted to alternate frames.

CELLULAR DOUBLE BOTTOMS WITH A FLOOR PLATE FITTED AT EVERY FRAME.

13. Construction.—Where double bottoms are constructed with floor plates, lightened with manholes, fitted to every frame, and continuous in one length from the middle line to the margin plate, intercostal side girders are to be

fitted between the centre girder and margin plate, in accordance with the requirements of Table 8, well connected to the floors and to the inner and outer bottom plating.

- 14. Additional girders in way of engines.—Additional intercostal girders are to be fitted in way of the engine seating.
- 15. Inner bottom plating.—The inner bottom plating is to be continuous and wrought longitudinally. The butts to be shifted well clear of each other and the edges to be shifted well clear of the girders.
- 16. Outside plating.—The outside plating (except flat keel plates and garboard strakes) which is entirely within the boundary of a double bottom having floors fitted at every frame, and which does not exceed '66 of an inch in thickness amidships, may be reduced '02 of an inch where the plating is '52 of an inch in thickness, '04 of an inch where the plating is '54 and not more than '64 of an inch in thickness, and '02 of an inch where the plating is '66 of an inch in thickness, but where the plating exceeds '66 of an inch in thickness amidships no reduction will be permitted in the outside plating.

CELLULAR DOUBLE BOTTOMS WITH FLOOR PLATES FITTED AT ALTERNATE FRAMES.

17. Construction.—Where double bottoms are constructed with floor plates lightened with manholes, fitted to alternate frames, side girders are to be fitted in accordance with the requirements of **Table 8**, well connected to the floors and to the inner and outer bottom plating.

In all cases floor plates are to be fitted under the boiler bearers, also to every frame in the engine space and from the three-fifths length amidships to the collision bulkhead.

Where the rule length of vessel exceeds 400 feet, and in single-deck vessels which exceed 26 feet moulded depth, the double bottom is to be constructed throughout with a floor plate at every frame and with longitudinal girders as required for that system of construction.

- 18. Intermediate frames and reversed frames.—Intermediate frames and reversed frames of the size given in Table 8 are to be fitted for stiffening the outside plating and tank top, unless the longitudinal girders are more closely spaced than required by the Table, or the inner bottom plating be increased '04 of an inch in thickness when the intermediate reversed angles may be dispensed with.
- 19. Bracket plates on intermediate frames.—Bracket plates are to be fitted to the centre girder and margin plates

at the intermediate frames inside the double bottom, and where the longitudinal number is 20,000 and above, the brackets are to be of sufficient breadth at the top to take three rivets in the vertical flange of the intermediate reversed angles, for $\frac{3}{5}$ ths the vessel's length amidships.

- 20. Stiffeners to Side Girders.—Vertical angles are to be riveted to the side girders and attached at their ends, by not less than two rivets, to the intermediate frames and reversed frames.
- 21. Inner bottom plating.—The inner bottom plating is to be continuous and wrought longitudinally. The butts to be shifted well clear of each other and of the butts of the longitudinal girders, and the edges to be shifted well clear of the latter.

Double Bottoms Formed with Girders on top of Ordinary Floors.

- 22. Construction.—Where double bottoms are fitted with longitudinal girders extending on top of ordinary floors the girders must be spaced not more than 3 feet apart with a continuous angle on the upper and lower edges, and in addition to be connected by vertical angles on the floors and girders. Side intercostal plates need not be fitted in the range of double bottom except where the breadth of the vessel exceeds 46 feet.
- 23. Accessibility.—The height of the tank top above the floors to be at least sufficient for easy access and examination of the inside of tank.
- 24. Floor end brackets.—Bracket plates are to be fitted inside and outside the double bottom attaching the margin plate to every floor plate and frame.

ADDITIONAL STRENGTHENING OF THE FORE PART OF THE FLAT OF BOTTOM OF STEAMERS OF FULL FORM.

Section 17. 1. Riveting.—Before the three-fifths length of a steamer having a tonnage co-efficient of \cdot 76 or having a full form at the fore part the rivets in the plating and frames in way of flat of bottom are to be spaced not more than $5\frac{1}{2}$ diameters apart.

2. Side girders.—Where a double bottom is constructed with a floor at every frame additional intercostal girders are to be fitted before the three-fifths length of the vessel, of one-half the depth of the centre girder, and extending as far forward as practicable.

Where the double bottom is constructed with floors at alternate frames and with the floor plates fitted to every frame forward of the three-fifths length, additional girders need not be fitted at that part provided the ordinary side girders extend as far forward as practicable.

- 3. Where there is no double bottom in the fore part of a steamer of full form intercostal side keelsons are to be fitted between the three-fifths length and the collision bulkhead.
- 4. Double Frames.—The frames are to be doubled from the three-fifths length forward to the Rule position of the collision bulkhead, from margin plate to margin plate of double bottoms, or to the turn of bilges where double bottoms are not fitted.
- 5. Outside plating.—The three strakes of outside plating next the keel are to have the midship thickness maintained forward to the collision bulkhead.

COASTING VESSELS INTENDED TO LOAD OR DISCHARGE WHILE LYING ON THE GROUND.

Section 18. In the case of small coasting vessels intended to load or discharge while lying aground, it is recommended that the bottoms be additionally strengthened in order to withstand the exceptional stresses to which they may be subjected.

WATERTIGHT BULKHEADS.

Section 19. 1. Number of Bulkheads.—Screw steamers are to have a watertight bulkhead at each end of the engine and boiler space.

A watertight collision bulkhead is, in addition, to be fitted at not less than one-twentieth of the vessel's length abaft the fore part of the stem measured at a point 8 feet below the upper deck, and a watertight bulkhead is also to be fitted at a reasonable distance from the after end of the vessel.

The foremost or collision bulkhead is to extend from the floor plates to the upper, awning or shelter deck, and its water-tightness is to be tested by filling the peak with water to the height of the load line. In very large vessels the height of this bulkhead will receive the special consideration of the Committee.

2. In steamers 285 feet and under 335 feet in length, an additional watertight bulkhead is to be fitted in the main hold about midway between the collision and boiler room bulkheads.

In steamers 335 feet and under 405 feet an additional watertight bulkhead is to be fitted in the after hold.

In steamers 405 feet and under 470 feet seven watertight bulkheads are to be fitted.

In steamers 470 feet and under 540 feet eight watertight bulkheads are to be fitted.

In steamers 540 feet and under 610 feet nine watertight bulkheads are to be fitted.

In steamers 610 feet and under 680 feet ten watertight bulkheads are to be fitted.

Where the machinery is fitted aft in vessels 220 feet and under 285 feet long, a watertight bulkhead is to be fitted about midway between the collision bulkhead and the bulkhead at the fore end of the engine and boiler space.

- 3. The bulkheads are to extend to the height of the upper deck, except in awning or shelter deck vessels, in which cases the bulkheads, with the exception of the collision bulkhead (see par. 1), may extend to the deck next below the awning or shelter deck. In awning or shelter deck vessels, or vessels with a continuous superstructure or bridge house, a deep web frame or partial bulkhead is to be fitted on each side in the 'tween decks, over each of the watertight bulkheads which extend only to the deck next below the awning or shelter deck. Partial bulkheads may be dispensed with if other efficient strengthening is provided to the satisfaction of the Committee.
- 4. When a bulkhead is not completed at one pair of frames from the floor plate up to its prescribed height per rule, but is recessed, stepped, or stopped at an intermediate part, the watertightness is to be completed with collars or chocks forming a "metal to metal" connection, to the exclusion of cement, wood, &c.

The bulkheads to be connected to the decks and to double bottom plating by angles of the sizes given in Table 10, and to be extended to the outside plating by a watertight sub-division at or near each bulkhead required by Rule.

- 5. Plating.—The plating of bulkheads to be of the thickness prescribed in Table 10, attached to each side of the vessel with angles of the sizes given in the Table, and strongly riveted to them, also connected to the floor plates by a double row of rivets.
- 6. Bulkhead liners.—Doubling plates between frames and outside plating in way of bulkheads, are to extend in one piece from the foreside of the frame before to the aftside of the frame abaft the bulkhead frames, or they may be of an approved diamond shape, fitted and

riveted as shown in **Sketch**. (See page 130.) These doubling plates may be dispensed with, provided the transverse watertight bulkheads are connected to the sides of the vessel by means of brackets of the dimensions shown by the **Sketch** on page 130, fitted at each side stringer and hold stringer. When one or more of the side stringers are omitted, and bulkhead liners are also omitted, brackets are to be fitted two frame spaces in length on each side of the bulkhead, attaching the transverse watertight bulkheads to the outside plating at such places as the side and hold stringers, provided for in the Rules, would be situated. The brackets are to be '06 of an inch thicker than the side stringer intercostal plates which would have been required had the side stringer, or stringers, been fitted.

- 7. Bulkhead Stiffening.—The bulkheads to be supported by vertical stiffening of the description and scantlings given upon Table 10, and the stiffeners are to be not more than 2 feet 6 inches apart. Bracket plates or other efficient attachments are to be fitted at the heads and heels of all vertical stiffeners except in the upper 'tween decks. (See Sketches on pages 126 to 129.)
- 8. The engine-room bulkheads are to extend from the floor-plates to the upper deck, except in awning or shelter deck vessels, in which cases they may extend to the deck next below the awning or shelter deck, provided the machinery openings be trunked in to the height of the awning or shelter deck.

The aftermost bulkhead will be required to extend to the height of the upper deck, unless a different arrangement of bulkheads be approved by the Committee. This bulkhead is to be made watertight by a stuffing box where the screw shaft passes through, and its watertightness is to be tested by the after compartment being filled with water to the height of the load line. The bulkhead plating is to be doubled or increased in thickness in way of the stuffing box.

- 9. Caulking.—All such bulkheads to be caulked and made thoroughly watertight, and to be tested by water from a hose, if considered necessary by the Surveyors, to ensure that they are watertight.
- 10. Bulkhead Recess.—When a recess extending above the hold beams is formed in the engine room bulkheads the bulkhead is to be efficiently connected from side to side by a tie or bridle beam at about the height of the hold beams, strongly riveted to the plating and fitted with efficient gusset plates.

BEAMS.

Section 20. 1. It is recommended that the round up of the beams of all weather decks should be about one

quarter of an inch per foot of length of beam, except when the longitudinal number exceeds 30,000 and at least half the length of the top continuous deck is covered by erections.

- 2. Form of Beam Section.—Beams are to be of the form and size given in Tables 11, 12 and 13 (see also Sketches, pages 109 to 113), or they may be of other approved form of equal strength.
- 3. The beams of the various decks, or of tiers of beams, are to be placed over each other and, as far as practicable, to be fitted to the frames which have reversed frames extended to the upper deck.
 - 4. Beams are to be fitted at every frame:
 - (a) At all watertight flats.
 - (b) At upper decks of single deck vessels above 15 feet in depth.
 - (c) At unsheathed upper decks when a complete steel deck is required by the Rules, also at unsheathed bridge decks, awning or shelter decks. In vessels over 450 feet in length the beams of upper, awning or shelter decks are to be fitted at every frame whether the plating is sheathed or not. Upper decks in way of poops, forecastles, and bridges of vessels less than 66 feet in breadth may have the beams fitted at alternate frames, except for one-tenth the vessel's length within each end of the bridge where they are to be fitted at every frame.
 - (d) Where no wood deck is laid on a steel or iron deck (required by the Rules) at sides of hatchways including those of engine and boiler room openings.

Elsewhere deck beams must in no case be spaced more than two frame spaces apart, and only when the frame spacing does not exceed 27 inches.

5. Rows of Pillars.—The number of rows of pillars is to correspond with the requirements of Tables 11 and 12. Where the length of the midship beams exceeds 44 ft. not less than two rows of pillars are to be fitted, and where the length exceeds 60ft. three rows are to be fitted. Where beams are at every frame, pillars are to be fitted at alternate beams and attached to continuous fore and aft girders under the beams. These girders are to be attached to each beam and to the bulkheads against which they abut, by short angles. For widely spaced pillars and girders at heads of same, see Tables 15 and 16, and Sketches.

Where one row of pillars is fitted, the beams at the ends of the vessel which are less in length than two-

thirds that of the beam amidships, may be of the sizes required by the columns numbered 2 in Tables 11 and 12; and beams at ends less than half the length of the beam amidships may be of the sizes required by columns 3 in Tables 11 and 12.

Where two rows of pillars are fitted amidships the athwartship distance between the rows is to be about one-third the breadth of the vessel amidships; the beams at the ends which are less than two-thirds the length of the beam amidships, may be supported by one row of pillars, and be of the sizes required by columns 2, and where the lengths of the beams at the ends are less than half the midship beam length the sizes may be as required by columns 3 if supported by one row of pillars.

Where three rows of pillars are fitted amidships, the athwartship distances between the rows of pillars is to be about one-fourth the breadth of the vessel amidships, and the beams throughout are to be of the sizes required for beams amidships by columns 3; but where the lengths of the beams at the ends are less than three-fourths the length of the beam amidships, two rows of pillars may be fitted; and where the beams at the ends are less than half the midship beam length, one row of pillars may be fitted.

- 6. If beams of bulb angle section are fitted at alternate frames in vessels exceeding 34 feet in breadth, a steel or iron deck should be fitted on these beams.
- 7. The beams at the ends of hatchways of 12 feet in length and above, where the through beams are fitted to every frame are to be equal in size to those required at alternate frames for their respective decks; where the through beams are fitted at alternate frames no increase in the size of the hatch end beams will be required.

All hatchways of 26 feet in length and above are to be supported at the corners by pillars or girders, in which case no increase is required in the size of the hatch end beams.

Single angles fitted to hatch end beams are to be equivalent to the double angles required by the Rules.

Half beams in way of hatchways or engine and boiler openings may be of the sizes required for beams with two rows of pillars, provided the half beams be efficiently pillared and attached to the coamings.

- 8. Passenger decks.—The beams of decks fitted exclusively for the accommodation of passengers may be of the size given for upper deck beams of the same length.
- 9. "Strong" beams in the machinery space of steamers are to have double angles on their upper and lower edges unless cross tie-plating is fitted on them, in which case only single angles need be fitted to the upper and lower edges of the beams.

10. Beam knees and bracket knees.—Where plate knees are not fitted, beam knees are to be efficiently welded.

The depth and thickness of welded knees, and the depth, breadth, and thickness of bracket knee plates (see Sketches, page 131) for beams fitted at every frame are to be as required by Table 11, and for beams to alternate frames as required by Table 12 for the respective decks, except in the following cases where the beam knees are to be as required by Tables 11 and 12 for upper deck beams of steamers having the same midship length of beam and having one tier of beams only:—

- (a) The upper deck beam knees where the beams below are widely spaced.
- (b) The beam knees at watertight flats for deep tanks.
- (c) The lower and orlop deck beam knees of sailing vessels.
- 11. In the upper deck of large vessels having no decks below, the beams at every frame are to have plate bracket knees as follows:—

Where the depth (d) of the vessel is

23 ft. and under 24 ft. the knees are to be $33 \times 33 \times 50$ ins.

The 42 in, bracket knees are to be stiffened by being flanged on the inner edge.

- 12. Beam knees are to measure across the throats not less than six-tenths of the depths required for the knees.
- 13. Riveting of beam knees.—Not more than two holes are to be punched in each beam knee before the beam is properly adjusted in its position.
- 14. The number and size of the rivets in the beam knees, or in both arms of bracket plate knees, are to be sufficient to ensure the riveted parts being efficiently closed, and in no case to be less than given in the following table:—

	DEP	TH OF]	KNEI	E.	Number of rivets.		Diameter of rivets.
		Under	17 i	inches.	4	$\frac{3}{4}$ of	an inch.
17	and	under	21	"	5	$\frac{3}{4}$,,
21	,,	,,	24	"	5	7 8	,,
24	"	,,	28	,,	6	7 8	,,
28	,,	,,	32	"	7	7 8	"
32	"	,,	36	"	8	78	"
36	"	"	40	"	9	7 8	"

WIDELY SPACED BEAMS IN HOLD.

Section 21. 1. A tier of beams in hold, such that the depth (d) (Section 2, paragraph 3) may be taken between it and the top of floors to determine the scantlings of transverse framing, must have the beams of the size given for "strong" hold beams by Table 12, and having a rider plate of at least the breadth and thickness of the beam plate.

These beams are to be fitted not lower than the middle of the depth of the hold and are to be spaced not more than 24 feet apart. They are to have a broad hold stringer plate riveted to the beam ends. The breadth and thickness of the stringer plate is to be as given below, and it is to be attached to the outside plating with double angles $3\frac{1}{2}$ " × $3\frac{1}{2}$ ", and of the thickness of the stringer plate.

A bulb angle, or equivalent channel, face bar of the size given below is to be riveted to the inner edge of the stringer, and the stringer is to be supported by brackets at alternate frames. See Sketch on page 123.

	DEPTH FROM TOP OF FLOORS TO TOP OF BEAM OF LOWEST LAID DECK AT SIDE.										
L × (B + D)	Feet. Above and Not exceeding 21 23	Feet. Above and Not exceeding 23 25	Feet, Above and exceeding 25 27								
Above and Not exceeding 18200 , 26400	Inches. 60×56	Inches, 64×58	Inches.								
26400 ,, 34800	64×*58	68×·60	72×·62								
Bulb Face Angle	$11 \times 3\frac{1}{2} \times 58$	$11\frac{1}{2} \times 3\frac{1}{2} \times 60$	12×4×·62								

2. Gusset plates, four frame spaces in length and of a breadth equal to one half their length, also of the thickness of the stringer plate, are to be fitted connecting the "strong" hold beams to the stringer plate; and brackets are to be fitted connecting the stringers to the bulkheads.

PILLARS.

Section 22. 1. Pillars are to be of malleable steel or iron of the sizes given in Tables 14 and 15, or they may be of other approved form of equal strength. The number of rows of pillars is to correspond with the requirements of Tables 14 and 15, and Section 20, paragraph 5. Where the length of the midship beam exceeds 44 feet, not less than two rows of pillars are to be fitted, and where the length exceeds 60 feet, three rows are to be fitted. Where beams are at every frame, pillars are to be fitted at alternate beams and attached to continuous fore and aft girders under the deck.

The girders are to be attached to each beam, and to the bulkheads against which they abut, by short angles. For widely spaced pillars and girders at heads of same, see Tables 15 and 16, and Sketches on pages 132 to 141.

2. Riveting of pillars.—Pillars to beams are to be arranged between decks and in the holds so as to form continuous ties from the floors to the weather deck beams. The heads of pillars are to be fitted close under the beams or girders, and the heels are also to be fitted close.

Where the lengths of pillars are under 18 feet, and the diameters are under 4 inches, the ends are to be attached by not less than two $\frac{7}{8}$ inch rivets. Where the lengths are 18 feet and under 24 feet, or the diameters are 4 inches and under 5 inches, there are to be not less than three rivets in each end of the pillars, and where the diameters of the pillars are 5 inches and over, not less than four rivets are to be fitted.

- 3. The heels of pillars at inner bottoms are to be fitted and riveted to short tee or angle bars.
- 4. Deck openings.—Where beams are fitted of the scantlings required with two or three complete rows of pillars, the row of pillars on each side is to be continued in way of all deck openings.

Where beams are fitted of the scantlings required with two rows of pillars, the pillars on each side in way of hatchways may be spaced four frame spaces apart provided they be increased $\frac{1}{2}$ an inch in diameter, and the lower edges of the coaming plates be flanged for a breadth of 6 inches.

- 5. Pillars under widely spaced hold beams may be of the sizes required for pillars of the same length under the deck next above the hold beams.
- 6. Passenger decks.—If the "second" deck is intended exclusively for the accommodation of passengers, the pillars between this deck and the floors may be $\frac{1}{4}$ inch less in diameter than required by the Tables; and where the deck next below is also intended for passengers exclusively, the pillars between this deck and the floors may be $\frac{1}{2}$ inch less than required by the Tables.
- 7. Quarter pillars in deep tanks.—A complete row of quarter pillars attached to an intercostal girder should be fitted on each side of the middle line bulkhead in deep tanks.
- 8. Additional Pillaring.—The pillars to the coamings of hatchways in vessels where only a centre row of pillars is fitted are not to exceed four frame spaces apart on each side, and hatchways 26 feet in length and above are to be

pillared at the corners in addition. Under deck houses, heel of bowsprit, windlass, steam winches and capstans, the beams are to be additionally pillared.

- 9. Where double pillars are fitted for the purpose of securing shifting boards, they are not to be less than three-fourths the diameter required for single pillars.
- 10. Pillars on a shaft tunnel.—If pillars be fitted on a shaft tunnel, the tunnel should be strengthened in way of them, by doubling plates, angle bars, and a transverse vertical plate, or by other efficient means.
- 11. Where a middle line bulkhead is fitted in lieu of a row of pillars, it is not to be less than $\frac{5}{16}$ of an inch in thickness if of iron, or '30 of an inch if of steel, and connected at the bottom and to plating on the beams by single angles not less than $3\frac{1}{2}'' \times 3\frac{1}{2}'' \times '40''$.

The vertical stiffeners are to be spaced not more than two frame spaces apart, and below the lowest laid deck they are to be of the size required by **Table 10** for transverse watertight bulkheads, where quarter pillars are fitted the size of these stiffeners may be modified subject to the approval of the Committee.

The stiffeners at the ends of hatchways are to be bracketed at top and bottom, and the remainder of the stiffeners are to be riveted to the beams and attached at the bottom by double riveted lugs.

In the 'tween decks the stiffeners are to be of double angles of the size required by Table 10 for 'tween deck stiffeners on transverse watertight bulkheads, or of single angles of equivalent size. They are to be spaced not more than two frame spaces apart and riveted at their upper ends to the deck beams.

12. The beams in the machinery space are to be pillared where practicable. Quarter pillars to these beams may be dispensed with provided they are supported by straight bunker sides or casings not less than '30 of an inch thick, having stiffeners extending from the lowest complete tier of beams to the inner bottom and spaced not more than two frame spaces apart. The stiffeners may be one inch less in depth than would be required for a middle line bulkhead. They are to be attached at their heels to the inner bottom by double riveted lugs and riveted at their heads to the beams and half-beams.

PLATING.

Section 23. 1. Thickness.—The thickness of the outside plating as given in Tables 17 and 18, for half the vessel's length amidships, is to be maintained for that length, and may thence be gradually reduced to the thickness given for the extreme ends.

In a steamer having a tonnage co-efficient of '76, or having a full form at the fore part, the three strakes of outside plating next the keel are to have the midship thicknesses maintained forward to the collision bulkhead.

In single screw steamers the plates connected to the stern frame, and in twin screw steamers the plates connected to the "spectacle frame" and to the stern frame must be of the thickness required for the same strakes amidships. Plates on the "spectacle frame" of twin screw steamers, and on the boss of single screw steamers which are to be furnaced should be supplied of the thickness required for propeller boss plates in Table 17. The outside plating is to be of increased thickness or doubled in way of hawse pipes.

- 2. Shift of butts.—No butts of outside plating in adjoining strakes to be nearer each other than two spaces of frames; and the butts of the alternate strakes not to be under each other, but shifted not less than one frame space.
- 3. The butts of the upper, awning or shelter deck stringer plates are in all cases to be shifted not less than two frame spaces clear of the butts of the sheerstrakes.
- 4. The butts of the strakes next to the keel are to be shifted clear of the keel butts, or scarphs, and not to be nearer each other on opposite sides of the vessel than two frame spaces.
- 5. Fitting and caulking of butts and edges.—All flush butts of plating to be planed and fitted close; all overlapped butts and edges of the plating to be sheared from the faying surfaces, or the "burr" caused by shearing to be carefully chipped off, and all outside edges of seams and lapped butts of plating are to be either planed or chipped fair. The butts and edges to be carefully caulked.
- 6. The sheerstrake to extend sufficiently above the upper deck beam ends to take at least two rows of rivets vertically in the butts above the upper flange of the gunwale angle bar.
- 7. Breadths of strakes.—The maximum breadths of strakes of outside plating for which the butt riveting required by Table 21 is applicable are to be as follows:—

Depth (D) of vessel.	Maximum breadth of strake of plating			
Feet.	Inches.			
Not exceeding 20	54			
Above 20 and ,, ,, 24	60			
,, 24 ,, ,, ,, 28	66			
,, 28	72			

If it is proposed to use wider strakes of plating than the foregoing, the riveting of the butts is to be specially submitted.

8. Where it is proposed to cut large openings in the topside plating, efficient compensation is to be provided to the satisfaction of the Committee.

BULWARK PLATING AND STANCHIONS.

9. Steamers.— The stanchions which support the bulwarks in steamers are not to be more than 6 feet apart, and the stanchions nearest to the ends of a bridge or a long poop are not to be more than 5 feet from the bridge or poop bulkhead, and to be made additionally strong to the satisfaction of the Surveyors. The bulwark plating at these parts is to be increased in thickness and supported by bracket plates.

The continuity of strength is to be carefully ensured at the break of erections; and gangways, doors, and other openings in the bulwark plating are to be kept well clear from these breaks. Freeing ports in bulwarks adjacent to the extremities of a bridge, or the front of a long poop, are to have rounded corners and substantial rims. When mooring pipes are fitted in bulwarks the plating in way of same must be doubled.

BUTT-STRAPS AND EDGE LAPS.

Section 24. 1. The breadth and thickness of buttstraps of outside plating, inner bottom plating, deck stringers, plating, floors, keelsons, &c., also the breadths of edge laps of the above, and the number of rows of rivets in such buttstraps and edge laps, together with the spacing of same, are to be as stated in Tables 19, 20, and 21.

LINING PIECES.

2. The space between the plating and the frames to have solid filling or lining pieces of iron or steel in one length, closely fitted; to be of the same breadth as the frames, excepting in way of bulkheads, where they are to be fitted as stated in Section 19, paragraph 6.

RIVETING AND RIVETS.

(See also Tables 19, 20, and 21.)

Section 25. 1. Workmanship.—The work is to be carefully closed with nut and screw bolts before the riveting is commenced. Unfair holes are to be properly rimed out and re-countersunk if necessary, and not to be cut with a

chisel or unduly drifted. The rivets are to be properly staved up so as to completely fill the holes, their heads are to be "laid up" close, and the points or outer ends are to be left full and are not to be below the surface of the plating.

The Surveyors are to see that the rivet holes are properly formed, and the "burr" caused by punching must be removed before the parts are fitted together for riveting.

The rivet holes are to be regularly and equally spaced and carefully punched from the faying surfaces, opposite each other in the adjoining parts, laps, lining pieces, buttstraps and frames. The rivet holes in frames at the turn of the bilge are not to be punched until the frames are bent to the required shape; the holes in way of the lands of the plating are to be drilled or "beared" after the frames are faired in place, and the plate edges lined off.

- 2. Quality and Testing of Rivets.—Rivets, whether of iron or steel, are to be of the best quality, and the Surveyors are to test samples of the rivets when delivered in the shipyards where they are to be used.
- 3. Form of Rivet.—The rivets are to be in diameter as required by Tables 19 and 20, and to be increased in size under their heads to fill the rivet holes. Those used for outside plating are to be of the form shown in Table 20.
- 4. Countersinking.—The countersinking of the rivet holes is to extend through the whole thickness of the plate or angle when the thickness is less than '60 of an inch, and when the thickness is '60 of an inch or above, the countersinking is to extend through nine-tenths the thickness of the plate. The size of the countersink is to be in accordance with the figured dimensions shown in Table 20.
- 5. Arrangement of Rivets.—The size and spacing of the rivets in the various parts of the structure are to be in accordance with the requirements of Tables 19, 20, and 21. The butts of outside plating, and all double and treble riveting, except in the keel, stem and sternpost are to be chain riveted. The keel, stem and sternpost, the butts of outside plating, deck stringers and tie plates on beams, keelsons, stringers, and all longitudinal ties, are to be at least double riveted in all vessels. The butts of deck plating are to be at least double riveted for half the length amidships. The butts and edges of the plating of watertight bulkheads may be single riveted, except the seam connecting the bulkhead plating to floor plate, which must be double riveted.

6. Number of Rows of Rivets in Seams of Outside Plating.—The landing edges of outside plating when '36 of an inch in thickness and above from the keel to the upper turn of bilge, and when '48 of an inch and above from the upper turn of bilge to the gunwale, must be at least double riveted; below these thicknesses the edges may be single riveted.

Where the side plating is '84 inch and above in thickness, the seams of the same are to be treble riveted for four-fifths the vessel's length amidships. The edges of the sheerstrakes are to be double riveted in all cases; except where the side plating is '84 of an inch and above in thickness, when they are to be treble riveted.

The thicker of the two plates is to regulate the size of the rivets and the requirements as to double riveting. When the plating is of a thickness amidships to require the edges to be double riveted, the same is to be continued all fore and aft.

In vessels of 480 feet in length and upwards, with side plating less than '84 inch in thickness, the landing edges are to be treble riveted for one-fourth of the vessel's length in the fore and after bodies for a depth of one-third the depth of the vessel, the actual position of this treble riveting to depend upon the arrangement of shell plating and the special design of the vessel; or other equivalent strengthening to be afforded.

Vessels of from 450 feet to 480 feet in length are to be additionally riveted at the before mentioned parts proportionately to their length, or to have other equivalent strengthening. Each case requiring this additional riveting of the seams is to be submitted for the approval of the Committee.

7. Spacing of Rows of Rivets.—The breadth of butt straps, butt laps and edge laps are to be in accordance with the requirements of **Tables 19** and **21**. The rivets are not to be nearer the butts or edges of the plating, butt straps, butt laps, or of any angle bar than a space equal to their own diameter.

In edge riveting the space between any two consecutive rows of rivets must not be less than once and a half their diameter.

In butt straps the space between any two rows must not be less than twice the diameter of the rivets, and in butt laps the space between consecutive rows is not to be less than two and a half times the diameter of the rivets.

8. Doubling Plates.—When plates have to be doubled the butts of these plates and of the doubling plates are to have the butt straps double or treble riveted, as may be required by Table 21, and in addition, these doubling plates are to be well riveted at the edges and middle of the plates between the frames, in addition to the rivets which pass through the frames, and the middle of the plates are to be riveted up before the edges.

DECKS.

WOOD DECKS.

Section 26. 1. The flat of decks, if of wood, to be of good quality, properly seasoned, free from sap and objectionable knots; the thickness to be as follows:—

Longitud Numbe		At U	pper eks.	At Awning or Shelter Decks, and at Decks of Erections.				
L × (B	+ D).	Thiel	kness.	Thickness.				
		Pine.	Teak.	Pine.	Teak.			
. 1200 and under	2400	inches. $2\frac{1}{2}$	inches.	inches.	inches.			
2400 ,,	3700	$2\frac{3}{4}$	$\frac{21}{4}$	$2\frac{1}{4}$				
3700 "	5200	3	$2\frac{1}{2}$	$2\frac{1}{4}$	-			
5200 ,,	7000	$3\frac{1}{4}$	$2\frac{3}{4}$	$2\frac{1}{2}$	2			
7000 ,,	8800	$3\frac{1}{2}$	3	$2\frac{3}{4}$	$2\frac{1}{4}$			
8800 "	11800	$3\frac{3}{4}$	3	$2\frac{3}{4}$	$2\frac{1}{4}$			
11800 ,,	82000	4	$3\frac{1}{4}$	3	$2\frac{1}{2}$			

The thickness of a wood deck below an upper deck need not exceed $3\frac{1}{2}$ inches.

- 2. Pitch Pine and Yellow Pine.—Pine planks for weather decks should not be laid within a period of from four to six months (according to their thickness) after being cut; and where pitch pine is used for weather decks the breadth of the planks should not exceed 5 inches, and the period of seasoning should not be less than six months.
- 3. Oregon Pine.—Oregon pine of good quality will be admitted for decks of vessels, provided it be laid with the grain vertical, and the width of planks and period of seasoning be as required for pitch pine.
- 4. Artificial Seasoning.—The above required periods of seasoning will not be necessary in cases where satisfactory artificial means of seasoning are adopted.
- 5. The Surveyors must ascertain that the requirement as to the seasoning has been complied with.

- 6. The deck is to be laid and caulked to the satisfaction of the Surveyors.
- 7. When gutter waterways are adopted at the upper deck, the angle bar forming the inner edge of waterways is not to be less in thickness than

·50 where the thickness of the deck is 4 inches.

•44	22	99	**	22	$3\frac{1}{2}$	inches.
•40	11	**	**		3	inches.

- 8. Margin Planks.—In all cases the margin planks of weather decks are to be either of Teak or Greenheart.
- 9. Fastenings.—When the deck planks are 6 inches in width or under, single fastening will be sufficient; but when they are above 6 inches and not exceeding 8 inches in width, there must be two bolts in each plank in every beam, one of which may be a short screw bolt; and planks exceeding 8 inches in width must be double fastened with nut and screw bolts.
- 10. The upper deck to be fastened by galvanised screw bolts with nuts at the under side of the angle bar of the beams and tie-plates. The bolts must be properly sunk, with oakum and white lead under their heads, and be carefully covered over with turned dowels bedded in white lead, marine glue, or other suitable composition.

Pine decks from 2 inches to $3\frac{1}{4}$ inches in thickness are to be fastened with bolts $\frac{1}{2}$ inch in diameter, and where the decks are from $3\frac{1}{2}$ inches to 4 inches in thickness, by bolts $\frac{5}{8}$ inch in diameter. Teak decks from 2 inches to $2\frac{3}{4}$ inches in thickness are to be fastened with bolts $\frac{1}{2}$ inch in diameter, and where the decks are from 3 inches to $3\frac{1}{4}$ inches in thickness, by bolts $\frac{5}{8}$ inch in diameter.

11. Pads not to be used.—Where diagonal plates are fitted on the beams, the deck planks are to be scored over the diagonal plates, so as to fit closely on the beams, thereby avoiding the use of wood pads.

STEEL DECKS.

- 12. Steel decks are to be fitted as required by Tables 17 and 18 of the Rules.
- 13. Where the beams at unsheathed iron or steel decks required by the Rules are not fitted at every frame (see Sec. 20, par. 4), the thickness of the plating is not to be less than required by the following Table:—

Spacing of beams in inches	 42 to 44	46 to 54
Thickness of plating Steel	 .36	.40
amidships in inches (Iron	 6	716

- 14. Continuity of Strength.—Where a steel or iron deck is required by the Rules care should be taken to preserve the continuity of strength at all parts where local stiffness is unavoidably introduced. If intercostal girders are not adopted for the purpose of supporting the beams such girders are to be fitted to prevent local straining between the coamings of hatchways, engine and boiler room openings, deck houses, &c., at the amidship portion of steel or iron bridge, awning or shelter, and upper decks as well as of the deck next below an awning or shelter deck. They should be efficiently connected to the various coamings and casings by laps or brackets, or if not in line with these they should be made to scarph them by a sufficient distance.
- 15. Steel Decks for one-half length.—Where a steel deck is prescribed in Table 18 to be fitted for one-half the vessel's length amidships, it is to be maintained the full breadth of the vessel for that length and then tapered gradually into the stringer plates for one-eighth the vessel's length at each end.
- 16. Wood Sheathing.—If a wood flat be laid over an iron or steel upper, awning or shelter deck, the thickness should not be less than 3 inches if of pine and $2\frac{1}{2}$ inches if of teak, and it should be efficiently secured between the beams to the deck plating. Steel or iron decks are not to be reduced in thickness from that given by Tables 17 and 18, when sheathed with wood.

The thickness of a wood flat laid over a steel or iron deck below an upper, awning or shelter deck need not exceed $2\frac{1}{2}$ inches.

- 17. Caulking.—All decks of steel or iron are to be caulked, unless sheathed with a properly caulked wooden deck.
- 18. Deck openings.—Where large openings are cut in deck plating, compensation is to be given for the same.

Where steel or iron decks are fitted as required by the Rules the thickness of the plating must be increased so as to efficiently maintain the strength of the deck in way of all hatchways and engine and boiler openings, and, in addition, doubling plates are to be fitted at the corners of all large deck openings, or the deck plating increased in thickness equivalent to the doubling plate.

19. Iron decks will be admitted in lieu of steel decks, provided the thickness of the plating be ten per cent. in excess of the thickness required by Tables 17 and 18 for steel decks.

20. Water Testing.—All upper and weather decks of new vessels, of whatever material they are constructed, are, when complete, to have their watertightness tested by a hose in the presence of the Surveyors, who are to state in their First Entry Report the results of such tests.

All gutterways of new vessels are to be tested by being flooded with water, where possible, to ensure watertightness, and the Surveyors are to state in their First Entry Report the results of such tests.

STRINGERS ON BEAMS.

Section 27. 1. Stringer plates are to be fitted upon the ends of each tier of beams. Those upon the ends of the upper, awning or shelter deck beams to be of the breadth and thickness given in Table 18, and those upon the ends of deck beams below upper, awning or shelter decks to be as given in Table 17. Deck stringer plates are to maintain their midship breadth and thickness for one-half the vessel's length amidships; from thence the breadth and thickness may be gradually reduced to those given in Tables 17 and 18 for the ends of the vessel. In way of a long bridge the upper deck stringer plates may be reduced in thickness as shown by Table 18. The stringer plates on widely spaced beams in hold to be as given in Section 21.

- 2. The stringer plates on all deck beams are to be fitted home and riveted to the outside plating, all fore and aft, with angle bars of the dimensions required by **Tables 17** and **18**. The stringer plates of all decks below the upper, awning or shelter decks are to have an additional angle bar of the same dimensions fitted inside the reversed frames and extending all fore and aft. For stringer angles on widely spaced hold beams see **Section 21**.
- 3. When the frames are extended through the upper deck stringer plate to form frames for bridges, poops and forecastles, there must be a continuous angle bar, of the size given in **Table 17**, wrought on the upper deck stringer plate inside the frames.
- 4. The upper deck stringer angle bar is in all cases to be fitted on the upper side of the stringer plate.
- 5. When gutter waterways are fitted to upper decks in vessels having poops or forecastles, the angle bars forming the ends of the gutters are to be welded, and the gutters to be carefully caulked.

TIE-PLATES ON BEAMS.

Section 28. 1. Where there are no steel decks laid, tie-plates are to be fitted on the beams, extending all fore and aft upon each side of the hatchways. Upon deck beams below the upper deck, on which no deck is laid, double angle bars of the sizes given in Table 17 for beam stringer angles, placed at middle line or at each side of the hatchways, will be admitted in lieu of plate ties.

2. The tie-plates are to be of the width and thickness given in **Tables 17** and **18**, for half the vessel's length amidships, tapered at the ends to the same thickness as the ends of the stringer plates. They are to be well riveted to each other and to the beams and stringers.

HOOKS AND CRUTCHES AND PANTING ARRANGEMENTS.

Section 29. 1. Spacing of stringers at ends.—
Stringers, where practicable, are to extend all fore and aft, and to be efficiently connected at their ends with plates forming hooks and crutches of the same thickness as the floor-plates amidships, and those below the hold beams are to be spaced about 4 feet apart. In vessels whose longitudinal number is 18,200, or above, an additional hook or crutch should be fitted at the ends of the vessel, between each tier of beams, to the satisfaction of the Surveyors.

- 2. Beams in peaks.—Tiers of beams are to be fitted throughout the depth of peaks, the tiers being spaced not more than 8 feet apart.
- 3. All vessels to have, in addition, provision made to prevent panting, by means of an extra tier or tiers of beams, also by bracket knees, and stringer plates, fitted abaft the collision bulkhead.
- 4. Where a vessel has considerable sheer, additional transverse strength in the form of beams or otherwise is to be provided, having regard to the form of the vessel.
- 5. Panting beams and stringers are to be fitted at the after end of vessel where considered necessary by the Surveyors. Sketches of panting arrangements are in all cases to be submitted for approval. The stringer plates on panting beams are to be worked intercostally between the beams, and attached to the outside plating.

ENGINE AND BOILER SPACE.

Section 30. 1. Engine and Boiler bearers.—In steam vessels care must be taken that the engine and boiler bearers are properly constructed, and fitted with efficient longitudinal ties. Where the bearers interfere with the longitudinal strength of the vessel, they must extend a sufficient distance beyond the bulkheads of the engine and boiler space to compensate for the same.

When engines of high power are fitted.—Where it is intended to fit engines of greater power than in ordinary cargo carrying steamers, the engine seating is to be of proportionately greater strength, and to be specially adapted with this object in view by being connected to the sides of the vessel. Other means are, if necessary, to be adopted in order to ensure the rigidity and strength necessary to withstand the vibration produced in this part of the vessel.

- 2. Strengthening in machinery space.—Additional strengthening by means of web frames, and "strong" beams, or otherwise is to be provided in the machinery space. Plans showing the proposed additional strengthening are to be submitted for approval.
- 3. Clearance between bulkheads and boilers.—Coal bunker bulkheads are to be kept well clear of the boilers and their uptakes. Where the boiler room bulkhead is recessed for a donkey boiler, the recess is to be of a size sufficient to give space all round the boiler to admit of its being properly attended to.

In order to afford protection against the heat from the boiler, the roof of the recess is to be not less than 4 feet clear of the top of the boiler, the space between the bunker or hold bulkhead plating and the chimney is to be not less than 18 inches, and a baffle plate is to be fixed between the chimney and the bulkhead; other efficient means may be provided. Wood lining is to be fitted on the hold side of the recess plating with an air space between it and the plating.

4. Tie-beams across recess.—When a recess extending above the hold beams is formed in the engine room bulkheads, the bulkhead is to be efficiently connected from side to side by a tie or bridle beam at about the height of the hold beams, strongly riveted to the plating and fitted with efficient gusset plates.

- 5. Protection of deck under donkey boilers.—Where vertical donkey boilers are placed on the decks of vessels, the deck underneath them is to be protected by being covered with firebrick or cement not less than 2 inches in thickness. The deck on which fires may be drawn from any donkey boiler is also to be protected by firebrick or cement not less than 2 inches in thickness.
- 6. Shaft tunnel.—The plating of shaft tunnels is to be of the thickness required in **Table 10** for the lower part of bulkhead plating; the top plating in way of the hatchways to be not less than '10 of an inch thicker than the remaining plates, or to be covered with wood not less than 2 inches thick.

The tunnel is to be strengthened with transverse angle bars of the size of the lower deck stringer angles spaced not more than two frame spaces apart, and 3 feet in way of the hatchways.

The plating is to be caulked, and the tunnel tested with water from a hose to ensure its being watertight.

The bulkheads and top plating of tunnel recesses to be strengthened and supported by similar angles, but spaced the same as the vessel's frames; the top plating where attached to the sides of the vessel to be made watertight with steel or iron collars or chocks, to the exclusion of wood or cement.

The tunnel to be fitted with a watertight sluice door on the engine-room bulkhead, capable of being closed from the upper deck.

If a pipe tunnel is led through the forward holds, its structure is to be the same as that of a shaft tunnel.

ENGINE AND BOILER OPENINGS.

Section 31. 1. Framing of openings.—The engine and boiler openings of the weather deck of steam vessels are to be properly framed for a height of not less than 18 inches above the deck, the coaming plates to extend to the lower edge of the beams, and iron or steel casings connected to the coamings should be fitted to a height of about 7 feet above the deck.

In awning or shelter, and part awning deck vessels the height of the casing need not exceed 4 feet 6 inches above the deck, provided suitable iron covers be fitted, and the openings have coamings on the top of the casings not less than 9 inches in height.

The thickness of the casings, where exposed, to be not less than that required for the side plating of poops, and to be efficiently stiffened by vertical angles spaced 30 inches apart, connected to the coaming plates. The thickness of the coamings to be 06 of an inch more than required for the casings.

Where the casings are enclosed by a bridge, and efficiently protected from the force of the sea, a reduction from the above thickness might be admitted, provided in such cases a plan showing the proposed arrangement be furnished for approval.

- 2. Trunk casings.—The engine and boiler openings in the 'tween decks of all vessels are also to be enclosed by trunk casings efficiently stiffened by angle bars 30 inches apart, and extending to the weather deck beams, to which they are to be secured.
- 3. Strong iron doors will be allowed in these trunk casings, provided their lower parts are at least 18 inches above the deck, and efficient arrangements made for their security.
- 4. Height of coamings.—When a poop, or bridge, covers the engine and boiler space, the coaming of the engine and boiler openings should not be less than 2 feet above such deck, unless these openings are constructed as provided for in the first paragraph of this Section.
- 5. The engine and boiler openings should be made as small as practicable, and be subdivided by athwartship iron divisional bulkheads. The two sides of the casing should in all instances be efficiently connected by angle beams within them at the upper part.
- 6. Skylights and gratings.—The engine-room skylights are to be substantially constructed, and to be securely bolted or riveted to the coamings, and where the skylight top is not solid, with bull's eyes fitted in the same, efficient deadlights must be provided. The grating openings over the stokehold must also be protected by plates, fitted with hinges, or otherwise in a manner satisfactory to the Surveyors.
- 7. Plating in way of openings.—Where either of the openings exceeds 15 feet, or the combined length exceeds 30 feet, the beams in way of the same are to be plated over from the stringer to the tie-plates, the plating extending two beam spaces beyond the openings, and tapered

from thence towards the stringer plate for a distance not less than the breadth of the plating required to be fitted.

- 8. Where large openings are adjacent to each other, the intervening space between the openings is to be plated over.
- 9. Steam Trawlers.—In all steam trawlers the deck beams should be wholly plated over in way of the engine and boiler casings, and the casings should extend down to the underside of the deck beams, and be connected to the deck plating with angle bars and to the half beam ends with angle lugs. If the casings be not extended down to the underside of the beams, they should be attached to the deck plating with angles $4\frac{1}{2}" \times 4\frac{1}{2}" \times 36$," having two rows of rivets in each flange. In order to ensure that the scantlings and construction of these casings are satisfactory in every case, detailed plans of the same should be submitted for approval.

HATCHWAYS.

(See also Sketches, pages 142 & 143.)

Section 32. 1. Hatchway Beams.—Beams at the ends of hatchways may be fitted with a large single angle bar, on the side of the beams clear of the hatchway, of equivalent sectional area to the double angles required by Table 13. Half beams are to be fitted to alternate frames in way of the hatchways where a wood deck is fitted, and to every frame under a steel or iron deck, unless a wood flat is laid thereon, in which case half beams may be fitted to alternate frames.

- 2. Depth of Coamings.—The side coamings are to extend to the lower edges of the beams at the ends of the hatchways. The end coaming plates are to extend to the lower part of the beams at the ends of the hatchways, and be riveted to them.
- 3. Thickness of Coamings.—The thickness of coamings to be as follows:—

		Len	gth o	of hatch		Side coamings.	End coamings.	
				Feet.			Inches.	Inches.
				Not e	xceeding	12	.36	.36
1	Above	12	and	"	,,	16	.40	.36
	,,	16	,,	"	,,	24	.44	•40
	"	24	,,	"	,,	26	•46	.40
	,,	26	,,	,,	,,	28	.48	.40
	"	28	,,	,,	"	30	.50	.40

4. Height of Coamings above Deck.—The minimum heights of hatchway coamings above weather decks to be as follows, unless otherwise submitted and approved:—

On awning or shelter decks, and bridge decks 18 inches.

On upper decks (except under awning, shelter decks, or long bridges), and raised quarter decks

On upper decks in wells of well deck steamers, and under tonnage openings of shelter decks

- 5. Shallow Coamings.—Shallow coamings to hatchways below the weather deck will be sanctioned, provided the total depth of the fore and aft carlings and coamings be not less than 16 inches in hatchways of 10 feet and not exceeding 14 feet in length, 18 inches in hatchways of above 14 feet and not exceeding 18 feet in length, and 20 inches in hatchways of above 18 feet and not exceeding 24 feet in length; but in all cases the coamings are to extend at least to the lower part of the beams at the ends of the hatchways. Hatchway side coamings below upper deck to be '04 of an inch thicker than side coamings to upper deck hatchways of the same length.
- 6. Where square corners are adopted, the angles connecting the side and end coaming plates are not to be of less thickness than the side coaming plates.
- 7. Connection of Coamings to Deck.—The coaming plates are to be connected to the deck plating or tie plates with angles of not less thickness than the side coaming plates, welded at the corners of the hatchways. Where a wood deck is fitted, the vertical flanges of the angle bars connecting the side and end coamings to the deck are to extend half an inch above the deck.
- 8. Material.—All hatchway coamings on weather decks and the companions at the fore-end of steamers to be of steel or iron.
- 9. Half Beams.—Where half beams are fitted to alternate frames, they are to be connected to the coaming plates with double angles, and half beams fitted to every frame may be connected to coaming plates, with single angles of not less thickness than the side coamings. There are to be three rivets in each flange of the angles connecting coamings to the half beams where the depth of the half beam is $7\frac{1}{2}$ inches to $9\frac{1}{2}$ inches, and four rivets where the depth is 10 inches to 12 inches,

- 10. Where there are no steel or iron decks, plates are to be fitted and riveted to the hatchway beams in order that the ends of the wood deck may be properly fastened, and side coaming plates are to be connected to deck plates of the thickness required for tie plates. The fore and aft tie plates in way of hatchways 16 feet and under 22 feet in length are to be double the width of those given in Tables 17 and 18 for a length extending two spaces of beams beyond each end of the hatchway.
- 11. Plating in Way of Long Hatchways.—Where the length of hatchway is 22 feet and above, the beams to upper deck (and deck above if fitted) are to be plated in way of same, and the plating is to be tapered before and abaft to stringer plate.

Where steel or iron decks are fitted in accordance with the Rules, the thickness of the plating must be increased so as to efficiently maintain the strength of the deck in way of all hatchways and engine and boiler openings, and, in addition, doubling plates are to be fitted at the corners of all large deck openings, or the deck plating increased in thickness equivalent to the doubling plate.

12. Web Plates and Shifting Beams.—Hatchways of above 10 feet and not exceeding 16 feet in length are to have shifting beams formed of plate and four angles, $3^{\prime\prime} \times 3^{\prime\prime} \times \cdot 40^{\prime\prime}$. If the hatchways are not more than 12 feet in width, the shifting beam is to be $12^{\prime\prime} \times \cdot 40^{\prime\prime}$ and if above 12 feet and not exceeding 16 feet in width $15^{\prime\prime} \times \cdot 40^{\prime\prime}$.

When the length of a hatchway is from 16 feet to 20 feet, a web plate beam is to be fitted at the middle of the length, extending in depth to the lower edges of the coamings. If the length is above 20 feet and not exceeding 30 feet, two web plate beams are to be fitted.

Efficient means are to be provided for securing the shifting beams and web plates to the coamings.

The web plate beams are to be stiffened at the upper and lower parts with double angles, and the thickness of the web plate is to be the same as that of the end coamings. Web plate beams in hatchways below the weather deck where shallow coamings are fitted are to be of not less thickness than the coamings to which they are attached, and to extend to the lower edge of the coamings.

Where shallow coamings are fitted, as described in paragraph 5 of this Section, the depth of the web plate at middle is to be not less than one and a quarter times the depth at ends, and the upper and lower parts of the web plate are to be stiffened with double angles.

13. Fore and Afters.—Fore and afters are to be fitted in hatchways as follows:—

STEEL BULB PLATES.

.hegsterl	ore s.	01 1 2		Distance	between	Web Beams	Centre to	Centre, in	Feet.	im suima	No seek	
Breadth	Number of Fore and Afters.	5 and unde	6.	6 and under	7	7 and under	. 8	8 and under	, de 191	9 and 10		
Hatchway.	Num	Centre.	Side.	Centre.	Side.	Centre.	Side.	Centre.	Side.	Centre.	Side.	
Feet.	1	Ins. 8 × ·40	Ins.	Ins. 9 × •40	Ins.	Ins. 10×*44	Ins.	Ins. 10×*50	Ins.	Ins. 11×*50	Ins.	
8 " 10	1	9×·40	6	9×·44	1=	10×·50	_	11×*50		11×·54		
10 ,, 12	3	8×.34	5 × ·24	8×·40	5 × ·24	9ו40	6 × ·24	9×·44	6×·30	10×·44	7×30	
12 ,, 14	3	8×40	5 × ·24	9×·40	6 × 24	9×·44	6×.30	10×·44	7×*30	10×·50	7 × 3	
14 ,, 16	3	9×.44	6 × ·30	10×44	7×.30	10×:50	7 × ·34	11×.20	8 × ·34	11×:54	8×4	
16 ,, 18	3	10×44	7×·30	10×·50	7× 34	11×50	8×·34	11×.54	8 × ·40	11×.60	8×.4	
18 ,, 20	5	8×:40	5 × ·24	9×·40	6 × ·24	9×:44	6×·30	10×44	-7×-30	10×.50	7×3	

WOOD.

1				- 1.	300		Di	stanc	e betv	veen	Web I	Beam	s, Cent	tre to	Centr	e, in	Feet.					
	Breadth of Hatchway.			5 an		M.	0.0	3 an	d 7		,	7 an	d 8			3 an	d 9		9	and	10 er 10	. 4
-	of Hatchway.	nd Af	Cent	re.	Sid		Cent	re.	Sid	.e.	Cent	re.	Sid	e.	Cent	re.	Sid	e. :	Cent	re.	Sid	e.
-	Hatenway.	Nun	Depth below Hatches.	Breadth.	Depth below Hatches.	Breadth.	Depth below Hatches.	Breadth.	Depth below Hatches.	Breadth.	Depth below Hatches.	Breadth.	Depth below Hatches.	Breadth	Depth below Hatches.	Breadth.	Devth below Hatches.	Breadth.	Depth below Hatches.	Breadth.	Depth below Hatches.	Breadth.
-	Feet.		Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins. $7\frac{1}{2}$	Ins.	Ins.	Ins.	Ins. 8	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.
1	6 and 8	1	6	6			7	6			12	-			0	-					1	0.0
	8 " 10	1	7	6	-	-	7	7		_	8	7		-	9	7			9	-8	<u></u>	
-	10 ,, 12	3	$5\frac{1}{2}$	6	5	5	6	6	5	5	7	6	$5\frac{1}{2}$	5	7	7	6	5	$7\frac{1}{2}$	7	$6\frac{1}{2}$	$\frac{5\frac{1}{2}}{-}$
1	12 ,, 14	3	6	6	5	5	7	6	$5\frac{1}{2}$	5	7	7	6	5	$7\frac{1}{2}$	7	$6\frac{1}{2}$	$5\frac{1}{2}$	8	7	7	6
	14 ,, 16	3	7	7	.6	5	$7\frac{1}{2}$	7	$6\frac{1}{2}$	$5\frac{1}{2}$	8	7	7	6	9	7	$7\frac{1}{2}$	$6\frac{1}{2}$	9.	8	8	7
-	16 ,, 18	3	$7\frac{1}{2}$	7	$6\frac{1}{2}$	$5\frac{1}{2}$	8	7	7	6	9	7	$7\frac{1}{2}$	$6\frac{1}{2}$	9	8	8	7	$9\frac{1}{2}$	8	81/2	$7\frac{1}{2}$
	18 ,, 20	5	6	6	5	5	7	6	$5\frac{1}{2}$	5	7	7	6	5	$7\frac{1}{2}$	7	$6\frac{1}{2}$	$5\frac{1}{2}$	8	7	7	6

The angles on the centre fore and afters are not to be less than $3'' \times 2\frac{1}{2}'' \times 30$ inch where the depth of the bulb plate is less than 9 inches, and not less than $3'' \times 3'' \times 36$ inch where the depth is 9 inches and above. The double angles on the side fore and afters are not to be less than $2\frac{1}{2}'' \times 2\frac{1}{2}'' \times 30$ inch. The wood fore and afters

are to be of pitch pine, or other wood of not less hardness and strength, free from shakes or other defects; and the centre fore and afters are to be cut from the solid wood. When wood fore and afters are used iron plates are to be fitted to their ends. All fore and afters to be efficiently supported at the end coamings and web plate beams with

castings or angles having a bearing of not less than 2 inches; and fore and afters, whether of steel or wood, should also be supported by the shifting beams when such are fitted in the hatchway.

14. Hatch covers when fore and afters are fitted.— The hatches of all vessels to be solid (or gratings of sufficient strength) and not less than $2\frac{1}{2}$ inches thick in hatchways not exceeding 16 feet in breadth; where this

breadth of hatchway is exceeded the hatches are not to be less than 3 inches in thickness, where fore and afters are fitted as described in paragraph 13. Efficient supports are to be provided, having at least 1³/₄ inches bearing, for the ends of the hatches.

15. Where fore and afters are dispensed with, deep transverse web plates are to be fitted in the hatchways as given in the following table:—

	UPP	ER AND ALL	WEATHER DECK 1	HATCHWAYS.					
Breadth		pacing of Wand under 4	eb Plates feet 6 inches.	Spacing of Web Plates 4 feet 6 inches and under 5 feet.					
of Hatchway.		epth below d thickness.	Double Angles on Upper and		lepth below d thickness.	Double Angles on Upper and			
e sekagaupa dik Limbolio di Ka	Centre.	Ends.	Lower Parts.	Centre.	Ends.	Lower Parts.			
Feet. 12 and under 14	Inches. 14 × 34	Inches. 11 × '34	Inches. 3 × 3 × '40	Inches. 16 × 34	Inches.	Inches. 3 × 3 × 40			
14 ,, 16	16 × 34	13 × ·34	3 × 3 × ·40	19 × ·34	14 × 34	3 × 3 × 40			
16	18 × 34	1.4 × ·34	† 4 × 3 × ·40	21 × ·34	16 × 34	†4.× 3× 40			
18 ,, 20	20 × 40	16 × 40	†.4 × 3 × ·40	23 × ·40	18 × ·40	† 4 × 3 × ·40			
giam das gainde se		HATCHWAYS	BELOW THE UPPE	R DECK.					
12 and under 14	13 × 40	13 × 40	3 × 3 × ·40	15 × ·40	13 × 40	3 × 3 × 40			
14 ,, 16	15 × ·40	13 × ·40	$3 \times 3 \times 40$	17 × ·40	14 × ·40	$3 \times 3 \times 40$			
16 ,, 18	16 × ·40	14 × ·40	†4 × 3 × ·40	18 × ·40	15 × 40	†4 × 3 × ·40			
18 ,, 20	18 × ·44	15 × '44	†4 × 3 × ·40	20 × ·44	16 × ·44	† 4 × 3 × '40			

†4 inch flange fitted horizontally.

The web plates are to be of the depth and thickness given in preceding Table, and are to be stiffened at the upper and lower parts by double angles, and alternate web plates are to be extended to the top of the wood hatches. If necessary, the web plates are to be increased in depth at the ends or are to have bracket plates fitted so as to extend to the lower edge of the coaming plates. The web plates are to be securely attached to the coamings by double angles $3\frac{1}{2} \times 3$ inches and of not less thickness than the web plates, or other efficient arrangements for securing the same are to be provided.

Hatch covers when no fore and afters are fitted.— Where this arrangement of web plates is adopted the hatches are to be solid (or gratings of sufficient strength) and not less than 3 inches in thickness, and efficient supports are to be provided, having not less than 3 inches bearing, for the ends of the hatches at the end coamings.

16. Additional requirements for large hatchways.—Plans of hatchways more than 30 feet in length or 20 feet in breadth, showing the scantlings and arrangements of deck plating, beams at ends of hatchways, coamings and web

plate beams are to be submitted for approval, together with the additional transverse strengthening proposed in way of the same, either by means of web frames, increased depth of framing, or by double reversed frames.

- 17. Cleats not more than 2 feet apart from centre to centre are to be fitted to the coamings for the purpose of efficiently securing the tarpaulin covers. The cleats to be of strong section. Flat iron bars and suitable wedges or other efficient means to be provided for securing the tarpaulins.
- 18. Wing boards.—In vessels having self-trimming hatchways, wing boards are to be fitted for preventing the shifting of cargo.

COAL BUNKER PIPES AND LIDS. .

Section 33. Coal bunker pipes, where practicable, are to be formed so as to be at least 12 inches above the upper deck, fitted with lids having studs to fit in openings made in the pipes, for their security; the pipes to be so formed that a tarpaulin may be securely lashed over them. Where there are coal bunker hatches in the weather deck they must be properly framed with coaming plates of suitable height having solid hatches secured by an iron bar or other approved fastening.

MASTHOLES.

Section 34. In way of mast wedging, where iron or steel decks are not fitted, plates are to be riveted to the beams of not less thickness than is required for stringer plates amidships, and of not less width than three times the diameter of the mast. In steamers the mast ring is to be of plain angle of not less size than the bulb angle frames required in peaks.

VENTILATORS.

Section 35. 1. Number and Size.—It is recommended that ventilators, sufficient in number and size, be efficiently fitted to upper decks of all vessels.

2. Ventilator Coamings.—The coamings of weather deck ventilators should not be less than 3 feet in height and of the following thicknesses:—

Under 12 inches in diameter ... $\frac{1}{4}$ of an inch. 12 inches and under 15 inches ... $\frac{5}{16}$,, 15 ,, 24 ,, ... $\frac{3}{8}$, Where a steel or iron deck is fitted, these coamings are to be connected to it with angles $\frac{1}{16}$ of an inch thicker than the coaming. Where there is no steel or iron deck fitted, plates are to be fitted under the wood deck to take the bolt fastenings.

3. Covers.—Means are to be provided for efficiently closing the openings when the cowls are unshipped.

When scuttles are fitted for ventilation in the topsides of vessels, strong covers for them are to be provided; these covers to be efficiently fitted, to the approval of the Surveyors.

4. Compensation for cutting side scuttles.—Where scuttles are fitted in the sheerstrake within three-fifths of the vessel's length amidships, compensation is to be given either by an extra thickness in the sheerstrake, doubling plate in way of the scuttles, or else by the introduction of strong angle bars over them.

PORTS AND SCUPPERS.

Section 36. 1. All vessels must be fitted with a sufficient number of freeing ports and scuppers, to readily discharge any large quantity of water from the upper deck. The ports and flaps, where such are adopted, are to be hung by strong hinges with yellow metal pins, and the scuppers formed in the vertical flange of the upper deck stringer angle bar, which is to be increased in depth so as to enclose the scuppers; or any other equally efficient plan may be adopted.

- 2. Where the bulwark plating and main rail are cut through to form a gangway or cargo port, the bulwark stays at each end of the port should be of increased strength, to the satisfaction of the Surveyors.
- 3. A sufficient number of scuppers, with proper pipes attached to them, are to be fitted in all 'tween decks below upper deck to convey water or leakage to the bilges.
- 4. In "Well deck" vessels, the freeing port area in the "Well" should be in accordance with the following Table:—

Ler

ngth of Bulwa			ng Port Area on each					
"Well," in fe	et.	side, in square feet.						
30	·	 	9.5					
35	ANGE, SI	 M	10.0					
40		 Minizo	10.5					
45		 	11.0					
50	old (orni, sv	11.5					
55		 	12.0					
60		 1	12.5					

65 and above, one square foot to each 5-ft. length of bulwarks.

WINDLASS AND HAWSE-PIPES.

Section 37. 1. The windlass is to be of suitable size for the cable, and to be efficiently secured.

2. The hawse-pipes must be of sufficient size and thickness, and the outside flange of proper form to admit of an easy lead for the cable to the windlass or capstan.

CHAIN PLATES.

Section 38. The chain plates to be in proportion to the size of the vessel, and riveted efficiently to the outside plating (not bulwark plating), the sheerstrake being preferable.

PUMPING ARRANGEMENTS.

Section 39. 1. In steam vessels the pumping arrangements according to the division of holds, &c., are to be as follows:—

2. Holds with double bottoms.—In the double bottom of each compartment of the holds and of the engine and boiler space, a steam pump suction is to be fitted at the middle line, and one on each side to clear the tanks of water when the vessel has a heavy list.

Where there is considerable rise of floor towards the ends of vessels, the middle line suction only will be required. A steam pump suction and a hand pump are also to be fitted to each bilge in each hold where there is no well.

Where there is a well, one or three steam pump suctions are to be fitted in the same according as there is considerable or little rise of floor, and hand pumps are to be fitted at the bilges.

- 3. Holds without double bottoms.—Where there is considerable rise of floor, one steam pump suction and one hand pump are to be fitted in each hold. Where there is little rise of floor, two or three steam pump suctions and at least one hand pump are to be fitted to each hold.
- 4. Engine and boiler space.—Where a double bottom extends the whole length of the engine and boiler space, two steam pump suctions are to be fitted to the bilge on each side. Where there is a well, one steam pump suction should be fitted in each bilge and one in the well. Where there is no double bottom in the machinery space, centre and wing steam pump suctions should be fitted.

The rose box, or strum, of the bilge injection is to be fitted where easily accessible. The main engine bilge pump and the donkey pump are to be arranged to draw from all compartments, and the donkey pump is to have also a separate bilge suction in the engine room, which can be used at the same time as the main engine bilge pumps are drawing from any other part of the vessel.

- 5. Fore and After Peaks.—If the peaks are fitted as water ballast tanks, a separate steam pump suction is to be led to each. If not used for water ballast, an efficient pump is to be fitted in the fore peak. If the after peak is used as a ballast tank, no sluice valve or cock is to be fitted to the after bulkhead; but if it is not so used, and if no pump is fitted in it, a sluice valve or cock is to be fitted to the after bulkhead, to allow water to reach the pumps when required.
- 6. Tunnel.—The tunnel well is to be fitted with a steam pump suction.
- 7. All Hand Pumps are to be capable of being worked from the upper or main decks or above the Load Water Line, the bottoms of the pump chambers are not to be more than 24 feet above the suction rose, and the pumps are to be tested by the Surveyors to ensure that water can be pumped from the limbers. The sizes of the hand pumps are to be not less than those given in the following Table:—

Hand Pumps in Holds.					
Diameter of Barrel.	Diameter of Tail Pipe.				
Inches.	Inches.				
$4\frac{1}{2}$	$2\frac{1}{4}$				
5	$2\frac{1}{2}$				
$5\frac{1}{2}$	$2\frac{3}{4}$				
	Diameter of Barrel. Inches. $\frac{4}{4\frac{1}{2}}$ 5				

In lieu of hand pumps in each compartment, an approved fly wheel pump may be fitted if it is connected to the steam pump bilge suction pipes of these compartments.

The hand pumps may be dispensed with in vessels which have two independent boiler rooms, or a donkey boiler above the bulkhead deck, and steam pumps (workable from either source of steam) in two separate compartments, connected to the suctions.

- 8. No Sluice Valve or Cock is to be fitted to the collision bulkhead.
- 9. No Sluice Valves or Cocks are to be fitted to the engine room or other watertight bulkheads unless they are arranged so as to be at all times accessible.
- 10. When Sluice Valves are fitted, they are to be so arranged as to be controlled above the Load Water Line, and the rods are to be boxed in to prevent injury.
- 11. Sounding Pipes are to be fitted on each side of holds and ballast tanks, and a doubling plate is to be fitted under each.
- 12. Air Pipes are to be fitted to each ballast tank as required.
- 13. All Cocks and Valves in connection with bilge and ballast suction pipes are to be fitted in places where they are at all times accessible.
- 14. All Bilge Suction Pipes are to be fitted with strum boxes or strainers, so constructed that they can be cleared without breaking the joints of the suction pipes. The total area of the perforations in the strainers should be not less than double that of the cross section of the suction pipe.
- 15. The filling pipes for deep tanks which can be used for either cargo or ballast must be controlled by valves placed in an accessible position, and so arranged that when the tank is being used for cargo it will be impossible to fill it with water. This result is to be obtained by taking out a short bend or wedge piece and fitting blank flanges in its place, or in some other way to be submitted to and approved by the Committee.
- 16. The Pipes for bilge or ballast suctions are to be fitted with flanged joints in convenient lengths, so that they may be easily disconnected for clearing. In the case of cast iron suction pipes, which are not also used as tank filling pipes, or which cannot be subjected to sea pressure, spigot and faucet joints made with india-rubber rings fitted over the spigots might be adopted, except in the case of bilge suction pipes passing through ballast tanks, which should be fitted with flanged joints.
- 17. The Suction Pipes to fore and after peaks, and to the tunnel well, should not be less than $2\frac{1}{4}$ inches inside

- diameter, except in vessels under 500 tons under deck, in which case they may be made 2 inches.
- 18. The Bilge Injection should not be less than two thirds of the diameter of the sea inlet to the circulating pump.
- 19. The inside diameter of other bilge suction pipes should not be less than given in the following Table:—

Tonnage under Upper Deck.	Engine Room Centre Suction, Separate Donkey Suction, and Hold Centre Suctions.	Wing Suctions in Holds where no Centre Suctions are fitted, and Wing Suctions in Engine Room.	Wing Suctions in Holds where Centre Suctions are also fitted.
In vessels under 500 tons	Inches.	Inches.	Inches.
" 500 tons but under 1,000 tons	$2\frac{1}{4}$	2	2
,, 1,000 ,, ,, 1,500 ,,	$2\frac{1}{2}$	$2\frac{1}{4}$	2
,, 1,500 ,, 2,000 ,,	3	$2\frac{3}{4}$	21/4
,, 2,000 ,, ,, 3,000 ,,	$3\frac{1}{2}$	3	$2\frac{1}{2}$
,, 3,000 tons and above	31	31	$2\frac{3}{4}$

In cases where more than one suction to any one compartment are connected to the pumps by a single pipe, this pipe should be not less than the size required for the centre suction.

COCKS, VALVES, AND SOIL PIPES.

Section 40. 1. All head and stern pumps if fitted are to be provided with sea-cocks fitted to the outside plating to the satisfaction of the Surveyors, and in places where they are at all times accessible.

2. Storm Valves.—Where soil or scupper pipes are attached to the outside plating below or near the Load Water Line, storm valves are to be fitted in substantial metal castings other than cast iron. The lower length of pipe should be of

galvanized iron or steel of substantial thickness, not less than standard steam pipe quality and thickness, or if of lead it must be efficiently cased with zinc. Where passing through cargo or bunker spaces the pipes are to be protected by a substantial casing, but wood casing is not to be used in coal bunkers.

CEMENT.

- Section 41. 1. The frames and plating of the bottom of all vessels to the upper parts of the bilges to be thickly and efficiently covered with Portland or other approved cement, which may be mixed with sand or other suitable substance. Care to be taken to have a proper thickness of cement at its termination, and to keep the watercourses clear all fore and aft. The whole to be to the satisfaction of the Surveyors.
- 2. Where asphalt, enamel cement, or similar compositions are to be used, the same must be sanctioned by the Owners, and samples are to be submitted for the approval of the Committee.

The condition of such compositions is to be ascertained by the Society's Surveyors biennially, and vessels coated with compositions as above described will be distinguished with a record of "Asp." in the Register Book.

CEILING.

- Section 42. 1. Close Ceiling. All vessels to be closely ceiled from the main keelson to the upper part of the bilges, the ceiling to be secured in such a manner as to be easily removed.
- 2. The ceiling on the floors of vessels not having double bottoms should be made in hatches where practicable, of convenient sizes, and when not so arranged to be fastened to the reversed angle bars or frames in such a manner as to be removed when required for the purpose of survey, or for cleaning and painting.
- 3. The ceiling on the double bottom of a cargo hold may be omitted, except under the hatchways and over the limbers at the bilges. If the ceiling is omitted under hatchways the tank top plating is to be increased '08 inch in thickness in way of the hatchways. Where the manhole covers in the double bottoms of cargo holds, or their fittings, project above the tank top, and the ceiling is

omitted, they must be protected by fitting an angle coaming around each manhole with a hatch either of wood or of steel fitted therein. Where the plating is protected with wood ceiling it should be $2\frac{1}{2}$ inches thick and laid on battens $1\frac{1}{2}$ inches thick, to admit of drainage water passing to the wells, or the ceiling may be laid on the top of the inner bottom embedded in a substantial covering such as Stockholm tar and cement. The ceiling on double bottoms to be removed when the tanks are required by the Rules to be tested.

- 4. Thickness.—The wood ceiling is to be 2 inches thick in vessels having a longitudinal number of 5,200 and under. In all larger vessels the ceiling is to be $2\frac{1}{2}$ inches in thickness.
- 5. Cargo battens to be fitted from the upper part of the bilges upwards, including the 'tween decks of all types of vessels, and in permanently enclosed spaces in bridges, poops and other deck erections. In spaces exclusively intended for carrying coal, cargo battens may be dispensed with.
- 6. Vessels carrying coal, ore or wood.—Vessels exclusively engaged in carrying coal, ore or wood need not have cargo battens fitted, but in each such case the certificate of classification will have the following words written on it, "Subject to the vessel being engaged exclusively in carrying coal, ore or wood, while without cargo battens."

STEERING GEAR. (See also Table 25.)

Section 43. 1. Rudder Stops.—Suitable stops for the rudder should be securely fastened to the deck in way of the tiller or quadrant tiller. Where a suitable brake is fitted to the tiller or quadrant tiller, or where the steering quadrant is geared direct on to the steam steering engine, the deck stops may be dispensed with. The stops of the steam steering engines should be fitted at a smaller angle of helm than the rudder stops, so as to prevent excessive strains consequent on a rudder being forced against its stops.

- 2. Spare Tiller.—Vessels which have not two independent steering gears are to have spare tiller and gear ready for use when required.
- 3. Independent Means of Steering.—Where combined hand and steam steering gear is adopted, and in which both gears depend upon the efficiency of a keyed quadrant or tiller, independent means of steering must be provided.

Steamers above 250 feet in length are to be fitted with two independent steering gears, one of which must be a steam or other mechanical steering gear, and it is recommended that the two controlling wheels of the mechanical gear should be placed one at the gear and the other one on the navigating bridge.

- 4. Protection of Steering Gear.—In steamers above 250 feet in length, not having full poops or awning or shelter decks, the after steering wheel and gear are to be protected by a substantially constructed iron or steel deck house or hood.
- 5. Springs or buffers are to be fitted to all steam steering gears of steamers.
- 6. Steering Chains or Rods.—The diameters of steering chains or rods are to be as given in Table 25 for the various diameters of rudder heads and the corresponding radii of quadrant tillers. Where the radius of quadrant or length of tiller adopted differs from that given in the Table, the diameter of steering chain is to be calculated from the following formula:—

$$d = .38 \sqrt{\frac{D^3}{R}}$$

where d = diameter of chain in inches;

D = diameter of rudder head in inches according to Table for rudder heads.

R = radius of quadrant or length of tiller at the centre of the chain in inches.

- 7. Leads of Steering Chains.—Care should be taken that the leads of the steering chains are made as direct as possible, sharp nips or bends being avoided.
- 8. The diameters at the centre of the chain of leading block sheaves are not to be less than sixteen times that of the steering chains, and the pins of the sheaves are not to be less than twice the diameter of the chains.

AWNING OR SHELTER DECK VESSELS AND VESSELS WITH PART AWNING DECKS.

Section 44. 1. In an awning or shelter deck vessel the transverse number is to be obtained from measurements taken to the deck next below the awning or shelter deck, provided the distance between these decks does not exceed 8 feet. Where the height of 'tween decks exceeds 8 feet the measurement is to be taken to a point 8 feet below the awning or shelter deck.

- 2. Freeboard a condition of Class.—It is a condition on which an awning or shelter deck, or part awning deck vessel is classed in the Society's Register Book that the freeboard assigned shall be marked on the vessel's sides as hereafter described.* The freeboard will also be inserted in the certificate of class and recorded in the Register Book. If the vessel proceed to sea with a less freeboard than that approved by the Committee, or if the freeboard mark be placed higher than the position assigned by the Committee, the vessel will be liable to have her class expunged from the Register Book.
- 3. Forfeiture of Class.—In all such cases, if the vessel has for any reason forfeited her class, the freeboard assigned as a condition of classification will be omitted in reprinting the Register Book, unless the class be previously reinstated.
- 4. Notation in Register Book.—Vessels to which this Section applies as regards an entire awning or shelter deck will be noted in the Register Book thus:—"Awng. dk." "Shelter dk." Those having a part awning deck will be noted "pt. Awng. dk."
- 5. Deck Erections on Awning or Shelter Deck.—When it is intended to fit erections on an awning or shelter deck, plans are to be submitted for the consideration of the Committee, showing the additional strengthening proposed to be fitted. Where a superstructure intended for passenger accommodation is to be built upon another superstructure, the deck beams above such accommodation are to be plated over in way of same.
- 6. Scantlings and Riveting.—The scantlings of the awning or shelter deck plating, side plating and stringer plates are to be as required by Table 18. The attachments and riveting of the butts, edges, &c., of the awning or shelter deck stringer and plating, sheerstrake and side plating are to be as required by Tables 19, 20, and 21, at an upper deck. The awning or shelter deck stringer angles are to be of the size given in Table 18 for upper deck stringer angles.
- 7. Framing.—All the frames are to extend to the awning or shelter deck stringer plate, and they are to be of the sizes given in Tables 2, 3, and 5, but in no case are they to be less than $3\frac{1}{2}$ × 3" × 30 inch. The reverse frames are to extend to the height required by Section 11.
- 8. Bulkheads and Casings.—The collision bulkhead is in all cases to extend to the awning or shelter, or partawning deck, the remaining bulkheads may stop at the deck

^{*} See Notes of Freeboard requirements printed at end of Rules,

next below, but a deep web frame or partial bulkhead is to be fitted on each side in the 'tween decks in continuation of each watertight bulkhead fitted below. Engine and boiler room hatchways on the deck next below awning or shelter, or part awning decks, to be enclosed by steel or iron trunk bulkheads efficiently strengthened, and extended from that deck to the awning or shelter or part-awning deck. (See Section 31, paragraphs 1 and 2.)

- 9. "Upper" Deck.—The deck below an awning or shelter deck, or part-awning deck, is to be laid and caulked. Coamings and hatches are to be fitted as to a weather deck, but the height of the coamings may be as required at the deck below an upper deck. (See Section 32.)
- 10. Deck Stringer to deck below awning or shelter deck.—This deck stringer plate is to be fitted and connected to the outside plating by angle bars between the frames of the size given in Table 17 for upper deck stringer angles in way of erections, and in addition, an inner stringer angle bar of the same size, passing continuously fore and aft, must be fitted inside the frames. The space between this angle bar and the outside plating all fore and aft, to be filled in and made watertight.

POOPS, BRIDGES, AND FORECASTLES.

Section 45. 1. "Short" Deck Erections.—In poops and forecastles, also in bridges not exceeding the lengths provided for in Table 17, the side plating, deck stringer plates and angles, tie plates and deck plating are to be of the scantlings required by that Table. The seams of the side plating may be single riveted except at the ends of the bridge, where they are to be double riveted for a length of about 20 feet. Where the bridge side plating is '46 inch or above in thickness the seams are to be double riveted throughout the bridge. The butts of the side plating should be not less than double riveted.

2. "Long" Bridges.—Where the length of bridge exceeds that provided for in Table 17 the scantlings of the bridge side plating, deck plating and stringer plates and angles are to be as required by Table 18. The attachments and riveting of the butts, edges, &c., of the bridge deck stringer and plating, sheerstrake and side plating are to be as required by Tables 19, 20, and 21. Where the seams of the side plating may not be required to be double riveted throughout, they must be double riveted for a length of about 20 feet at the ends of the bridge.

- 3. Framing.—All frames are to extend to the poop, bridge, or forecastle stringer plate. Partial bulkheads are to be fitted in bridges in way of large deck houses, also in continuation of watertight bulkheads fitted below, and at such other places as may be considered necessary by the Surveyor.
- 4. Reversed Frames in Forecastles.—In top-gallant forecastles of vessels whose longitudinal number is 14,000 and above, the alternate reversed frames are to extend to the forecastle deck, or other efficient means of strengthening the forecastle may be adopted if approved by the Committee.
- 5. Beams and Pillars.—The poop, bridge, and forecastle beams are to be of the sizes given in Table 12, and placed at every alternate frame. Where an iron or steel bridge deck is fitted, the beams are to be of the sizes given in Table 11, and placed at every frame unless the iron or steel deck is sheathed with wood, in which case the beams may be placed at alternate frames, except in vessels over 450 feet in length, when the beams are to be fitted at every frame whether the plating is sheathed or not. (For diameter of pillars, see Tables 14 and 15.)
- 6. Upper Deck Stringer Plate.—The upper deck stringer plate in way of the deck erections is to be fitted and connected to the sheerstrake by angle bars between the frames, of the size given in Table 17, and in addition an inner stringer angle bar of the same size passing continuously fore and aft must be fitted inside the frames. The space between this angle bar and the sheerstrake to be filled in and made watertight.
- 7. Wood Decks.—The wood decks of these erections are to be as stated in Section 26.
- 8. Strengthening at ends of Bridges and long Poops.—The upper deck sheerstrake is to be doubled its full breadth with plates not less than 20 feet in length and the stringer plate doubled or increased in thickness at the ends of a bridge. This additional strengthening is also required at the fore end of a poop or after end of a forecastle which exceeds one-fourth of the vessel's length. The bulwark plating at these parts is to be increased in thickness and supported by bracket plates; the freeing ports should have rounded corners and substantial rims, and the nearest stanchions to the ends of bridge or front of a long poop are not to be more than 5 feet from bridge or poop bulkhead and to be of additional strength, to the satisfaction of the Surveyors.

- 9. Superstructures.— Where a superstructure intended for passenger accommodation is to be built upon another superstructure, the deck beams above such accommodation are to be plated over in way of the same.
- 10. Vessel's Proportions.—All vessels having a length of $13\frac{1}{2}$ depths and above to the upper deck are to have a bridge extending over the midship half length of the vessel or such special compensation for extreme proportions as may be required by the Committee.
- 11. Poop and Bridge Bulkheads.—Bulkheads at the fore end of all bridges and poops are to be of the thickness required for the side plating of short bridges, but need not exceed '40 of an inch in thickness, with coaming plates '04 of an inch thicker than the bulkheads. Those erections extending over the engine and boiler or other deck openings, are to have the bulkheads stiffened with bulb angles of the sizes stated in subjoined Table.

Breadth of Ship.	Size of Bulb Angle Stiffeners.	Breadth of Ship.	Size of Bulb Angle Stiffeners.	
Feet. 24	Inches. $5 \times 3 \times 40$	Feet.	Inches. $7\frac{1}{2} \times 3\frac{1}{2} \times 56$	
30	$6 \times 3 \times 44$	50	$8 \times 3\frac{1}{2} \times 64$	
36	$7 \times 3 \times 50$	54	$8\frac{1}{2} \times 3\frac{1}{2} \times 64$	
42	7 × 3 × ·56	58 and above	$9 \times 3\frac{1}{2} \times 64$	

The stiffeners are to be spaced 30 inches apart, and connected both to the coaming plates and to the deck plating, or to an athwartship plate on the beams both below and above, with a bracket plate to each end of the bulb stiffener. Bulkheads at the fore end of poops not extending over engine and boiler, or other deck openings, to be stiffened with plain angles of the size required for frames in the fore and after peaks, spaced 30 inches apart. The bulkheads at the ends of all poops, bridges, and forecastles are to be placed over a deck beam.

12. Deck Erections on Small Vessels.—Where it is proposed to fit a poop, bridge, or top-gallant forecastle to a vessel whose moulded depth is less than 15 feet, plans showing the proposed additional transverse strengthening are to be submitted for the consideration of the Committee.

RAISED QUARTER-DECKS.

(See also Sketches on page 144.)

Section 46. 1. Framing and Side Stringers.—
The scantlings and arrangements of framing and side stringers

- in the way of a raised quarter-deck must be in accordance with the Rules for the increased depth of vessel, having regard to the position of the lowest tier of beams, as described in Section 2, paragraph 4.
- 2. Side Plating and Deck Stringers.—The scantlings of raised quarter-deck stringer, sheerstrake and strake below are to be as required by the Rules for a vessel of the depth and proportions to the raised quarter-deck.
- 3. Beams.—The size of beams of raised quarter-deck to be regulated as prescribed in Tables 11, 12, and 13.
- 4. Strengthening at Break.—The upper deck sheer-strake is to be extended for a reasonable distance abaft the break and to be doubled or increased in thickness in way of the same; except in the case of a raised quarter-dec l connected to a long bridge, when the raised quarter-deck sheerstrake is to be doubled or increased in thickness at the break. The bulwark plates of the raised quarter-deck adjoining the bridge side plating are to be increased in thickness and the upper deck sheerstrake is to be doubled at the front of the bridge.
- 5. Butt Connections.—The butts of the deck stringers and side plating throughout are to be arranged clear of each other and in way of the break the butts of the raised quarter-deck sheerstrake and two strakes of plating below the same are to be at least treble riveted. The upper deck stringer plate is to extend abaft the break about seven frame spaces, and the raised quarter-deck stringer plate about four frame spaces before the break, and the stringer plates below the upper deck are to have a shift of about 16 feet overlap; the bridge stringer also is to extend abaft the break.
- 6. Break Bulkhead.—The front or break bulkhead of the raised quarter-deck is to be of the thickness of the side plating required by Table 17 for short bridges. It is to be connected to the raised quarter-deck side plating by double angles, and is to be efficiently stiffened. An athwartship plate is also to be fitted, which will receive the deck ends, and be supported by bracket plates when it is not riveted to a beam. When the longitudinal number exceeds 15,000, or the vessel is over 13½ depths to length at upper deck, the break bulkhead is to be not less than four frame spaces abaft the after end of the engine room opening.
- 7. Overlap of Decks. —In vessels requiring by Table 18 a steel deck or part steel deck, the upper deck plating is to scarph the raised quarter-deck for a length of two to three

frame spaces, according to the size and proportions of the vessel, and the raised quarter-deck side plating is also to be doubled at this part for a length of from 18 feet to 20 feet. There are to be from four to five diaphragm plates fitted, of the thickness of the upper deck plating, connecting the two decks. They are to be attached to the decks and bulkhead by double angles, and stiffened by an angle on the after edges, also they are to be associated with web plates not less than 15 inches deep, fitted on the fore side of the bulkhead in the way of the same, and efficiently bracketed to the upper and bridge deck plating.

Where the longitudinal number is 18,200 and under 19,500, the main and raised quarter-decks are to be scarphed four frame spaces, and where the longitudinal number is 19,500 and above, five frame spaces. The webs on the fore side of the break bulkhead are to be not less than 18 inches deep. In such vessels the raised quarter-deck side plating is to be doubled, commencing at one-fourth the length of the vessel from the stern and extending to 8 feet beyond the break of the raised quarter-deck.

Vessels which from their size and proportions do not require the decks to be scarphed, are to have from four to five bracket knees fitted on each side of the break bulkhead, the thickness of which is not to be less than that of the upper deck plating.

SAILING VESSELS.

Section 47.—The foregoing requirements for steamers are also applicable to sailing vessels except as regards the following particulars:—

- 1. All the reversed frames are to extend to the upper deck in sailing vessels having more than one tier of beams.
- 2. Sailing vessels of 20 ft. and under 33 ft. moulded depth are to have at least one tier of beams, spaced not more than two frame spaces apart, below the upper deck.
- 3. Sailing vessels of 22 ft. and under 27 ft. moulded depth are to have a deep web frame, of the breadth and thickness of the stringer plate at second deck, fitted in way of each mast and connected to the outside plating with double angles. These web frames are to extend to the upper deck stringer plate.
- 4. Where the moulded depth is 27 ft. and under 33 ft., instead of the deep web frames prescribed in the preceding paragraph, partial bulkheads, as shown by the Sketch on page 145, are to be fitted in way of each mast.

- 5. Where a system of web frames as required by Section 13 is adopted, the web frames are to extend in all cases to the upper deck. Where the moulded depth is 22 ft. and under 27 ft., the web frames in way of the rigging of each mast are to be spaced not more than 4 frame spaces apart. Where, however, the moulded depth exceeds 27 feet, partial bulkheads are to be fitted as required by paragraph 4 of this section, when the web frames in way of the rigging may be of the ordinary spacing.
- 6. Panting Arrangements.—The stringer plates on all tiers of panting beams are to be of the breadth and thickness required by Table 17 for the second deck stringer plates at ends, and are to extend abaft the collision bulkhead for a length of not less than one-fourth the midship breadth of the vessel, attached to the outside plating and efficiently supported by brackets at alternate frames.

Sketches of panting arrangements are in all cases to be submitted for approval.

In sailing vessels of 20 ft. moulded depth and above panting beams and stringers are to be fitted at the after end.

- 7. Where the length of the midship beam is less than 30 feet, the upper and lower deck beams are to be $\frac{1}{2}$ inch deeper than given in Tables 11 and 12 for upper deck beams of the same length in steamers where one tier of beams only is fitted; and where the length is 30 feet and above, the upper, lower and orlop deck beams are to be one inch deeper than given in the Tables. The depths of the beam knees are to be correspondingly increased.
- 8. Where plate knees are not fitted the beam knees are to be "turned."
- 9. Outside Plating. The outside or overlapping strakes of plating for one quarter the length at the fore end should be reduced not more than '06 of an inch from the midship thickness. Where the longitudinal number is under 11,000 the sheerstrake is to be increased '06 of an inch in thickness, and where the longitudinal number is 11,000 or above it is to be increased '10 of an inch in thickness, in each case for \(\frac{3}{4}\text{ths the vessel's length amidships.}\) In addition, when the longitudinal number is 13,000 or above, three strakes of plating at the bilges are to be increased '06 of an inch in thickness throughout. When the longitudinal number is 17,000 and above, the strake of plating in way of the beams to second deck is to be increased '06 of an inch in thickness for one-half the vessel's length amidships.
- 10. In sailing vessels only the foremost or collision bulkhead will be required, and it is to be placed at not less than one-half the vessel's midship breadth abaft the stem at the lower deck.

- 11. Diagonal tie plates are to be fitted on the beams of all sailing vessels in way of the masts at the deck on which they are wedged; and, in addition, where the longitudinal number is 11,000 and above diagonal tie plates are to be fitted all fore and aft on the upper deck. Where diagonal tie plates cross each other, or the fore and aft tie plates between the beams, and a deck is to be laid thereon, one set of tie plates must be set down in way of the crossing, so as to leave one thickness only projecting above the beams. The diagonal tie plates are to be of the width and thickness given in Tables 17 and 18. They are to be well riveted to each other and to the beams and stringers.
- 12. Bulwark Stanchions.—The stanchions which support the bulwarks are not to be more than 5 ft. apart. Where stanchions are fitted on the butt straps of the bulwark plating, the straps are to be sufficiently broad to receive the spur in the middle of the stanchion, and the bulwark plating is to be doubled or fitted with vertical straps in way of the intermediate stanchions. The heel of each stanchion is to be attached by not less than four $\frac{7}{8}$ in. bolts, tapped through the stringer plate and secured with a nut and grommet. Their size may be from $1\frac{3}{8}$ in. to 2 in. in diameter, regulated by the length of the stanchion and the size of the vessel. Other forms of stanchion may be adopted, provided they be submitted for approval.
- 13. The mast rings in sailing vessels are to be formed of bulb angle of the size required by the Tables for frames in fore and after peaks.
- 14. The chain plates, rigging, &c., are to be in accordance with the requirements of Table 28.
- 15. Hand pumps only are required to be fitted to sailing vessels, and they are not to be of less size than required by Section 39, paragraph 7.

VESSELS NOT BUILT UNDER SURVEY.

Section 48. 1. In cases of vessels not surveyed while building, for which a character may be required application must be made to the Committee in writing, and such drawings, with scantlings of the vessel marked thereon, as may be obtainable, should be furnished, also particulars of the testing of the steel used in the construction of the vessel. The Committee will then direct a special examination to be made by two Surveyors of the Society (one of whom shall be an exclusive officer), for which

purpose the vessel is to be placed on high blocks in a dry dock or on ways; the hold to be cleared and proper stages made; the rivets and plating of keel, and flat of bottom, thoroughly examined; the close ceiling in the hold to be removed where deemed necessary, but in no case less than required for Special Survey No. 2. The coal bunkers of steam vessels to be cleared; the whole of the frames, stringers, hooks, floor-plates, keelsons, engine and boiler bearers, ends of beams, water-tight bulkheads, rivets, and inner surface of the plating exposed to view; all oxidation to be removed by being cut or beaten off the several parts above named, also from the outside plating, rivets, keel, stem, stern-post, and rudder.

In cases where the inner surface of the bottom plating is coated with cement or asphalt, if the coating be carefully inspected, and tested by beating or chipping and found sound and adhering satisfactorily to the steel, its removal may be dispensed with, provided that upon the removal of a portion, the plating, frames, and rivets under it be found in satisfactory condition.

- 2. When the vessel is so prepared, the Surveyors are to ascertain the scantlings of the various parts, and verify the particulars given on the drawings furnished, drilling the shell plating where deemed necessary for this purpose. A few rivets are to be removed from various parts to ascertain their quality and the character of the countersinking and workmanship. A full report is to be made on a first entry report form for the information of the Committee, who will then assign the vessel such character as the facts may appear to them to warrant.
- 3. In addition to the above, if the age of the vessel be ten years or upwards, the requirements of the Special Survey No. 3 are to be complied with. The periodical surveys are subsequently to be held as in the case of vessels built under survey.
- 4. In steam vessels the Engines and Boilers are to be opened out for Survey, at least to the extent required for the Special Surveys Nos. 1, 2, and 3. The Screw Shaft is to be drawn and examined. The arrangements of sea cocks, bilge suctions, valves, &c., are to be made to conform to the requirements of the Rules, and the working pressure of the boilers is to be determined from their actual scantlings in accordance with the Rules for the construction of boilers, and particulars should be furnished respecting the testing of the steel.

RULES FOR THE BURNING AND CARRYING OF LIQUID FUEL.

Section 49. 1. In vessels fitted for burning liquid fuel, the record "Fitted for liquid fuel" will be made in the Register Book.

- 2. The compartments for carrying oil fuel must be strengthened to efficiently withstand the pressure of the oil when only partly filled and in a seaway. They must be tested by a head of water extending to the highest point of the filling pipes or 12 feet above the load line, or 12 feet above the highest point of the compartment, whichever of these is the greatest.
- 3. If peak tanks or other deep tanks are used for carrying liquid fuel the riveting of these should be as required in the case of vessels carrying petroleum in bulk. The strengthening of these compartments must be to the Committee's satisfaction.
- 4. Each compartment must be fitted with an air pipe to be always open discharging above the upper deck.
- 5. Efficient means must be provided by wells and sparring or lining to prevent any leakage from any of the oil compartments from coming into contact with cargo or into the ordinary engine room bilges.
- 6. If double bottoms under holds are used for carrying liquid fuel, the ceiling must be laid on transverse battens, leaving at least 2 inches air space between the ceiling and tank top and permitting free drainage from the tank top into the limbers.
- 7. The pumping arrangements of the oil fuel compartments and their wells must be absolutely distinct from those of other parts of the vessel and must be submitted for approval.

If it is intended to sometimes carry oil and sometimes water ballast in the various compartments of the double bottom, the valves controlling the connections between these compartments and the ballast donkey pump, and also those controlling the suctions of the special oil pump, must be so arranged that the suctions for each separate compartment cannot be connected at the same time to both pumps.

- 8. No wood fittings or bearers are to be fitted in the stokehold spaces.
- 9. Where oil fuel compartments are at the sides of, or above, or below the boilers, special insulation is to be

fitted where necessary to protect them from the heat from the boilers, their smoke boxes, casings, &c.

- 10. If the fuel is sprayed by steam, means are to be provided to make up for the fresh water used for this purpose.
- 11. If the oil fuel is heated by a steam coil the condensed water should not be taken directly to the condensers but should be led into a tank or an open funnel mouth, and thence led to the hot well or feed tank.
- 12. The above arrangements are applicable only to the case of oil fuel, the flash point of which as determined by Abel's close test does not fall below 150° Fahrenheit.

EQUIPMENT.

Section 50. 1. All vessels having masts, spars, rigging, and sails shall be required to have them maintained in good order.

- 2. Every ship is to be provided with anchors, cables, &c., of approved quality, tested at a *public machine* recognised by the Committee, in number and length as set forth in Tables 30 and 31.
- 3. To entitle vessels classed A "For Channel Purposes" to the Figure 1, the equipment of Anchors and Chain Cables, &c., should be as required by Table 31, with the exception that not more than two bower anchors and one stream anchor need be supplied. The first bower anchor should be of the full weight required by the Table, and the second bower may be 15 per cent. lighter. This rule, however, applies only to vessels intended for short passages.
- 4. In vessels classed "For Channel Purposes" which are intended for longer voyages, such as the Queenboro'-Flushing, the Channel Islands, or the Irish Sea service, the equipment must be in accordance with the requirements of Table 31.
- 5. In the cases of foreign owned vessels classed with the Figure 1, in which the chains and anchors, or part of the same, have been tested under the inspection of the Society's Surveyors at Proving Establishments out of the United Kingdom recognised by the Committee, and test certificates of the same are furnished, duly signed by the Society's Surveyors and the Secretary, the vessel will have recorded in the Register Book the notation A.&C.P., A.P. or c.P. as the case may be. Where, however, the anchors or

cable for foreign owned vessels are manufactured abroad and test certificates are furnished setting forth that they have been tested at a Government machine, or at a machine under the control of a municipal body or a similar responsible body, but not under the inspection of a Surveyor to the Society, the record of A.&C.P., &c. will not be made in the Register Book, though such certificates will be accepted, as complying with the requirements of the Rules, for assigning the Figure 1, provided the remaining requirements of Tables 30 and 31 be complied with.

- 6. A certificate of all chains and anchors having been tested, and of the strain applied to them, must be produced before the ship is classed with the Figure 1.
- 7. Equipment Number.—The equipment as regards anchors, chains, warps, &c., is to be regulated by the number produced by the sum of the measurements in feet of the greatest moulded breadth of the vessel and the depth from the upper part of the keel to the top of the upper deck beams at side at the middle of the length, multiplied by the length of the vessel. In awning or shelter deck or part awning deck vessels, the measurement of depth defined above is to be taken to the deck next below the awning or shelter deck, provided the height between the decks does not exceed 8 feet. If the 'tween deck height exceeds 8 feet the measurement is to be taken to a point 8 feet below the awning or shelter deck. In turret deck vessels it is to be taken to the normal beam line at base of turret.

For a vessel having **erections** on deck the number obtained by the previous paragraph is to be increased as follows:—

For a raised quarter deck, add the product of the height and length in feet of the erection.

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For an awning or shelter deck, part awning deck, poop, bridge or forecastle, add three-fourths the product of the height and length in feet of such erections, 8 feet being taken as the maximum height for awning or shelter deck, or part awning deck erections.

For deck houses or other erections not extending to the side, but exceeding either in length or breadth half the rule breadth of the vessel, add one-half the product of the height and length of such erections.

Where erections are fitted upon erections the equipment number is to be correspondingly increased.

- 8. The equipment for Sailing and Steam Trawlers and Tugs is to be as given on back of Tables 30 and 31.
- 9. All vessels under 150 tons to be provided with one good boat; and every vessel of 150 tons and above to have a suitable number. The Surveyors are to be particular in examining and reporting the condition of the boats of all vessels.
- 10. Anchor Cranes and Boats' Davits to be in accordance with Table 29.
- 11. The efficient state and condition of the whole of a vessel's equipment will be designated by the Figure 1 placed after the character assigned to the vessel; and in cases in which the equipment is found insufficient in quantity or defective in quality, a dash thus—, will be inserted in place of the Figure 1. In cases where the Figure 1 is expunged on account of deficiencies in the anchors or chains, the record of Lloyd's A.&C.P. or A.&C.P. will also be expunged.

By order of the Committee,

ANDREW SCOTT,
Secretary.

RULES FOR THE CONSTRUCTION OF VESSELS INTENDED TO CARRY OIL IN BULK.

GENERAL.

Section 51. 1. The scantlings, arrangements and equipment, also the Rules for Special and other surveys and all requirements relating to vessels intended for the carriage of oil in bulk are to be as prescribed by the Society's "Rules for the construction of Steel Vessels," except where otherwise specified by the following Rules and Tables.

- 2. Submission of Plans.—In addition to the usual sketches of Midship Section, profile and deck plans, sketches are to be submitted showing the arrangement of oil tanks and cofferdams, the stiffening proposed for the transverse and longitudinal bulkheads, the construction of the tunnel and the bracket attachments at the ends of beams, stringers, webs, bulkhead stiffeners, &c.
- 3. Length of Oil Compartments.—The oil compartments are not to exceed from 24 feet to 28 feet in length.
- 4. Expansion trunks are to be fitted over the oil compartments of sufficient capacity to admit of the expansion or contraction of the oil due to changes of temperature. They are to be so arranged that the surface of the oil will not fall below the sides of the trunks when the vessel is rolling or pitching in a seaway. The breadth of the expansion trunk is not to exceed one-half the moulded breadth of the vessel, and where the height of the trunk exceeds eight feet above the top of the oil compartments the scantlings in way of the oil compartments are to be increased.
- 5. Cofferdams are to be fitted at the fore and after ends of the space intended for the oil cargo, and where the machinery is fitted amidships cofferdams are also to be fitted at each end of the machinery space in order that the oil cargo may be isolated from the holds and from the engine and boiler spaces. The cofferdams are to be not less than two frame spaces in length and are to extend from the keel to the top of the continuous expansion trunk for the full breadth of the vessel.

- 6. The number of watertight bulkheads extending to the upper deck is to be as required by Section 19.
- 7. Deck Erections.—In vessels having the machinery aft, a poop must be fitted of sufficient length to cover the machinery space. Where the engines are fitted amidships, the bridge is to be of sufficient length to overlap the ends of the middle line bulkhead in the oil compartments.
- 8. Cement.—Portland Cement may be dispensed with in compartments intended for carrying oil in bulk.
- 9. Testing.—Each oil compartment is to be filled separately with water and tested by pressure before the vessel is launched, or while in dry dock. The pressure is to be obtained by means of a head of water eight feet above the highest point of the expansion trunk. Cofferdams are to be tested by being filled with water to the top of the hatchway.
- 10. Electric light is to be fitted throughout on the double wire system.

WORKMANSHIP.

Section 52. 1. Owing to the penetrating character of the oil and the stresses to which oil vessels are subjected, due to the cargo being carried directly upon the outside plating of the vessel, it is of primary importance that the workmanship throughout be of the highest character.

- 2. The butts of plating to be planed and fitted close; the edges of the plating to be sheared from the faying surfaces, or the "burr" caused by shearing to be carefully chipped off, and all outside edges of plating are to be either planed or chipped fair. The butts and edges to be carefully caulked.
- 3. The riveting is to be of the most efficient character and the points of the rivets left full or convex. Special care is to be taken in the punching and countersinking of the holes and the fitting together of the various parts. Where any unfairness exists in the holes they are to be rimered, not

drifted, and larger rivets used in the rimered holes. The "burr" caused by punching, and all drillings and rimerings must be removed before the different parts are screwed together for riveting. Where the heads of the rivets are not laid up close to the plating or angle bars, or where rivets when tested are found unsatisfactory they are to be removed, not caulked. All oil-tight joints are to have the surfaces of steel plates fitted close to each other and caulked, without, as far as practicable, the use of canvas, &c.

- 4. In oil-tight work all angles are to be welded at the corners and neither mitred nor overlapped.
- 5. The angles attaching bracket plates to the bulk-heads are to extend along the bulkhead six inches beyond the points of the bracket plates. The bracket plates and angles are to be kept sufficiently clear of the bulkhead boundary bars to admit of the latter being efficiently caulked.
- 6. Where the boundary bars of oil-tight bulkheads consist of double angles, both flanges of each bar are to be caulked.

FLAT KEEL AND VERTICAL KEEL PLATES.

Section 53. 1. Flat plate keels are to be of the dimensions given in Table 17. The vertical keel plate forming the lowest strake of the middle line bulkhead is to be of sufficient breadth to admit of the seam at upper edge being above the upper end of the brackets attaching the floor plates to the bulkhead, and its thickness is to be '10 of an inch more than the thickness required by Table 33 for floor plates.

2. Keel Angles.—The angles connecting the vertical keel plates to the flat keel plates, are to be of the dimensions given in Table 34.

FRAMES AND REVERSED FRAMES.

Section 54. 1. The dimensions and spacing of the frames and reversed frames are to be as given in Table 32.

2. Bulb angle frames will not be required to extend to the middle line, provided they be carried down round the bilge and be scarphed to angle frames fitted at the lower edges of the floor plates. The scarphs are to be in length not less than six times the depth of the bulb angle frames and the butts are to be shifted on adjacent floors not less than the length of the scarph. In these cases the angle

frames are to be of the same thickness as the floors, and their flanges of the breadth required for the fore and aft flanges of frames by **Table 32**. The angle and bulb angle frames are to be fitted on opposite sides of the floor plates.

- 3. When bulb angle frames are extended to the middle line they are to have a lap of not less than $4\frac{1}{2}$ inches with the floor plates.
- 4. In all cases the frames are to be cut in way of the deck forming the top of the tanks.
- 5. The frames in the 'tween decks may be of angles '06 of an inch thicker than required by Table 32, in which case the reversed frames may be dispensed with, and they must be bracketed to the tank deck stringer at heel and to the beams above.
- 6. The brackets at the heels of the 'tween deck frames are to be of the same thickness as the frames, and are to be attached to the tank deck by double or single angles as required by **Table 36** for the attachment of bulkheads to tank deck. The brackets are to measure along each edge not less than five times the depth of the standing flange of the frames to which they are to be double riveted.
- 7. Web Frames in 'tween decks.—Web frames or partial bulkheads of the dimensions given in Table 32 are to be fitted in the 'tween decks in line with the bulkheads and web frames fitted below. They are to be stiffened at their inner edges by angle bars, or the plates may be flanged.
- 8. Reversed Frames on Floors.—A reversed frame is to be fitted at the upper edge of each floor plate, of the dimensions required for double angles at face of web frames by Table 32.
- 9. Height of Reversed Frames.—Where the intermediate frames are formed of frames and reversed frames riveted together, all reversed frames are to extend to the deck at the top of the oil compartments.

FLOOR PLATES.

Section 55. 1. The floor plates are to be of the dimensions given in Table 33, and are to extend in one length from the middle line bulkhead to the bilge.

2. Height of Floor Ends.—The floors may be either turned up at the bilge to a vertical height of not less than twice the midship depth of floor above top of keel throughout the oil compartments, or bracket plates of the thickness of the floors may be fitted at the bilge extending to the same height.

- 3. Moulding of Floor Plate.—The brackets at bilge are to be attached to the floor plates by means of a double riveted overlap not less in length inside the frame than the midship depth of floor; and the depth of the floor plate at three-fourths the half moulded breadth of vessel from middle line, or at the inner end of the bracket, is to be not less than three-fourths the depth of floor amidships. The upper edge of the floor is, however, at no part to fall below the level of the upper edge of the floor at middle line. The rivet attachment of the bracket to the frame bar is not to be less than that to the floor.
- 4. Bracket plates are to be fitted attaching the floor plates to the middle line bulkhead. They are to be of the thickness of the floors, and are to measure along each edge clear of the attachments not less than the midship depth of floor plate. The brackets are to be attached to the floors by double riveted overlaps, and the floors and brackets are to be attached to the middle line bulkhead on one side by double attachment angles, and on the opposite side by double angles consisting of the vertical stiffener on middle line bulkhead and a short attachment angle extending from the keel to beyond the point of the bracket.
- 5. The floor brackets both at middle line and bilge are to be stiffened at their inner edges by angle bars, or the bracket plates may be flanged.
- 6. The floor plates at the transverse bulkheads are to be increased to twice the Table depth and their thickness is to be as required by **Table 33**, but in no case less than that of the bulkhead plating to which they are attached.
- 7. The floor plates to which web frames are attached are to be at no part less in depth than the depth of the web frames.

SIDE AND BILGE KEELSONS.

Section 56. 1. Intercostal keelsons are to be of the scantlings given in Table 34. The intercostal plates are to be closely fitted between the floor plates and attached to the outside plating by angles of the size required by Table 32, these angles are to be double for a length of three frame spaces on each side of the bulkheads.

2. Number of Keelsons.—Two intercostal keelsons are to be fitted on each side where the moulded breadth of vessel amidships is less than 50 feet, and three where the breadth is 50 feet and under 64 feet. Where three keelsons are required each is to be fitted with a vertical plate of three-fourths the depth given in Table 34.

- 3. Attachment of Keelsons to Bulkheads.—The keelsons are to be cut at the transverse bulkheads, to which they are to be attached, by brackets of the thickness of the floor plates measuring not less than two frame spaces in length along each edge from the bulkhead and top of floor. They are to be connected to the bulkhead on one side by double attachment angles, and on the other side by the vertical stiffeners or webs on the bulkheads, with an additional attachment angle in the way of the brackets, see Sketch on page 148.
- 4. The keelson brackets are to be stiffened at their inner edges by angle bars, or the plates may be flanged.
- 5. Where it may be desired to modify the arrangements of floors and keelsons, alternative proposals are to be submitted for approval.

WEB FRAMES AND SIDE STRINGERS.

Section 57. 1. Web frames and side stringers are to be fitted throughout the oil compartments and machinery space, and are to be as given in Table 32. The web frames are to be spaced not more than four frame spaces apart, and the side stringers as required by the Table.

- 2. The web frames are to be attached to the floors by treble riveted overlaps, and their heads are to be attached to strong beams and brackets at the tank deck; they are to be continuous from the floors to the top of the oil compartments, the stringers being fitted intercostally.
- 3. Face angles of the dimensions given in Table 32 are to be fitted at the inner edges of the web frames and stringer plates. Those on the web frames are to extend along the upper edges of the floor plates to within the outer keelson. The face angles on the stringer plates are to be connected across the face of the webs by buttstraps of the dimensions given in Table 32.
- 4. Attachments.—The stringer plates are to be closely fitted between the web frames. The double angles connecting the stringers to the web frames, and the angles connecting the stringers and web frames to the outside plating, are to be of the size required by Table 32. Where the depth of web frames is 24 inches or above, the web frames are to be attached to the outside plating by double angles, or by equivalent single angles double riveted. The stringer plates are to be attached to the outside plating by double angles for a length of three frame spaces on each side of the bulkheads.
- Brackets under stringers.—Where the side stringers are 16 inches and above in depth they are to be supported

by bracket plates fitted midway between the web frames, efficiently riveted to the frames and connected to the stringer plates by single attachment angles.

- 6. Brackets to bulkheads.—The stringers are to be attached to the transverse bulkheads by large bracket knee plates of the thickness of the stringer plates, extending fore and aft for a distance of three frame spaces from the bulkhead, or inner edge of horizontal girder, and transversely for two frame spaces from the inner edge of the stringer plate. The brackets are to be attached to the stringer plates by double riveted overlaps and to the bulkheads, on one side by double attachment angles, and on the opposite side by a double riveted overlap to the horizontal stiffener on the bulkhead; an additional attachment angle is to be fitted connecting the horizontal stiffener to the bulkhead in way of the brackets. (See Sketch on page 150.)
- 7. The brackets attaching the stringer plates to the bulkheads are to be stiffened at their inner edges by angle bars, or the bracket plates may be flanged.

TRANSVERSE BULKHEADS TO OIL COMPARTMENTS.

Section 58. 1. The transverse oil-tight bulkheads are to be of the thickness given in Table 35, and are to extend to the top of the expansion trunk.

- 2. Boundary angles.—The bulkheads are to be attached to the outside plating, to the tank deck and to the sides and top of the expansion trunk by angles of the dimensions given in Table 36.
- 3. Bulkhead liners are to be fitted to the outer strakes of outside plating of sufficient length to take one row of rivets clear of the bulkhead frames, these rivets are to be closely spaced to admit of the ends of the liners being efficiently caulked.
- 4. Bulkhead stiffeners.—The bulkheads are to be supported by means of vertical bulb angle stiffeners and web plates and horizontal girders, of the dimensions given in Table 35. (See also Sketches on page 148.)
- 5. The vertical bulb angle stiffeners are to be spaced as required by Table 35, and their ends are to be kept sufficiently clear of the bulkhead boundary angles to admit of these being caulked.
- 6. The heels of the stiffeners are to be attached to the outside plating by bracket plates two frame spaces in length, and of a height equal to once and a half the depth of

- the floors measured from the outside plating, the floor plate adjacent to the bulkhead being dispensed with to admit of the brackets being fitted as described. The brackets are to be attached to the floor plates and outside plating by single attachment angles, and are to be of the thickness required by Table 33 for floor plates amidships. They are to be stiffened along their upper edges by angle bars, or the plates may be flanged.
- 7. The heads of the bulb angle stiffeners are to be attached to the under side of the tank deck plating, or to a shelf plate in way of expansion trunk by bracket plates one frame space in length and in depth.
- 8. Vertical web plates of the dimensions required by Table 35 are to be fitted, extending from the keelson brackets to the tank deck, or top of the expansion trunk. Two web plates are to be fitted on each side of the middle line where the breadth is under 50 feet, and three on each side where the breadth is 50 feet and under 64 feet. The webs are to be attached to the bulkheads by single attachment angles. Double angles are to be fitted attaching the heads of the webs to the tank deck plating, or shelf plate. The heels of the webs are to be attached to the keelson brackets as shown by Sketch on page 148. The inner edges of the web plates are to be stiffened by angle bars or the plates may be flanged.
- 9. Horizontal girders in number and dimensions as given in Table 35 are to be fitted in line with the side stringers and extending from the middle line bulkhead to the sides of the vessel. Where plate girders are fitted they are to be connected to the transverse bulkheads by single attachment angles. The ends of the girders are to be attached to the sides of the vessel by means of the side stringer brackets and to the middle line bulkhead by brackets of the thickness of the side stringer plates, extending fore and aft and athwartships for a distance of two frame spaces and arranged as shown in Sketch on page 150. The inner edges of the brackets are to be stiffened by angle bars, or the bracket plates may be flanged.
- 10. The vertical web plates and horizontal girders are to be supported by brackets to prevent them from tripping.
- 11. In the expansion trunk the transverse bulkhead is to be stiffened by vertical angles as required by Table 35, bracketed at head and heel.
- 12. It is recommended the bulkhead plating be fitted vertically with the edges of the plating between the vertical stiffeners.

COFFERDAMS.

Section 59. 1. The cofferdam bulkheads are to be of the same thickness, and are to be attached to the outside plating, decks, &c., as required for the transverse bulkheads to the oil compartments.

- 2. Bulkhead stiffening.—The bulkheads are to be stiffened by bulb angles of the same size and spacing as required for the bulkheads in the oil compartments. The two bulkheads forming a cofferdam are to be tied together at each of the vertical stiffeners by a series of plate stays efficiently riveted to the vertical stiffeners, and flanged on the upper and lower edges, as shown in Sketches on pages 146 and 147.
- 3. The keelsons and side stringers are to be continued in the cofferdams by plates of the same thickness as the floor plates and extending to the inner ends of the keelson and stringer brackets. The plates are to be connected to the outside plating by double angles, and to the cofferdam bulkheads by the vertical stiffeners and doubling angles, the inner edges of the plates are to be stiffened by angle bars, or the plates may be flanged.
- 4. The vertical bulb angle stiffeners are to be bracketed at their ends as required at the other transverse bulkheads. Where cofferdams do not exceed two frame spaces in length the floor in the cofferdam may be dispensed with provided the lower ends of the stiffeners be connected by fore and aft plates of the depth and thickness of the floor plates amidships. The beam at the upper part of the cofferdam may also be dispensed with, provided the upper ends of the stiffeners be connected by fore and aft plates similar to those at the lower ends, but of three-fourths the depth. These connecting plates at the upper and lower ends of the stiffeners are to have angle bars on their inner edges or the plates may be flanged; they are to be connected to the deck and outside plating by single attachment angles.

MIDDLE LINE BULKHEAD.

Section 60. 1. Throughout the oil compartments and cofferdams an oil-tight middle line bulkhead of the thickness required by Table 35 is to be fitted extending from the keel to the top of the expansion trunk. Beyond the cofferdams arrangements are to be made to avoid an abrupt termination of the strength by the fitting of large webs, brackets, etc.

- 2. Boundary Angles.—The middle line and transverse bulkheads are to be attached to each other by double angles $3\frac{1}{2}$ " \times $3\frac{1}{2}$ " for $\frac{3}{4}$ " rivets, and 4" \times 4" for $\frac{7}{8}$ " rivets, and of the same thickness as required for the double frame angles at sides of vessel. The middle line bulkhead is to be attached to the plating at top of expansion trunk by double angles of the same size as those at the top of transverse bulkheads.
- 3. Bulkhead stiffeners. The bulkhead is to be supported by means of vertical bulb angle stiffeners and web plates and horizontal girders, of the dimensions given in Table 35. (See also Sketches on page 149.)
- 4. The Vertical bulb angle stiffeners are to be spaced the same as the frames, and their lower ends are to be kept sufficiently clear of the keel angles to admit of these being caulked; they are to be attached to the floors and brackets by two rows of rivets. An additional attachment angle is to be fitted connecting the stiffener to the bulkhead in way of the floor plate and bracket. The stiffeners are to be attached at their heads to the bracket knees of beams crossing the expansion trunk at the tank deck, or be bracketed to a shelf plate fitted at the same height. Where a tunnel is fitted through the after oil compartments the vertical stiffeners are to be efficiently bracketed to the top of the tunnel.
- 5. Vertical web plates of the same thickness as the plating at lower part of bulkhead are to be fitted opposite the web frames at the sides of the vessel. Their depth at the heel is not to be less than that of the floors at middle line, and at the head not less than two-thirds that at the heel. The lower ends of the web plates are to be overlapped and double riveted to the floor plates and further attached by brackets of the same thickness and breadth as the web, double riveted to both the floor and the web. The inner edges of the brackets are to be stiffened by angle bars, or the plates may be flanged. The web plates are to be attached at the head, either by a double riveted lap and bracket to the strong beams crossing the trunk at the tank deck, or by double angles to a shelf plate fitted at the same height. The inner edges of the web plates are to be stiffened by angle bars, or the plates may be flanged. The webs are to be connected to the bulkheads by single attachment angles.
- 6. Where the vertical stiffeners and webs are fitted extending continuously from the keel to the top of the expansion trunk, the shelf plate at tank deck may be dispensed with on that side of the bulkhead.
- 7. Horizontal girders in number and dimensions as given in Table 35 are to be fitted in line with the horizontal girders on the transverse bulkheads. Where plate girders

are fitted they are to be attached to the middle line bulk-heads by single attachment angles. The ends of the girders are to be attached to the transverse bulkheads by brackets of the thickness of the side stringer plates extending fore and aft and athwartships for a distance of two frame spaces as shown in **Sketch** on page 150. The brackets are to be connected to the girders on one side of the transverse bulkhead by double riveted overlaps, and on the opposite side to the bulkhead plating by double attachment angles, or large single angle double riveted. The inner edges of the brackets are to be stiffened by angle bars or the bracket plates may be flanged.

- 8. The vertical web plates and horizontal girders are to be supported by brackets to prevent them from tripping.
- 9. In the expansion trunk the middle line bulkhead is to be stiffened by vertical angles as required by Table 35 spaced the same as the frames and bracketed at head and heel, and by web plates fitted in line with those below.

BEAMS.

- Section 61. 1. The deck beams are to be fitted at every frame at tank deck and decks above, also at top of expansion trunk. Their scantlings are to be regulated by the requirements of Table 11.
- 2. "Strong" beams of the dimensions required by Table 12 for "strong" hold beams, or equivalent thereto, are to be fitted at the heads of all web frames in the oil compartments extending from the middle line bulkhead to the sides of the vessel.
- 3. The strong beams are to be overlapped and well riveted to the web frames at the sides of the vessel, and the two are to be additionally connected by brackets of the same thickness as the web frames, the inner edges of the brackets being stiffened by angle bars, or the plates may be flanged. The breadth and depth of these knees are to be equal to the depth of the web frame, and they are to be measured from the lower edge of the beam and the inner edge of the web frame. The knees are to be double riveted in each arm.
- 4. The strong beams are to be connected to the middle line bulkhead by brackets similar to those at the sides of the vessel. On the one side of the bulkhead the brackets are to be connected to the vertical web plates by double riveted overlaps, and on the opposite side to the bulkhead plating by double attachment angles. The inner edges of the brackets are to be stiffened by angle bars, or the bracket plates may be flanged.

- 5. Where it may be desired to dispense with any of the strong beams in way of the expansion trunk on account of their interfering with the arrangement of hatchways leading to the oil compartments, plans showing the arrangements proposed with a view to providing equivalent strength are to be submitted for approval.
- 6. Shelf Plates.—One beam on each side of the transverse bulkheads is to be extended to the middle line bulkhead and to be attached thereto in the same way as at the sides of the vessel. The spaces between the transverse bulkheads and these adjacent beams are to be plated over in the expansion trunk.
- 7. The remainder of the beams are to extend within the sides of the expansion trunk sufficiently to admit of their ends being connected to the vertical stiffeners on the sides of the trunk by means of **bracket plates** of a breadth and depth equal to three times the depth of the beam. Any other efficient arrangement for obtaining the attachment at this part may be submitted for approval.
- 8. The beams of decks above the tank deck are to be cut at the sides of the expansion trunk and connected to the same by bracket plates, of the dimensions of beam knee brackets, and single attachment angles.
- 9. The beams at the top of expansion trunks are to be of upper deck size, efficiently bracketed at their ends to the sides of the expansion trunk and middle line bulkhead with plates of the dimensions of beam knee brackets.

PILLARS.

- Section 62. 1. Quarter pillars formed of double channel bars of the dimensions required by **Table 15** are to be fitted at each strong beam in the oil compartment. The quarter pillars are to be fitted practically in line with the sides of the continuous expansion trunk.
- 2. Where the trunk is not continuous, girders of the dimensions required by Table 16 are to be fitted under the tank deck at the heads of the pillars. Intercostal girders are also to be fitted to the decks above.
- 3. The pillars are to be attached at their heads to the beams or girders by large gusset plates; the lower ends of the pillars are to extend down and be well riveted to the floor plates and further attached by transverse gusset plates, double riveted, to the upper edges of the floors. The gusset plates are to be of the same thickness as the floor plates, their depth three times and their breadth five times the breadth of the channel bars.

OUTSIDE PLATING.

Section 63. 1. The thickness of the outside plating is to be as required by Tables 17 and 18.

2. The butts of outside plating are, so far as practicable, to be kept clear of the frame spaces adjacent to the oil tight bulkheads, and the plate edges are not to be joggled.

DECK PLATING AND STRINGERS.

Section 64. 1. The decks of vessels intended to carry oil in bulk are to be of steel of not less thickness than required by Tables 17 and 18, and in no case less than '30 of an inch. The thickness of tank deck plating and top of expansion trunk is not to be less than required by the following Table:—

	Longit	Minimum thickness.					
					inches.		
		Ţ	Inde	16,400	.30		
16	,400 8	and	unde	r 20,100	•32		
20	,100	,,	"	24,300	.34		
24	,300	,,	,,	27,100	.36		
27	,100	,,	"	29,900	.38		
29	,900	,,	,,	39,700	.40		
39	,700	"	"	43,900	.42		
43	,900	,,	"	48,100	•44		
48	,100	"	,,	50,000	•46		

- 2. The steel deck forming the top of the oil tanks is to be fitted continuously over the oil compartments and through the cofferdams.
- 3. The stringer angles at tank decks are to be of the dimensions given for flat keel angles in Table 34, but in no case less than required by Table 18.
- 4. Shelf plates, one frame space in breadth and of the thickness of the tank deck plating, are to be fitted inside the expansion trunks along each side of the middle line and transverse bulkheads at the height of the tank deck, and additional cross tie plating supported by beams is to be fitted to the satisfaction of the Committee. A single angle of the size required for lower deck stringer angles is to be fitted

along the inner edges of the shelf plates on the middle line bulkhead or the plates may be flanged.

5. All hatchways and deck openings are to have rounded corners and the deck plating is to be increased in thickness in way of the openings.

EXPANSION TRUNKS.

Section 65. 1. The plating forming the sides of the expansion trunks is to be of the thickness required by Table 36. It is to be stiffened by vertical angles, spaced the same as the frames, fitted inside the trunk and bracketed to the beams at head and heel. Vertical web plates, flanged on the inner edges and attached to the trunk plating by single attachment angles, are to be fitted opposite the web frames at the sides of the vessel. The vertical stiffeners and web plates are to be of the dimensions given in Table 36.

- 2. The side plating of the trunks is to be attached to the tank deck plating by single angles having flanges of the breadth required for the tank deck stringer angles and '06 of an inch less in thickness. The trunk side plating is to be attached to the upper deck plating, or top of expansion trunk, by single attachment angles.
- 3. Where expansion trunks are continuous, the sides of the same are to be carried through all cofferdams except the forward one, and also through the after one when the engines are fitted amidships.
- 4. Where the expansion trunks are not continuous, the plating and stiffening of the ends of the short trunks are to be at the sides as required by **Table 36** and the corners of the trunks are to be of rounded form.
- 5. Small hatchways in the top of expansion trunks are to be fitted with hinged plate covers capable of being made oil tight. A 6 inch screw plug is to be fitted in the cover to each tank, also a gas cock to admit of the release of gas from the tanks without opening the covers.
- 6. Where large cargo hatchways are fitted in the top of expansion trunks, sketches of the oil tight covers proposed to be fitted, also of the arrangements of strong beams and cross tie plating at the tank deck in way of the hatchways, are to be submitted for approval.

SUMMER TANKS.

Section 66. In cases where "summer tanks" are fitted in the 'tween decks they are to be constructed and tested as required for the ordinary oil compartments and efficient arrangements are to be made for the expansion of the oil.

ENGINE AND BOILER SPACE.

Section 67. 1. The scantlings and arrangements of web frames and side stringers in the machinery space are to be similar to those in the oil compartments.

- 2. The sides of continuous expansion trunks are to be carried through the machinery space to form the casings of the engine and boiler openings; or to be efficiently overlapped with the same. The coaming plates of the casings are to extend below the deck at least twice the depth of the strong beams and to be fitted with double angles at the lower edge. They are to be incorporated with the deep web plates or large brackets at the bulkheads. The through beams in the machinery space are to be cut at the coamings and attached to the same by gusset plates and brackets.
- 3. Where a double bottom is fitted in the machinery space, care is to be taken to provide against an abrupt termination of the longitudinal strength at the bulkheads, by the fitting of webs, or large brackets, in way of the keelsons.

TUNNEL.

Section 68. 1. When engines are situated amidships, a shaft tunnel is to be fitted through the after oil compartments. It is to be entirely separated from the engine room by means of a cofferdam.

- 2. There is to be a **trunkway** at each end, leading from the upper deck to the tunnel, to afford means of readily entering and leaving the same. The trunkway at the forward end is to be abaft the cofferdam.
- 3. Construction.—The tunnel is to be circular in form and constructed of plating '06 of an inch thicker than required by Table 33 for floor plates amidships. It is to be attached to the middle line bulkhead above and below and to the transverse bulkheads by double angles of the size required for the angles attaching middle line and transverse bulkheads (Section 60, paragraph 2). A stiffening angle of the size required for flat keel angles is to be fitted round the outside of the tunnel in way of each web plate on middle line bulkhead. These angles are to be efficiently bracketed to the middle line bulkhead at upper part of tunnel and to the middle line bulkhead and floors at lower part. Efficient plate bearers are also to be fitted under the tunnel in way of the tunnel stools. Where horizontal girders on the transverse bulkheads are cut by the tunnel, their ends are to be connected to the tunnel plating by large plate brackets as to the middle line bulkhead,

RIVETING.

Section 69. 1. The riveting is to be of the most efficient character and the points of the rivets left full or convex. Special care is to be taken in the punching and countersinking of the holes and the fitting together of the various parts. Where any unfairness exists in the holes they are to be rimered, not drifted, and larger rivets used in the rimered holes. The "burr" caused by punching, and all drillings and rimerings must be removed before the different parts are screwed together for riveting. Where the heads of the rivets are not laid up close to the plating or angle bars, or where rivets when tested are found unsatisfactory they are to be removed, not caulked. All oil tight joints are to have the surfaces of steel plates fitted close to each other and caulked, without, as far as practicable, the use of canvas, &c.

- 2. The butts of flat keel plates are to be double strapped and treble riveted, the butts of the vertical keel plates over-lapped and treble riveted, and the flanges of the flat keel angles double riveted.
- 3. The seams and butts of the plating of the middle line and transverse bulkheads of the oil compartments, cofferdams and expansions trunks are to be double chain riveted; the flanges of single bulkhead frames and the transverse flange of the larger of the two bulkhead frames where doubles frames are fitted are also to be double riveted.
- 4. The seams of outside plating in way of the oil compartments are not to be less than double chain riveted with an additional pair of rivets in each frame space beyond the number required by Table 20. In vessels of 450 feet and under 475 feet in length three seams of outside plating on each side between the bilge and tank deck are to be treble riveted between the peak bulkheads, in vessels of 475 feet and under 500 feet four seams, and in vessels 500 feet to 550 feet all the seams from the bilge to the tank deck are to be treble riveted.
- 5. The butts of outside plating in way of the oil compartments are not to be less than treble riveted and are to be either overlapped or double strapped. Double straps are to be fitted to the butts of the strake of outside plating in way of the deck forming the top of the tank, and all vessels of 380 feet and above in length are to have double straps fitted to the butts of the sheerstrake. In vessels of 380 feet and under 400 feet in length double straps are to be fitted to the butts of the plating forming the flat of the

bottom, in vessels of 400 feet and under 450 feet double straps are to be fitted to the butts of the bottom and bilge plating, and in vessels of 450 feet to 550 feet in length double straps are to be fitted to the butts of all outside plating for three-fourths the vessel's length amidships.

- 6. The butts of the deck stringer plates are to be not less than treble riveted and must be overlapped or double strapped. Where the stringer plates are '60 of an inch and above in thickness double straps are to be fitted to the butts. The flanges of the deck stringer angles and the angles attaching the sides of the expansion trunk to the tank deck are to be double riveted.
- 7. The seams and butts of the deck plating forming the top of the oil compartments are not to be less than double chain riveted. When the deck plating is '46 of an inch or more in thickness the butts of the same are to be treble riveted.
- 8. The seams and butts of the plating forming sides and top of expansion trunk are to be not less than double chain riveted.
- 9. The seams and butts of tunnel plating are to be double chain riveted, and the flanges of the tunnel stiffeners double riveted to the tunnel plating, web plates and brackets.
- 10. Spacing of rivets.—The rivets in the various parts are to be spaced as follows, viz.:—

3½ diam.
 C. to C.

In butts of flat and vertical keel plates, butts of all outside plating and deck stringer plates, seams and butts of tank deck plating and middle line and transverse bulkheads, sides and top of expansion trunk and tunnel plating.

4 diam. C. to C. In flat keel angles, boundary bars of bulkheads, tank deck stringer angles and angles at upper and lower corners of expansion trunks.

5 diam. C. to C. In bracket knee plate attachments to floor plates, side stringers and bulkhead stiffeners.

6 diam. C. to C. In frames, reversed frames, floors, keelsons, face angles on web frames and side stringers, bulkhead stiffeners, web plates and girders, expansion trunk stiffeners, tunnel stiffeners and deck plating and top of expansion trunk to beams.

- 11. Wherever the frames, beams or stiffeners to bulk-heads and expansion trunks cross the seams or butts of the plating, two rivets are to be fitted through the plating and bars.
- 12. Attachment Angles. The breadths of the flanges of attachment angles are to be as follows:—

for $\frac{5}{8}$ inch and $\frac{3}{4}$ inch rivets ... 3 inches.

for $\frac{7}{8}$ inch rivets... ... $3\frac{1}{2}$,,

for 1 inch rivets... ... 4 ,,

the angles are to be of the mean thickness of the plates they attach.

PUMPING ARRANGEMENTS.

Section 70. 1. Oil pumps fitted for the purpose of filling or discharging the oil compartments are to be kept entirely separate from the pumps fitted for filling or clearing the water ballast compartments of water.

- 2. The water ballast pipes are not to pass through the oil compartments, nor the pipes for the oil through any water ballast spaces. A separate ballast pump is to be fitted forward of the oil compartments for the purpose of filling and clearing the forward ballast tanks.
- 3. Oil pump rooms are to be enclosed by watertight bulkheads and have no direct communication with the machinery space.
- 4. The **limber holes** in the floors and intercostals in the oil compartments are to be so arranged in the vicinity of the pumps as to admit of a sufficient flow of oil to the pump suctions.
- 5. Efficient arrangements are to be provided for clearing the tunnel and 'tween deck spaces of water.
 - 6. Sounding pipes are to be fitted in the cofferdams.

VENTILATION.

Section 71. 1. It is of the greatest importance in oil carrying vessels that the internal arrangements should be such that the compartments can be readily cleared of gas, and efficient means are to be provided for clearing the dangerous gases from the tanks by the injection of steam or by the adoption of some efficient system of artificial ventilation.

2. Ventilators are to be fitted to the pump rooms, cofferdams, 'tween decks, deck erections and other enclosed spaces, to allow of the free escape of all gases from these parts.

3. The tunnel is to be efficiently ventilated by large ventilators placed on the upper part of the trunks at the ends of the tunnel.

ELECTRIC LIGHTING.

Section 72. 1. The single wire system must not be adopted for any part of the insulation in vessels carrying petroleum.

2. Switches and cut-outs must not be fitted in places liable to the accumulation of petroleum vapour or gas, and all lamps in places where it is possible for gas to accumulate must be made with an outer glass globe made airtight. All wires in such places are to be lead covered, or the insulation of the cables employed is to be of such a nature as not to be affected by petroleum.

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3. No joints of cables, switches, or cut-outs, should be fitted in the pump rooms, but the wires for each lamp therein should be carried to the lamp from a distributing junction box placed outside the pump room or companion.

PERIODICAL SURVEYS.

Section 73. 1. Preparation of Tanks.—When vessels classed for carrying oil in bulk are undergoing special survey, the tanks are to be cleaned out and thoroughly cleared of gas to admit of their being properly examined, and every precaution is to be taken to ensure safety during inspection.

2. **Testing.**—Each oil compartment and cofferdam is to be tested by being filled with water to the top of the hatchway in the expansion trunk or cofferdam.

By order of the Committee,

ANDREW SCOTT,

Secretary.

RULES

FOR THE

SURVEY AND CONSTRUCTION OF ENGINES AND BOILERS OF STEAM VESSELS.

Section 1. In steam vessels, the machinery and boilers are to be inspected throughout construction, the boilers tested by hydraulic pressure, and the machinery tested under steam by the Society's Engineer-Surveyors, who will furnish a report to the Committee describing them in the manner shown in form No. 4. If found satisfactory, the Committee will thereupon grant a certificate, and insert in the Register Book the notification, "LMC" in red (i.e. "LLOYD'S MACHINERY CERTIFICATE"), indicating that the machinery and boilers are certified to be in good order and safe working condition.

SPECIAL SURVEY OF NEW ENGINES OR BOILERS,

- Section 2. 1. In steam vessels built under Special Survey, the Machinery and Boilers must also be constructed under Special Survey.
- 2. In cases of machinery or new boilers being built under Special Survey, the distinguishing mark # will be noted in red, thus: "#LMC," or "#NE & B," or "#NB."
- 3. In order to facilitate this inspection, the plans of the machinery and boilers are to be examined, and from them the working pressure fixed.
- 4. The Surveyors are to examine the materials and workmanship from the commencement of the work until the final test of the machinery under steam; any defects, &c., to be pointed out as early as possible.
- 5. The Surveyors may also, if desired, compare the work as it progresses with the requirements of the specification agreed upon by the parties concerned, and certify to the conditions thereof, as far as can be seen, being satisfactorily complied with.

BOILERS.

- Section 3. 1. The Surveyors will be guided in fixing the working pressure by the tables and formulæ annexed. (See Section 11.)
- 2. Any novelty in the construction of the machinery or boilers to be reported to the Committee.
- 3. The boilers, together with the machinery, to be inspected at different stages of construction.

All the holes in steel boilers should be drilled, but if they be punched the plates are to be afterwards annealed.

All plates that are dished or flanged, or in any way heated in the fire for working, except those that are subjected to a compressive stress only, are to be annealed after the operations are completed.

No steel stays are to be welded.

Unless otherwise specified, the Rules for the construction of iron boilers will apply equally to boilers made of steel.

- 4. The boilers to be tested by hydraulic pressure, in the presence of the Engineer-Surveyor, to twice the working pressure, and carefully gauged while under test.
- 5. Two safety valves to be fitted to each boiler, and loaded to the working pressure in the presence of the Surveyor. In the case of boilers of greater working pressure than 60 lbs. per square inch, the safety valves may be loaded to 5 lbs. above the working pressure. If common valves are used their combined areas to be at least half a square inch to each square foot of grate surface. If improved valves are used they are to be tested under steam in the presence of the Surveyor; the accumulation in no case to exceed 10 per cent. of the working pressure.
- 6. An approved safety valve also to be fitted to the super-heater.

- 7. In winch boilers one safety valve will be allowed, provided its area be not less than half a square inch per square foot of grate surface.
- 8. Each valve to be arranged so that no extra load can be added when steam is up, and to be fitted with easing gear which must lift the valve itself. All safety-valve spindles to extend through the covers and be fitted with sockets and cross handles, allowing them to be lifted and turned round in their seats, and their efficiency tested at any time.
- 9. Stop-valves to be fitted so that each boiler can be worked separately.
- 10. Each boiler to be fitted with a separate steam gauge, to accurately indicate the pressure.
- 11. Each boiler to be fitted with a blow-off cock independent of that on the vessel's outside plating.
- 12. The machinery and boilers are to be securely fixed to the vessel to the satisfaction of the Surveyor.

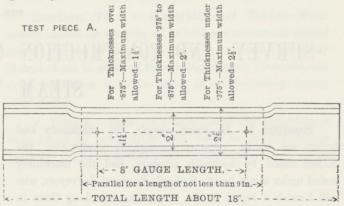
QUALITY AND TESTING OF BOILER STEEL.

Section 4. 1. When steel is used in the construction of boilers intended for vessels classed or proposed for classification in the Society's Register Book, the boilers shall be constructed in accordance with the requirements of the Rules, and the following conditions be fulfilled:—

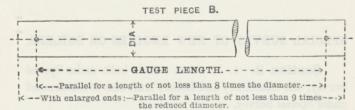
- 2. Process of Manufacture.—Steel for Marine Boilers shall be made by the Open Hearth process, acid or basic.
- 3. Freedom from Defects.—The finished material shall be free from cracks, surface flaws, and lamination. It shall also have a workmanlike finish, and must not have been hammer-dressed.
- 4. Testing and Inspection.—The following tests and inspections shall be made at the place of manufacture prior to despatch; but, in the event of any of the material proving unsatisfactory in the course of being worked into boilers, such material shall be rejected, notwithstanding any previous certificate of satisfactory testing, and such further tests of the material from the same charge may be made as the Surveyor may consider desirable.
- 5. Tensile Test Pieces.—The tensile strength and ductility shall be determined from Standard test pieces cut lengthwise or crosswise from the rolled material. When material is annealed or otherwise treated before despatch, the test pieces shall be similarly and simultaneously treated with the material before testing.

Plates, Angles, and Tee Bars:—Wherever practicable the rolled surfaces shall be retained on two opposite sides of the test piece. The elongation shall be measured on a Standard test piece having a gauge length of 8 inches.

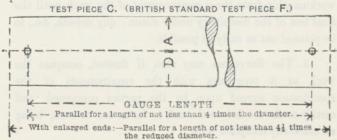
For material more than '875 in. in thickness the width of the test piece between the gauge points shall not exceed $1\frac{1}{2}$ ins.; for material '875 in. to '375 in. in thickness, inclusive, the width shall not exceed 2 ins.; for material less than '375 in. in thickness the width shall not be more than $2\frac{1}{2}$ ins. In other respects the test pieces shall conform generally to the Standard test piece A.



Round Bars:—Round bars may be tested either full size as rolled, or turned down when the diameter is considerable. The test piece shall have a gauge length of not less than 8 times its diameter, and a sectional area of not less than $\frac{1}{4}$ square inch. When enlarged ends are used the length of the parallel portion shall not be less than 9 times the reduced diameter, see Standard test piece B.



Where bars are above one inch diameter, and are tested full size as rolled, or have been turned down and the resulting test piece is above one inch diameter, a gauge length of 4 times the diameter may be used if preferred by the Manufacturer, in which case an increased elongation will be required, as specified in paragraph 7. When enlarged ends are used, the length of the parallel portion shall be not less than $4\frac{1}{2}$ times the reduced diameter, see Standard test piece C.



Any straightening of test pieces which may be required shall be done cold.

- 6. Mechanical Tests and Selection of Test Pieces.— Plates and bars for boilers shall comply with the following mechanical tests. All test pieces shall be selected by the Surveyor and tested in his presence, and he shall satisfy himself that the conditions herein described are fulfilled.
- 7. Tensile Tests. Plates:—The tensile breaking strength of steel plates for shells and girders, determined from Standard test pieces, shall be between the limits of 28 and 32 tons per square inch. For plates intended for flanging or welding, and for combustion chambers and furnaces, the tensile breaking strength shall be between the limits of 26 and 30 tons per square inch. In the case of material for purposes in which tensile strength is not important, the tensile test may be dispensed with and the bend test only be made, if so specified by the builders and approved by the Committee. The elongation, measured on a Standard test piece having a gauge length of 8 ins., shall not be less than 20 per cent. for material of '375 in. in thickness and upwards required to have a tensile breaking strength of 28 to 32 tons per square inch; and not less than 23 per cent. for material of '375 in. in thickness and upwards required to have a tensile breaking strength of 26 to 30 tons per square inch.

Stay, Angle and Tee Bars:—The tensile breaking-strength of longitudinal stays and angle and tee bars shall be between the limits of 28 and 32 tons per square inch, with an elongation of not less than 20 per cent. of the gauge length measured on the Standard test piece A or B, or 24 per cent. measured on the Standard test piece C. For bars for combustion chamber stays the tensile breaking strength shall be between 26 and 30 tons per square inch, with an elongation of not less than 23 per cent. of the gauge length measured on the Standard test piece B, or 28 per cent. measured on the Standard test piece C.

For material under '375 in. in thickness the elongation may be not more than 3 per cent. below the above-named elongations.

Rivet Bars:—The tensile breaking strength of rivet bars shall be between the limits of 26 and 30 tons per square inch of section, with an elongation of not less than 25 per cent. of the gauge length measured on the Standard test piece B, or 30 per cent. measured on the Standard test piece C. The bars may be tested the full size as rolled.

8. Number of Tensile Tests. Plates.—One tensile test shall be taken from each plate as rolled. For plates exceeding $2\frac{1}{2}$ tons in weight one tensile test shall be taken from each end.

Angle, Tee, Rivet and Stay Bars:—At least two tensile tests for angle bars, tee bars, rivet bars, and stay bars shall be taken from each charge; but when the number of the bars, as rolled, from one charge exceeds 15, an additional tensile test shall be made for each further batch of 15 bars or portion thereof. In round bars of $1\frac{3}{4}$ inch diameter and under, the number shall be 50 in place of 15.

Should a tensile test piece break outside the middle half of its gauge length, and the elongation be less than that required by the Rules the test may, at the Maker's option, be discarded and another test be made of the same plate or bar.

9. Bend Tests. Cold Bends:—Test pieces shall be sheared lengthwise or crosswise from plates or bars, and shall not be less than $1\frac{1}{2}$ ins. wide, but for small bars the whole section may be used. For rivet bars bend tests are not required.

Temper Bends:—The test pieces shall be similar to those used for cold bend tests. For temper bend tests the samples shall be heated to a blood red and quenched in water at a temperature not exceeding 80 degrees Fahr. The colour shall be judged indoors in the shade.

In all cold bend tests, and in temper bend tests on samples 5 in. in thickness and above, the rough edge or arris caused by shearing may be removed by filing or grinding, and samples 1 in. in thickness and above may have the edges machined, but the test pieces shall receive no other preparation. The test pieces shall not be annealed unless the material from which they are cut is similarly annealed, in which case the test pieces shall be similarly and simultaneously treated with the material before testing.

For both cold and temper bends the test piece shall withstand, without fracture, being doubled over until the internal radius is equal to $1\frac{1}{2}$ times the thickness of the test piece, and the sides are parallel.

For small sectional material these bend tests may be made from the flattened bar.

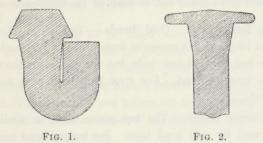
Bend tests may be made either by pressure or by blows.

10. Number of Bend Tests. Plates:—One cold or temper bend test shall be taken from each plate as rolled. For plates exceeding $2\frac{1}{2}$ tons in weight one bend test shall be taken from each end—one bend test to be temper and the other cold.

Angle Bars:—A cold or a temper bend test shall be made from each angle bar rolled.

Stay Bars:—A cold and temper bend test shall be made from every 15 stay bars as rolled from each charge.

- 11. Tests for Manufactured Rivets.—Rivets selected by the Surveyor from the bulk shall withstand the following tests:—
 - (a) The rivet shanks are to be bent cold, and hammered until the two parts of the shank touch in the manner shown in Fig. 1, without fracture on the outside of the bend.
 - (b) The rivet heads are to be flattened, while hot, in the manner shown in Fig. 2, without cracking at the edges. The heads are to be flattened until their diameter is $2\frac{1}{2}$ times the diameter of the shank.



- 12. Additional Tests before Rejection.—Should any of the test pieces first selected by the Surveyor not fulfil the test requirements, two further tests may be made from the same plate or bar, but should either of these fail, the plate or bar from which the test pieces were cut shall be rejected. In all such cases further tests shall be made before any material from the same charge can be accepted.
- 13. Branding.—Every plate and bar shall be clearly and distinctly marked by the Maker in two places with the Society's brand, thus:—indicating that the material has complied with the Society's tests.

No plates or bars bearing this brand shall be forwarded from the Steel Works until the prescribed tests have been made by the Surveyor, and the mill sheets have been signed by him. All plates and bars shall also be legibly stamped in two places with the Maker's name or trade mark, and the place where made. They shall also be stamped with numbers or identification marks by which they can be traced to the charge from which the material was made.

- 14. Maker's Certificate.—Before the mill sheets are signed by the Surveyor, the Maker shall furnish him with a certificate guaranteeing that the material has been made by the Open Hearth process, and that it has been subjected to, and has withstood satisfactorily, the tests above described in the presence of the Surveyor. The following form of certificate will be accepted if printed on each mill sheet with the name of the firm, and initialled by the Test House Manager:—
 - "We hereby certify that the material described below has been made by the Open Hearth process, and

- is that which has been satisfactorily tested in the presence of the Surveyor in accordance with the Rules of Lloyd's Register."
- 15. Defacing of Rejected Material.—In the event of the material failing, in any case, to withstand the prescribed tests, the Surveyor shall see that the Society's brand stamped on the plates and bars by the Maker has been defaced by punch marks extending beyond the brand in the form of a cross, thus:— denoting that the material has been rejected.
- a system of marking the ingots, billets, slabs, plates, bars, &c., which will enable all finished material to be traced to the original charge, and the Surveyor must be given every facility for tracing all plates and bars to their respective charges, and for witnessing the required tests. When he is satisfied with the material and with the results of the tests, he shall be furnished with two copies of the advice notes of the material for his signature, one of which is to be forwarded by the manufacturer to the Boiler Maker, and the other is to be forwarded by the Surveyor to the Surveyors at the port where the boiler is to be built.
- 17. Steel not produced where Rolled.—Where steel is not produced in the works at which it is rolled, a certificate shall be supplied to the Surveyor, stating the Open Hearth process by which it was made, the name of the Steel Maker who supplied it, also the numbers of the charges for reference to the books of the Steel Maker. The number of the charge shall be marked on each ingot or billet for the purpose of identification, and the finished plates and bars shall also be legibly stamped in two places with the Maker's name or trade mark, and the place where made. They shall also be stamped with numbers or identification marks by which they can be traced to the charge from which the material was made.
- 18. General.—Besides the foregoing tests, samples of all material may be subjected to additional tests at the discretion of the Surveyors.
- 19. In cases wherein it may be desired by Owners and Builders, consideration will be given by the Committee to proposals for the use of steel of other tenacity than is provided for in the foregoing Rules.

QUALITY AND TESTING OF STEEL CASTINGS.

Section 5. 1. Process of Manufacture.—Steel for castings shall be made by the Open Hearth process, Acid or Basic, or by such other process as may be approved by the Committee.

- 2. Annealing.—All steel castings shall be thoroughly annealed in a properly constructed annealing furnace, which must permit of the whole casting being uniformly raised in temperature throughout its whole extent to the necessary intensity required for annealing purposes. The casting shall be allowed to cool down prior to removal from the annealing furnace; and if subsequently heated for any purpose it shall again be similarly annealed if required by the Surveyor.
- 3. Testing and Inspection.—The following tests and inspections shall be made, preferably at the place of manufacture prior to despatch, but in the event of any casting proving unsatisfactory in the course of preparation or erection, such casting shall be rejected notwithstanding any previous certificate of satisfactory testing.
- 4. Tensile and Bend Test Pieces.—The tensile strength and ductility shall be determined from standard test pieces, which are to be prepared from sample pieces cast on the casting. These sample pieces are not to be cut or partially cut from the castings until the annealing of such castings has been completed, nor until they have been stamped by the Surveyor. The test pieces are to be stamped by the Surveyor after the annealing. All test pieces shall be selected by the Surveyor and tested in his presence, and he shall satisfy himself that the conditions herein described are fulfilled.
- 5. Number of Tests.—At least one tensile test and one cold bend test are to be taken from each casting. In castings of complex design, referred to in paragraph 12, at least two tensile and two cold bend tests are to be taken. Where a casting is made from more than one charge of steel, at least four tensile and four cold bend tests are to be taken from pieces cast as far apart as possible on the casting, some test pieces being taken from as near the top, and others from as near the bottom of the casting as practicable.
- 6. Dimensions of Tensile Test Pieces.—The tensile test pieces are to be turned so as to have a diameter of $\cdot 564$ inch with a gauge length of 2 inches, or a diameter of $\cdot 798$ inch with a gauge length of 3 inches, or a diameter of $\cdot 977$ inch with a gauge length of $3\frac{1}{2}$ inches.
- 7. Dimensions of Bend Test Pieces.—The bend test pieces are to be machined to a rectangular section 1 inch wide by $\frac{3}{4}$ inch thick, with the edges rounded to a radius of $\frac{1}{16}$ th of an inch. They are to be bent over the thinner section. The bending may be performed either by pressure or by blows.
- 8. Tensile Tests.—The tensile breaking strength determined from test pieces of standard dimensions is to be between the limits of 26 and 35 tons per square inch with an elongation of not less than 20 per cent. measured on the standard test piece.

- 9. Bend Tests.—The bend test pieces must withstand without fracture being bent cold through an angle of 120 degrees, the internal radius of the bend being not greater than one inch.
- 10. Additional Tests before Rejection.—Should either the tensile or bend test or both fail and the Surveyor consider the fractured test piece or test pieces, or the results obtained therefrom, do not fairly represent the quality of the casting, a duplicate of the test or tests which failed shall be made if requested by the Maker. In such cases the quality of the casting shall be judged by the result of the duplicate test or tests and not by the original test or tests which failed.
- 11. Percussive Tests.—The castings are to be dropped on hard ground from a height of from 7 to 10 feet, according to the design, shape, and weight of the casting.
- 12. Castings of Complex Design.—Castings of complex design which would be liable to be deformed if submitted to the drop or percussive test, may have this test dispensed with provided two tensile and two cold bend tests be made upon pieces taken from positions as far apart as possible on each casting; one tensile and one bend test being taken from as near the top and the others from as near the bottom of the casting as practicable.
- 13. Hammering Tests.—After being subjected to the percussive test, the casting in each case is to be subsequently slung up and well hammered with a sledge hammer not less in weight than 7 lbs., to satisfy the Surveyors that the casting is sound and without flaw. This hammering test is also to be applied to castings of complex design which may not have been submitted to a percussive test.
- 14. When the castings are to be used for purposes for which cast iron is ordinarily employed they need not be submitted to tensile and bend tests, but they must be submitted to the drop and hammering tests specified in paragraphs 11 and 13.
- 15. Branding.—Every casting after it has satisfactorily withstood the prescribed tests, shall be clearly and distinctly marked by the Society's Surveyor indicating that the casting has complied with the Society's requirements.

QUALITY AND TESTING OF INGOT STEEL FORGINGS.

Section 6. 1. Process of Manufacture.—Ingot steel for forgings shall be made by the Open Hearth process, Acid or Basic, or by such other process as may be approved by the Committee.

The forgings must be sound, they are to be made from sound ingots, and for all important forgings such as crank and propeller shafts, connecting rods, piston rods, the forgings must be gradually and uniformly forged. The sectional area of the body of the forging (as forged) shall not exceed one-fifth of the sectional area of the original ingot, and no part of the forging (as forged) shall have more than two-thirds of the sectional area of the original ingot.

- 2. Annealing.—All important ingot steel forgings shall be thoroughly annealed in a properly constructed annealing furnace, which must permit of the whole forging being uniformly raised in temperature throughout its whole extent to the necessary intensity required for annealing purposes. If the forging be subsequently heated for any further forging it shall again be similarly annealed, if required by the Surveyor.
- 3. Testing and Inspection.—The following tests and inspections shall be made, preferably at the place of manufacture prior to despatch, but in the event of any forging proving unsatisfactory in the course of preparation or erection, such forging shall be rejected notwithstanding any previous certificate of satisfactory testing.
- 4. Tensile and Bend Test Pieces.—The tensile strength and ductility shall be determined from standard test pieces which are to be prepared from sample pieces cut lengthwise from the forging from a part of not less sectional dimensions than the body of the forging. Such standard test pieces shall be machined from the sample pieces without forging down, and the sample pieces shall not be detached from the forging until the annealing of such forging has been completed. The test pieces are to be stamped by the Surveyor after the annealing. All test pieces shall be selected by the Surveyor and tested in his presence, and he shall satisfy himself that the conditions herein described are fulfilled.
- 5. Number of Tests.—At least one tensile and one cold bend test are to be taken from each forging. Where a number of articles are cut from one forging, one tensile and one cold bend test from this whole forging will be sufficient.
- 6. Dimensions of Tensile Test Pieces.—The tensile test pieces are to be turned so as to have a diameter of '564 inch with a gauge length of 2 inches, or a diameter of '798 inch with a gauge length of 3 inches, or a diameter of '977 inch with a gauge length of 3½ inches.
- 7. Dimensions of Bend Test Pieces.—The bend test pieces are to be machined to a rectangular section 1 inch wide by $\frac{3}{4}$ inch thick, with the edges rounded to a radius of $\frac{1}{16}$ th of an inch. They are to be bent over the thinner

- section. The bending may be performed either by pressure or by blows.
- 8. Tensile Tests.—The tensile breaking strength determined from test pieces of standard dimensions is to be between the limits of 28 and 32 tons per square inch with an elongation on the standard test piece of not less than 29 per cent. for 28 ton steel, and 25 per cent. for 32 ton steel, and in no case must the sum of the tensile breaking strength and corresponding elongation be less than 57.
- 9. Bend Tests.—The bend test pieces must withstand without fracture being bent cold through an angle of 180 degrees, the internal radius of the bend being not greater than $\frac{1}{4}$ inch.
- 10. Additional Tests before Rejection.—Should either the tensile or bend test, or both, fail, and the Surveyor consider the fractured test piece or test pieces, or the results obtained therefrom, do not fairly represent the quality of the forging, a duplicate of the test or tests which failed shall be made if requested by the maker. In such cases the quality of the forging shall be judged by the result of the duplicate test or tests and not by the original test or tests which failed.
- 11. Branding.—Every forging after it has satisfactorily withstood the prescribed tests, shall be clearly and distinctly marked by the Society's Surveyor indicating that the forging has complied with the Society's requirements.
- 12. General.—The requirements as to annealing and testing are intended to apply to shafts of all descriptions, also to connecting rods and piston rods which require to be made in several heats. They are not intended to apply to small forgings which during their last stage of manufacture are uniformly heated throughout.

ENGINES.

- Section 7. 1. The engines are to be fitted with two feed-pumps, each capable of supplying the boilers; the pumps, etc., to be so arranged that either can be overhauled whilst the other is at work.
- 2. The engines are to be fitted with two bilge pumps, which are to be so arranged that either can be overhauled whilst the other is at work.
- 3. In engines of 70 H.P. and under, and in engines of steam fishing vessels, one feed pump and one bilge pump will be deemed sufficient, provided they are of adequate capacity.

The main feed pumps may be worked by independent engines provided they are fitted with automatic regulators for controlling their speed. If only one such pump is fitted for the main feed, the auxiliary feed pump required by paragraph 6 should also be fitted with an automatic speed regulator.

- 4. A bilge injection, or a bilge suction to the circulating pump, is to be fitted.
- 5. The engine bilge pumps are to be fitted capable of pumping from each compartment of the vessel, the peaks excepted. All bilge suction pipes are to be fitted with strum boxes or strainers, so constructed that they can be cleared without breaking the joints of the suction pipes. The total area of the perforations in the strainers should be not less than double that of the cross section of the suction pipe. The mud boxes and roses in engine room are to be placed where they are easily accessible, and to the satisfaction of the Surveyor.
- 6. A steam pump is to be provided capable of supplying the boilers with water; this pump to be provided with suctions to the hotwell and also to the sea. A steam pump is to be so fitted as to pump from each compartment, to deliver water on deck, and if no hand pump is fitted in engine room it must be fitted to be worked by hand. In small vessels in which only one steam pump is fitted, it must comply with all the requirements.
- 7. In all steam pipes provision is to be made for expansion and contraction to take place without unduly straining the pipes, and all main steam pipes are to be tested by hydraulic pressure to twice the working pressure, in the presence of the Engineer Surveyor.
- 8. All discharge-pipes to be, if possible, carried above the deep load-line, and to have discharge valves fitted on the plating of the vessel in an accessible position.
- 9. No pipes are to be carried through the bunkers without being properly protected.
- 10. Bilge suction-pipes to be arranged to pump direct from each compartment, the roses to be fixed in places where they can be easily accessible.

SHAFTS.

Section 8. 1. All shafts are to be turned all over and are to be examined when rough turned and when finished. In the case of screw shafts scrap steel is not to be used, and in no case is a mixture of scrap iron and scrap steel to be employed. It is recommended that screw shafts be made of ingot steel or forged from blooms made from rolled iron bar of good fibrous quality.

- 2. Gauges of an approved description for testing the truth of the crank shafts are to be supplied with all new engines, and adjusted in the presence of the Surveyor.
- 3. The length of the stern bush is to be at least four diameters of the shaft. It is recommended that the shaft liner should be continuous the whole length of the stern tube, and that the after end should be tapered in thickness and made watertight in the propeller boss. If the liner is made in two pieces the joint should be burned. If the liner does not fit tightly at the part between the bearings in the stern tube, the space between the shaft and the liner should be charged or "forced" with a plastic material insoluble in water and non-corrosive. If two liners are used, it is recommended that they be tapered in thickness at the ends, and that the shaft should be lapped or protected between the liners. In this case, and also if no liners are used, the diameter of the shaft should be $\frac{21}{20}$ ths of that required for a shaft with a continuous liner.
- 4. For dimensions of shafts, see the formula in Section 18.

COCKS, PIPES, AND SEA CONNECTIONS.

- Section 9. 1. With a view to insuring better control over cocks, valves, and pipes connecting the engines and boilers with the sea, they are to be fixed as follows, in all new vessels and vessels having new engines or boilers:—
- 2. All sea-cocks to be fitted on the plating of the vessel above the level of the stoke-hold and engine-room platforms, or attached to Kingston valves of a height sufficient to lift them up to the level of these platforms.
- 3. The bolts securing all cocks or sea connections to the plating of the vessel are to be tapped into the plating of the vessel or fitted with countersunk heads.
- 4. The blow-off cocks on the plating of the vessel are to be fitted with spigots passing through the plating, and a brass or gun-metal ring on the outside. The cocks are to be so constructed that the key or spanner can only be taken off when the cock is shut.
- 5. Cocks and valves connecting all suction pipes to be fixed above the stoke-hold and engine-room platforms.
- 6. The arrangements of pumps, bilge injections, suction and delivery pipes, is to be such as will not permit of water being run from the sea into the vessel by an act of carelessness or neglect. Any defective arrangement to be reported to the Committee.

SPARE GEAR.

Section 10. The articles of spare gear mentioned in the following list will be required to be carried in all steam vessels classed in the Society's Register Book, viz.:—

- 2 connecting rod or piston rod top-end bolts and nuts.
- 2 connecting rod bottom-end bolts and nuts.
- 2 main bearing bolts.
- 1 set of coupling bolts.
- 1 set of feed and bilge pump valves.
- 1 set of piston springs (where common springs are used).

A quantity of assorted bolts and nuts.

Iron of various sizes.

In addition to the foregoing the following articles are recommended to be carried with a view to expedite repairs and lessen delay in distant ports, viz.:—

Crank shaft.

Propeller shaft.

Propeller, or a full set of blades.

Stern bush, or lignum vitæ lining for bush.

- 1 pair of connecting rod brasses.
- 1 pair of cross head brasses.
- 1 set of link brasses.
- 1 eccentric strap complete.

Air pump rod.

Circulating pump rod.

- H. P. valve spindle.
- L. P. valve spindle.
- 1 set of check valves.
- 6 cylinder cover bolts.
- 6 junk ring bolts.
- 4 valve chest cover bolts.
- 2 dozen boiler tubes.
- 3 dozen condenser tubes.
- 1 cylinder escape valve and spring.
- 1 set of safety valve springs.

RULES FOR DETERMINING THE WORKING PRESSURE TO BE ALLOWED IN NEW BOILERS.

CYLINDRICAL SHELLS OF IRON BOILERS.

Section 11. The strength of circular shells of iron boilers to be calculated from the strength of the longitudinal joints by the following formula:—

$$\frac{\mathbf{C} \times \mathbf{T} \times \mathbf{B}}{\mathbf{D}}$$
 = working pressure.

where C = co-efficient as per following table,

T = thickness of plate in inches,

D = mean diameter of shell in inches,

B = percentage of strength of joint found as follows—the least percentage to be taken.

For plate at joint
$$\mathbf{B} = \frac{p-d}{p} \times 100$$
.

For rivets at joint $\mathbf{B} = \frac{\mathbf{n} \times \mathbf{a}}{\mathbf{p} \times \mathbf{T}} \times 100$ with iron rivets

in iron plates with punched holes.

$$\textbf{B} = \frac{n \times a}{p \times \textbf{T}} \times 90 \text{ with iron rivets}$$

in iron plates with drilled holes.

(In case of rivets being in double shear, 1.75a is to be used instead of a.)

where p = pitch of rivets.

d = diameter of rivets.

a = sectional area of rivets.

n = number of rows of rivets.

MEM.—In any case where the strength of the longitudinal joint is satisfactorily shown by experiment to be greater than given by this formula the actual strength may be taken in the calculation.

TABLE OF CO-EFFICIENTS.

IRON BOILERS.

Description of Longitudinal Joint.	For Plates ½-inch thick and under.	For Plates \$\frac{3}{4}\$-inch thick and above \$\frac{1}{2}\$-inch.	For Plates above ³ / ₄ -inch thick.
Lap Joint, Punched Holes	155	165	170
Lap Joint, Drilled Holes	170	180	190
Double Butt Strap Joint, Punched Holes	170	180	190
Double Butt Strap Joint, Drilled Holes	180	190	200

Note.—The inside butt strap to be at least \(^3_4\) of the strength of the longitudinal joint,

CYLINDRICAL SHELLS OF STEEL BOILERS.

Section 12. The strength of cylindrical shells of steel boilers is to be calculated from the following formula:—

$$\frac{\textbf{C}\times(\textbf{T}-2)\times\textbf{B}}{\textbf{D}}=$$

working pressure in lbs. per square inch.

where D = mean diameter of shell in inches.

T = thickness of plate in sixteenths of an inch.

C = 22 when the longitudinal seams are fitted with double butt straps of equal width.

- C = 21.25 when they are fitted with double butt straps of unequal width, only covering on one side the reduced section of plate at the outer lines of rivets.
- C = 20.5 when the longitudinal seams are lap joints.

If the minimum tensile strength of shell plates is other than 28 tons per square inch, these values of **C** should be correspondingly modified.

B = the least percentage of strength of longitudinal joint found as follows:—

For plate at joint
$$\mathbf{B} = \frac{p - d}{p} \times 100$$

For rivets at joint $\mathbf{B} = \frac{\mathbf{n} \times \mathbf{a}}{\mathbf{p} \times \mathbf{t}} \times 85$ where steel rivets are used.

$$\mathbf{B} = \frac{\mathbf{n} \times \mathbf{a}}{\mathbf{p} \times \mathbf{t}} \times 70 \text{ where iron rivets}$$

where p = pitch of rivets in inches.

t = thickness of plate in inches.

d = diameter of rivet holes in inches.

n = number of rivets used per pitch in the longitudinal joint.

a = sectional area of rivet in square inches.

(In case of rivets in double shear 1.75a is to be used instead of a.)

Note.—The inside butt strap to be at least 4 of the strength of the longitudinal joint.

Note.—For the shell plates of superheaters or steam chests enclosed in the uptakes or exposed to the direct action of the flame, the co-efficients should be $\frac{2}{3}$ of those given in the preceding tables.

Proper deductions are to be made for openings in shell.

All manholes in circular shells to be stiffened with compensating rings.

The shell plates under domes in boilers so fitted to be stayed from the top of the dome or otherwise stiffened.

STAYS.

Section 13. 1. The strength of stays supporting flat surfaces is to be calculated from the smallest part of the stay or fastening, and the strain upon them is not to exceed the following limits, namely:—

- 2. Iron Stays.—For stays not exceeding $1\frac{1}{2}$ inches smallest diameter, and for all stays which are welded 6,000 lbs. per square inch; for unwelded stays above $1\frac{1}{2}$ inches smallest diameter, 7,500 lbs. per square inch.
- 3. Steel Stays.—For screw stays not exceeding $1\frac{1}{2}$ inches smallest diameter, 8,000 lbs. per square inch; for screw stays above $1\frac{1}{2}$ inches smallest diameter, 9,000 lbs. per square inch. For other stays not exceeding $1\frac{1}{2}$ inches smallest diameter, 9,000 lbs. per square inch, and for stays exceeding $1\frac{1}{2}$ inches smallest diameter, 10,400 lbs. per square inch. No steel stays are to be welded.
- 4. Stay Tubes.—The stress is not to exceed 7,500 lbs. per square inch.

FLAT PLATES.

Section 14. 1. The strength of flat plates supported by stays is to be taken from the following formula:—

$$\frac{\mathbf{C} \times \mathbf{T}^2}{\mathbf{P}^2}$$
 = working pressure in lbs. per square inch;

where T = thickness of plate in sixteenths of an inch,

- \mathbf{P}^2 = square of pitch in inches. If the pitch in rows is not equal to that between the rows, then the mean of the squares of the two pitches is to be taken,
- C = 90 for iron or steel plates $\frac{7}{16}$ thick and under, fitted with screw stays with riveted heads,
- C = 100 for iron or steel plates above $\frac{7}{16}$ thick fitted with screw stays with riveted heads,
- C = 110 for iron or steel plates $\frac{7}{16}$ thick and under, fitted with stays and nuts,
- C = 120 for iron plates above $\frac{7}{16}$ thick, and for steel plates above $\frac{7}{16}$ and under $\frac{9}{16}$ thick, fitted with screw stays and nuts,

- C = 135 for steel plates $\frac{9}{16}$ thick and above, fitted with screw stays and nuts,
- **C** = 140 for iron plates fitted with stays with double nuts,
- C = 150 for iron plates fitted with stays with double nuts and washers outside the plates, of at least $\frac{1}{3}$ of the pitch in diameter and $\frac{1}{2}$ the thickness of the plates,
- **C** = 160 for iron plates fitted with stays with double nuts and washers riveted to the outside of the plates, of at least $\frac{2}{5}$ of the pitch in diameter and $\frac{1}{2}$ the thickness of the plates,
- $\mathbf{C} = 175$ for iron plates fitted with stays with double nuts and washers riveted to the outside of the plates, when the washers are at least $\frac{2}{3}$ of the pitch in diameter and of the same thickness as the plates.

For iron plates fitted with stays with double nuts and doubling strips riveted to the outside of the plates, of the same thickness as the plates, and of a width equal to $\frac{2}{3}$ the distance between the rows of stays, **C** may be taken as 175, if **P** is taken to be the distance between the rows, and 190 when **P** is taken to be the pitch between the stays in the rows.

For steel plates, other than those for combustion chambers, the values of C may be increased as follows:—

2. If flat plates are strengthened with doubling plates securely riveted to them, having a thickness of not less than $\frac{2}{3}$ of that of the plates, the strength to be taken from

$$\mathbf{C} \times (\mathbf{T} + \frac{t}{2})^2 =$$
 working pressure in lbs. per square inch;

where t = thickness of doubling plates in sixteenths, and C, T and P are as above.

Note.—In the case of front plates of boilers in the steam space, these numbers should be reduced 20 per cent., unless the plates are guarded from the direct action of the heat.

3. For steel tube plates in the nest of tubes the strength to be taken from

$$\frac{140 \times \mathbf{T}^2}{\mathbf{P}^2}$$
 = working pressure in lbs. per square inch;

where **T** = the thickness of the plates in sixteenths of an inch,

P = the *mean* pitch of stay tubes from centre to centre.

For the wide water spaces between the nests of tubes the strength to be taken from

$$\frac{\mathbf{C} \times \mathbf{T}^2}{\mathbf{P}^2}$$
 = working pressure in lbs. per square inch;

where **P** = the horizontal distance from centre to centre of the bounding rows of tubes, and

C = 120 where the stay tubes are pitched with two plain tubes between them and are not fitted with nuts outside the plates,

C = 130 if they are fitted with nuts outside the plates,

C = 140 if each alternate tube is a stay tube not fitted with nuts,

C = 150 if they are fitted with nuts outside the plates.

C = 160 if every tube in these rows is a stay tube and not fitted with nuts,

C = 170 if every tube in these rows is a stay tube and each alternate stay tube is fitted with nuts outside the plates.

4. The thickness of tube plates of Combustion Chambers in cases where the pressure on the top of the chambers is borne by these plates is not to be less than that given by the following rule:—

$$\mathbf{T} = \frac{\mathbf{P} \times \mathbf{W} \times \mathbf{D}}{1750 \times (\mathbf{D} - d)}$$

where P = working pressure in lbs. per square inch.

W = width of Combustion Chamber between plates in inches.

D = horizontal pitch of tubes in inches.

d = inside diameter of plain tubes in inches.

T = thickness of tube plates in sixteenths of an inch.

GIRDERS.

Section 15. The strength of girders supporting the tops of combustion chambers and other flat surfaces to be taken from the following formula:—

$$\frac{\textbf{C}\times\mathrm{d}^2\times\textbf{T}}{(\textbf{L-P})\times\textbf{D}\times\textbf{L}} = \text{working pressure in lbs. per square inch} \; ;$$

where **L** = width between tube plates, or tube plate and back plate of chamber,

P = pitch of stays in girders,

D = distance from centre to centre of girders,

d = depth of girder at centre,

T = thickness of girder at centre. All these dimensions to be taken in inches.

Wrought Iron.

C=

6,000, if there is one stay to each girder.

9,000, if there are two or three stays to each girder.

10,000, if there are four or five stays to each girder.

10,500, if there are six or seven stays to each girder.

10,800, if there are eight stays or above to each girder.

Wrought Steel.

7,110, if there is one stay to each girder.
10,660, if there are two or three stays to each girder.
11,850, if there are four or five stays to each girder.
12,440, if there are six or seven stays to each girder.
12,800, if there are eight stays or above to each girder.

If the minimum tensile strength of girder plates is other than 28 tons per square inch, these values of **C** should be correspondingly modified.

CIRCULAR FURNACES.

Section 16. 1. The strength of plain furnaces to resist collapsing to be calculated as follows:—

Where the length of the plain cylindrical part of the furnace exceeds 120 times the thickness of the plate, the working pressure is to be calculated by the following formula:—

$$\frac{1{,}075{,}200\,\times\,{\color{red}{\textbf{T}}}^2}{{\color{blue}{\textbf{L}}}\times{\color{blue}{\textbf{D}}}}=$$

working pressure in lbs. per square inch;

Where the length of the plain cylindrical part of the furnace is less than 120 times the thickness of the plate, the

working pressure is to be calculated by the following formula:—

$$\frac{50 \times (300 \mathbf{T} - \mathbf{L})}{\mathbf{D}} =$$

working pressure in lbs. per square inch,

where D = outside diameter of furnace in inches,

T = thickness of plates in inches,

L = length of plain cylindrical part in inches, measured from the centres of the rivets connecting the furnaces to the flanges of the end and tube plates, or from the commencement of the curvature of the flanges of the furnace where it is flanged or fitted with Adamson rings.

- 2. In the furnaces referred to below the formulæ given are applicable if the steel used has a tensile strength of not less than 26 nor more than 30 tons per square inch. If the material of furnaces has a less tensile strength than 26 tons per square inch, then for each ton per square inch which the minimum tensile strength falls below 26, the co-efficient is to be correspondingly decreased by $\frac{1}{26}$ th part.
- 3. The strength of corrugated furnaces made on Fox's, Morison's, Deighton's, or Beardmore's plan, to be calculated from

$$\frac{1,259 \times (T-2)}{D} =$$

working pressure in lbs. per square inch.

4. The strength of spirally corrugated furnaces is to be calculated from the following formula:—

$$\frac{912\times (T-2)}{\mathsf{D}} =$$

working pressure in lbs. per square inch; where T = thickness of plate in sixteenths of an inch, and **D** = outside diameter of corrugated furnaces, in inches.

5. The strength of the Improved Purves' furnaces with ribs 9 inches apart, and of Brown's Cambered furnaces with ribs either 8 inches or 9 inches apart, to be calculated from the following formula:—

$$\frac{1,160 \times (T-2)}{D} =$$

working pressure in lbs. per square inch.
where T = thickness of plate in sixteenths of an inch,
and D = smallest outside diameter of furnaces, in
inches.

6. The strength of the Leeds Forge bulb furnace is to be calculated from the following formula:—

$$\frac{1,259\times(T-2)}{D} =$$

working pressure in lbs. per square inch; where T = thickness of plate in sixteenths of an inch, and D = smallest outside diameter in inches.

7. The strength of Holmes' patent furnaces, in which the corrugations are not more than 16 inches apart from centre to centre, and not less than 2 inches high, to be calculated from the following formula:—

$$\frac{945 \times (T-2)}{D} =$$

working pressure in lbs. per square inch;

where T = thickness of plain portions of furnace in sixteenths of an inch,

and **D** = outside diameter of plain parts of the furnace in inches.

DONKEY BOILERS.

Section 17. The iron used in the construction of the fire boxes, uptakes, and water tubes of donkey boilers shall be of good quality, and to the satisfaction of the Surveyors, who may in any cases where they deem it advisable apply the following tests:—

Thickness of	To Bend cold through an angle of						
Plates.	With the Grain.	Across the Grain.					
. 5 16	80°	45°					
6 16	70°	35°					
7 16	55°	25°					
8 16	40°	20°					

The material to stand bending *hot* to an angle of 90 degrees, over a radius not greater than $1\frac{1}{2}$ times the thickness of the plates.

RULES FOR DETERMINING SIZES OF SHAFTS.

Section 18. 1. The diameters of intermediate shafts are to be not less than those given by the following formula:—

For Compound Engines with two cranks at right angles— Diameter of intermediate shaft in inches =

$$(.04 \text{ A} + .006 \text{ D} + .05 \text{ S}) \times \sqrt[3]{\text{P}}$$

For Triple expansion engines with three cranks at equal angles—

Diameter of intermediate shaft in inches= $(.038 \text{ A} + .009 \text{ B} + .002 \text{ D} + .0165 \text{ S}) \times \sqrt[3]{\text{P}}$

For Quadruple expansion engines with two cranks at right angles—

Diameter of intermediate shaft in inches=

$$(.034 \, \text{A} + .011 \, \text{B} + .004 \, \text{C} + .0014 \, \text{D} + .016 \, \text{S}) \times \sqrt[3]{\text{P}}$$

For Quadruple expansion engines with three cranks— Diameter of intermediate shaft in inches=

$$(.028\,A + .014\,B + .006\,C + .0017\,D + .015\,S) \times \sqrt[3]{P}$$

For Quadruple expansion engines with four cranks—

Diameter of intermediate shaft in inches=

$$(.033 \, \text{A} + .01 \, \text{B} + .004 \, \text{C} + .0013 \, \text{D} + .0155 \, \text{S}) \times \sqrt{\frac{3}{3}} \, P$$

where **A** = diameter of High Pressure Cylinder in inches,

B = diameter of first Intermediate Cylinder in inches,

C = diameter of second Intermediate Cylinder in inches,

D = diameter of Low Pressure Cylinder in inches,

S = Stroke of Pistons in inches,

P = Boiler pressure above atmosphere in lbs. per square inch.

- 2. The diameter of crank shaft, and of thrust shaft under the collars, to be at least $\frac{21}{20}$ ths of that of the intermediate shaft. The diameter of thrust shaft may be tapered off at each end to the same size as that of the intermediate shaft.
- 3. The diameter of the screw shaft to be equal to the diameter of intermediate shaft (found as above) multiplied by $\left(\cdot 63 + \frac{\cdot 03}{\mathsf{T}} \right)$, but in no case to be less than 1.07 **T**, where **P** is the diameter of propeller, and

T the diameter of intermediate shaft, both in inches.

This size of screw shaft is intended to apply to shafts fitted with continuous liners the whole length of the stern tube, as provided for in Section 8, paragraph 3. If no liners are used or if two separate liners are used, the diameter of the shaft should be $\frac{21}{20}$ ths that given above.

The diameter of screw shaft is to be tapered off at the forward end to the size of the crank shaft.

4. Note.—The Rules are intended to apply to Two Cylinder Compound Engines, in which the ratio of areas of Low and High Pressure Cylinders does not exceed 4.5 to 1; to Triple Expansion Engines in which it does not exceed 9 to 1; to Quadruple Expansion Engines in which it does not exceed 12 to 1; and in all cases, as regards the stroke, in which the length of stroke is not less than one half the diameter or greater than the diameter of the Low Pressure Cylinder. Engines of extreme proportions beyond these limits being specially submitted to be dealt with on their merits.

PERIODICAL SURVEYS. (See N.B.)

Section 19. 1. The machinery and boilers of all steam ships and the donkey boilers of sailing vessels are to be surveyed annually if practicable, and in addition are to be submitted to a Special Survey upon the occasions of the vessels undergoing the Special periodical Surveys Nos. 1, 2, and 3, prescribed in the Rules, unless the machinery and boilers have been specially surveyed within a period of twelve months.

- 2. At these Special Surveys, and on other occasions if deemed necessary by the Surveyors, the propeller, stern-bush, sea connections, and their fastenings, are to be examined while the vessel is in dry dock.
- 3. The stern shaft is to be examined annually and drawn at intervals of not more than two years.**
- 4. The cylinders, pistons, slide valves, crank and tunnel shafts, and pumps are to be examined, and if necessary the condenser is to be examined and tested.
- 5. The arrangements of cocks, pipes, bilge-suctions, roses, &c., are to be examined.
- 6. The boilers and superheaters are to be examined internally and externally, and if deemed necessary by the Surveyors, both boilers and superheaters are to be drilled or tested by hydraulic pressure; the safe working pressure is to be determined by their actual condition.
- 7. The safety valves are to be examined and set to the safe working pressure.
- * On the application of owners, the Committee will be prepared to give consideration to the circumstances of any special case.

- 8. If satisfactory, these Surveys will be recorded in the Register Book thus:—"LMC6,11" in red or "B&MS6,11" in red.
- 9. "LMC" (LLOYD'S MACHINERY CERTIFICATE) denotes that the machinery and boilers are fitted in accordance with the Rules; and when followed by a date, indicates that they were found at that time to be in good condition. MS. with a date denotes that the engines at that time were found upon inspection to be in good condition. BS. with a date denotes that the boilers were found upon inspection at that time to be in good condition.
- 10. "B&MS" (BOILERS AND MACHINERY SURVEYED), with a date, denotes that the boilers and machinery, though not fitted strictly in accordance with the Rules, were found upon inspection at that time to be in good condition.
- 11. In the event of either the machinery or boilers appearing to be impaired to such an extent as to render it desirable that either or both be specially surveyed within the periods prescribed above, a Certificate for either machinery or boilers for a limited period will be granted according to the nature of the case.

BOILERS.

- 12. The boilers of all steam ships and the donkey boilers of sailing vessels are to be specially surveyed when six years old, and subsequently they are to be specially surveyed annually.
- 13. At these surveys the boilers and superheaters are to be examined internally and externally, and if deemed necessary by the Surveyors, both boilers and superheaters are to be drilled or tested by hydraulic pressure; the safe working pressure is to be determined by their actual condition.
- 14. The safety valves are to be examined and set to the safe working pressure.
- 15. If satisfactory these surveys will be recorded in the Register Book thus:—"BS6,11" in red in the case of steam vessels, and "DBS6,11" in red in the case of sailing vessels.

16. "BS" (Boilers Surveyed) or "DBS" (Donkey Boiler Surveyed), with a date, denotes that the boilers were found upon inspection at that time to be in good condition.

17. In the event of the boilers appearing to be impaired to such an extent as to render it desirable that they be specially surveyed within the periods prescribed above, a Certificate for a limited period will be granted according to the nature of the case.

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N.B.—In reference to the Rules above quoted, and in order to prevent the disappointment arising from Ships losing their Characters from want of survey, it is hereby intimated that the duty of giving Notice of Periodical Surveys required by the Rules, or when repairs are necessary in consequence of damage, or from other causes, rests with the Owners, Masters, or Agents.

By order of the Committee,

ANDREW SCOTT,

Secretary.

RULES FOR THE SURVEY OF INTERNAL COMBUSTION ENGINES FOR MARINE PURPOSES.

GENERAL.

Section 1. In vessels propelled by Internal Combustion Engines, the Rules as regards Machinery will be the same as those relating to steam engines so far as regards the testing of material used in their construction and the fitting of sea connections, discharge pipes, shafting, stern tubes and propellers.

CONSTRUCTION.

- Section 2. 1. The following points should be observed in connection with the design of the engines.
- 2. The shaft bearings, connecting rod brasses, the valve gear, the inlet and exhaust valves must be easily accessible.
- 3. The reversing gear and clutch must be strongly constructed and easily accessible for examination and adjustment.
- 4. In engines of above 60 B.H.P. which are not reversible and which are manœuvred by clutch, a governor or other arrangement must be fitted to prevent racing of the engine when declutched.
- 5. Efficient positive means of lubrication (preferably sight feed) must be fitted to each part requiring continuous lubrication.
- 6. If the engines are of the closed-in type, they must be so fitted that the contained lubricating oil can be drained when necessary, and in wood vessels an easily drained metal or metal-lined tray must be fitted to prevent leakage of either fuel oil or of lubricating oil from saturating the wood work.
- 7. Carburettors, where petrol is used, and vaporisers, where paraffin is used, should be so designed that when the engine is stopped the fuel supply is automatically shut off. If an overflow is provided in the carburettor or vaporiser, a gauze covered tray with means of draining it must be fitted to prevent the fuel from flowing into the bilges.

Strong metallic gauze diaphragms should be fitted either between the carburettor (or vaporiser) and cylinders or at the air inlets.

8. If the ignition is electric, either by magneto or by coil and accumulator, all electric leads must be well insulated and suitably protected from mechanical injury. The leads should be kept remote from petrol pipes, and should not be placed where they may be brought into contact with oil.

The Commutator must be enclosed; and the sparking coils must not be placed where they can be exposed to explosive vapours.

- 9. No exposed spark gap should be fitted.
- 10. In paraffin and heavy oil engines where lamps are used for ignition or for vaporising, these lamps should be fixed by some suitable bracket, and the flame enclosed when in use.
- 11. The circulating pump sea suction is to have a cock or valve on the vessel's skin placed on the turn of the bilge in an easily accessible position, and the circulating pipe is to be provided with an efficient strainer inside the vessel. The discharge overboard is to be fitted with a cock or valve on the vessel's skin if it is situated under or near the load line of the vessel.
- 12. A bilge pump worked by the engines or an independent power-driven bilge pump is to be fitted, to draw from each part of the vessel. In open launches this bilge pump may be omitted provided suitable hand pumps are fitted.
- 13. The cylinders are to be tested by hydraulic pressure to twice the working pressure to which they will be subjected. The water jackets of the cylinders to 50lbs. per square inch, and the exhaust pipes and silencer to 100lbs. per square inch.

- 14. The exhaust pipes and silencer should be efficiently water cooled or lagged to prevent damage by heat, and if the exhaust is led overboard near the water-line, means must be arranged to prevent water from being syphoned back to the engine.
- 15. The machinery must be tried under full working conditions, the report stating the approximate speed of vessel, the number of revolutions of the engines at full power, both ahead and astern, and the lowest number of revolutions of the engines which can be maintained for manœuvring purposes.

RULES FOR DETERMINING SIZES OF SHAFTS.

Section 3. The crank, intermediate, and other shafts if of ordinary mild steel are to be of not less diameters than as given in the following table. When special steel is used, the sizes are to be submitted for consideration.

1. For Petrol or Paraffin Engines for smooth water services:—

$$\frac{\text{Diameter of crank}}{\text{shaft in inches}} = \mathbf{C} \sqrt[3]{\mathbf{D}^2 \mathbf{S}}$$

where $\mathbf{D} = \text{diameter of cylinder in inches}$,

S = stroke of piston in inches.

Four Stro	Two	Strycle		Bearing between each crank.	Two cranks between the bearings.		
For 1, 2, 3,	or 4	Cyls.	1 or	2	Cyls.	C = ·34	C =:38
"	6	"	W Los	3	"	C =.36	C = 40
"	8	"		4	"	C =.38	C = 425
"	12	. ,,		6	,,	C = 44	C =:49

For open sea service add .02 to C.

Diameter of intermediate and screw shafts in inches
$$= \mathbf{C} \sqrt[3]{\mathbf{D}^2 \mathbf{S} (n+3)}$$

where D = diameter of cylinder in inches,

S = stroke of piston in inches,

n = number of cylinders.

For smooth water services— C = 155 for intermediate shafts.	
C = 170 for screw shafts fitted with continuous liners.	C = :180
C = 180 for screw shafts fitted with separate liners or with no liners.	C = :190

In engines of two-stroke cycle, n is to be taken as twice the number of cylinders.

- 2. When ordinary deep thrust collars are used the diameter of the shaft between the collars is to be at least $\frac{2}{20}$ ths of that of the intermediate shaft.
- 3. In the cases of **Diesel** and other Engines in which very high initial pressures are employed, particulars should be submitted for special consideration.

FUEL TANKS AND CONNECTIONS.

- Section 4. 1. Separate fuel tanks are to be tested with all fittings, to a head of at least 15 feet of water. If pressure feed tanks are employed, they are to be tested to twice the working pressure which will come on them but at least to a head of 15 feet of water. If the tanks are made of iron or steel they should be galvanized.
- 2. Strong and readily removable metallic gauze diaphragms should be fitted at all openings on petrol tanks.
- 3. Paraffin or heavy oil tanks, not used under pressure, are to be fitted with air pipes leading above deck. Pressure-feed tanks and tanks containing petrol, should be provided with escape valves discharging into pipes leading to the atmosphere above deck. The upper ends of all air pipes are to be turned down and pipes above 1 inch diameter are to be provided with gauze diaphragms at the end.
- 4. No glass gauges are to be fitted to fuel tanks containing either petrol, paraffin or heavy oil.
- 5. Filling pipes are to be carried through the deck so that the gas displaced from the tanks has free escape to the atmosphere.

- 6. Separate fuel tanks should be provided with metallined trays to prevent any possible leakage from them flowing into the bilges, or saturating woodwork. Arrangements are to be provided for emptying the tanks and draining the trays beneath them. For petrol tanks the trays must have drains leading overboard where possible or they should be gauze covered trays with means for draining them.
- 7. All fuel pipes are to be of annealed seamless copper with flexible bends. Their joints are to be conical, metal to metal. A cock or valve is to be fitted at each end of the pipe conveying the fuel from the tank to the carburettor or vaporiser. The fuel pipes should be led in positions where they are protected from mechanical injury and can be exposed to view throughout their whole length.
- 8. The engine room, and the compartment in which the fuel tanks are situated, are to be efficiently ventilated.
 - 71, FENCHURCH STREET, LONDON, E.C. 16th June, 1910.

9. An approved fire extinguishing apparatus must be supplied.

PERIODICAL SURVEYS.

Section 5. 1. The machinery is to be submitted to survey annually. At these surveys the cylinders, pistons, connecting rods, crank and other shafts, inlet and exhaust valves and gear, clutches, reversing gear, propeller, sea connections, and pumps are to be examined. The electric ignition is to be examined and the electric leads tested. The fuel tanks and all connections are to be examined, and if deemed necessary by the Surveyor, to be tested to the same pressure as required when new. If practicable, the engines should be tested under working conditions.

2. The screw shaft is to be drawn at intervals of not more than four years.

By order of the Committee,

ANDREW SCOTT,

Secretary.

USE OF ELECTRIC LIGHT ON BOARD VESSELS.

The following requirements as to the sizes, positions, and protection of the cables, and to the fitting of the cut-outs are now embodied as Rules.

LEADS OR CIRCUITS.

- 1. The sectional area of the copper wires in the cables should be at least in the proportion of one square inch per 1,000 ampères carried.
- 2. No single wire of greater size than 14 or of less than 18 standard wire gauge should be used. For portable leads, cables composed of stranded wires should be used having sufficient conductivity and flexibility for the purposes intended.
- 3. The copper used in all wires or cables should have a conductivity of at least 98 per cent. that of pure copper.
- 4. The insulation resistance of all wires, including portable leads, should be not less than 600 megohms per statute mile, after 24 hours immersion in sea water.
- 5. The insulating material used must not appreciably soften if subjected to a temperature of 180° F. If indiarubber insulation is used, the wires should be first covered with a layer of pure rubber, then with a separator, then with a layer of vulcanizing india-rubber, and then with a layer of india-rubber coated tape. The whole should then be vulcanized together. The cable should afterwards be satisfactorily protected, preferably with a braided covering of waterproof fibre.
- 6. Wires which are insulated with any other material than india-rubber should fulfil the same conditions as to insulation resistance, and should be of equal durability with those above specified.

JOINTS.

7. Joints in branches, or of branches with leads of small circuits, must be made in properly constructed watertight junction boxes, or should have the copper wires thoroughly soldered and the insulation carefully carried out, all the

- joints being made watertight. Joints in flow and return wires should not be made opposite one another. All joints should be in accessible positions, none being made in bunkers, cargo spaces, or spaces which may at any time be used for carrying cargo, stores or baggage.
- 8. For soldering wires, resin only should be used as a flux.
- 9. Where practicable, the leads should be placed where they can always be accessible; if they are laid in wood battens the covers should be screwed on, not nailed, and care should be taken that the casings are so arranged that water will not lodge in them. Cables which are properly covered with protective metal sheathing, or which are protected by galvanized wire armouring, may be unencased. They should, however, be secured by screwed clips, not by staples. All sharp bends in cables should be avoided.
- 10. All cables which are liable to be exposed to the weather or moisture should be lead covered, or be otherwise specially protected. Where great heat is experienced, no wood casing should be used, but the cables should be protected by iron casings, or if they are not exposed to mechanical injury, they may be armoured with galvanized wire and fastened to decks or bulkheads with screwed clips spaced not more than 12 inches apart.
- 11. If cables are led through cargo spaces, coal bunkers, or spaces which may at any time be used for carrying cargo, stores, or baggage, or which are not at all times accessible, they should be strongly protected against damage, preferably by iron casings. If they are led through metal tubes, these must be strongly secured, and should be fitted so that water cannot lodge in them.

Armoured cables may be used without casings or tubes provided they are strongly secured to the under side of decks or to bulkheads by screwed clips and provided they are armoured in conformity with the standard of the Engineering Standards Committee, viz. :—

For cables below $\frac{1}{2}$ inch diameter over lead by galvanized steel wires '072 diameter, for cables $\frac{1}{2}$ inch to 1 inch over lead by two layers of steel tape each '03 inch thick, for cables above 1 inch to 2 inches diameter by two layers of steel tape each '04 inch thick, and for larger cables by two layers of steel tape '06 thick.

- 12. Where cables pass through beams, bulkheads, or other iron work, they should be led through special fittings of sheet lead, hard wood or vulcanized fibre to prevent their being chafed, and where they pass through decks they should be led through metal tubes lined with wood, or vulcanized fibre, and securely fastened to the decks, standing at such a height above the deck level that water cannot stand above them. Where cables pass through watertight bulkheads the fittings should be provided with brass watertight screwed glands.
- 13. In vessels having spaces allotted alternately for passengers and cargo the lamp fittings in these spaces should be removable, and the terminals so arranged that they can be properly covered up with strong metal covers, or the whole of the fittings should be similarly provided with strong metal covers. The main switches and cut-outs should be outside these spaces, or if placed inside, they should be in strong iron boxes provided with iron covers, or otherwise securely arranged to prevent the fittings being tampered with.

DISTRIBUTION.

- 14. A main switchboard should be fitted in the dynamo room, to which all the main circuits throughout the ship should be brought, a switch and cut-out being fitted thereon for each circuit. The auxiliary switchboards for further sub-division of the current should be placed in conveniently accessible positions, and each such switchboard should be similarly fitted with a separate switch and cut-out for each sub-circuit. Cut-outs should be fitted to each lamp circuit where these are made with reduced size of wire. If vessels are wired on the double-wire system, cut-outs should be fitted to each cable of these circuits.
- 15. In cases where electric lights are used for the masthead light and side lights, the switches controlling these lights should be placed in a position where they can be controlled by the Officer of the watch, or other responsible person, and cannot be tampered with by other members of the crew, or by passengers, &c.

- 16. The switchboards should be of slate or other incombustible material. The switches should be on the quick break principle, and should be so constructed that they must be either full "on" or completely "off," that is, they must not be able to remain in an intermediate position. They should have ample rubbing surfaces, and their conductivity should not be less than that of the wires connected to them.
- 17. Cut-outs should be fitted to each main or auxiliary circuit, on the switchboards, as near as possible to the switches of these circuits. If the switchboard is not fitted near the dynamo, or if more than one dynamo may be used on any one circuit, then cut-outs should also be fitted to the main cable as near as possible to each of the dynamo terminals.
- 18. All other cut-outs should also be in easily accessible places, and as near as possible to the commencement of the cables or wires they protect. They should be mounted on slate or other incombustible bases, and be arranged so that the fused metal may not be a source of danger, and where fitted with covers these should be incombustible.
- 19. All fuses should be of easily fusible and non-oxidizable metal, and should be so proportioned as to melt with a current of 100 per cent. in excess of the normal current, that is they should melt with a current in the proportion of 2,000 ampères per square inch of section of the wires they protect. The fuses for branch wires to single lights should, however, if of tin wire, be of not greater size than 22 s.w.g.
- 20. The fuses for each cable should be made of standard dimensions, so that a large fuse cannot be used for a small cable by mistake, or, if wire fuses are used, permanent instructions should be fitted on or near each switchboard, giving particulars of the proper size of fuse for each circuit.
- 21. In shaft passages, and in damp places, all lamp switches and cut-outs should be of a strong watertight pattern, or should be placed in watertight boxes having hinged or portable watertight covers. No switches or cut-outs are to be placed in bunkers.
- 22. There should be no joints in the cables leading from the dynamo to the main switchboard, nor in those leading from the main to auxiliary switchboards, nor should branches to single lamps be taken off these cables.
- 23. A voltmeter should be supplied with each installation. If more than one dynamo is fitted, neither being capable of the whole of the output, an ampère meter should be supplied with each dynamo.

JOINTS WITH HULL.

24. In vessels fitted on the single-wire system, all the joints with the hull should be placed in accessible positions. Those for single lamps or for small cables should be made with brass screws not less than three-eights of an inch in diameter, carefully tapped into the iron or steel, having white brass washers, between the wires and the vessel, or the wires should be soldered to brass faced-washers. For larger cables and for the pole of dynamo the cable wires should be properly sweated into brass or copper shoes, which should be bolted to the vessel. The iron or steel where contact is made should be filed bright, and the area of contact should not be less than eight times the section of the copper of the cable.

IN VESSELS CARRYING PETROLEUM.

25. The single wire system must not be adopted for any part of the installation. Switches and cut-outs must not be fitted in places liable to the accumulation of petroleum vapour or gas, and all lamps in places where it is possible for gas to accumulate must be made with an outer glass globe made air tight. All wires in such places are to be lead covered, or the insulation of the cables employed is to be of such a nature as not to be affected by petroleum. No joints of cables, switches, or cut-outs should be fitted in the pump room, but the wires for each lamp therein should be carried to the lamp from a distributing junction box placed outside the pump room or companion.

The following paragraphs referring to the effect of the Electric Light Installations upon the Compasses are issued as suggestions, not as Rules.

POSITION OF DYNAMOS AND OF ELECTRIC MOTORS.

26. The position and type of Dynamos and Electric Motors should be such that the compasses will not be affected. Dynamos and large motors should be at least 30 feet from the standard compass.

71, FENCHURCH STREET, LONDON, E.C. 17th June, 1909.

CABLES.

27. In vessels fitted with continuous current dynamos, and wired on the single-wire system, no single cable should be carried within 15 feet of any compass, and cables conveying heavy currents should be fixed at still greater distance. If it is necessary to fix any cables within this distance, then for all parts of the vessel lighted from this cable the concentric or double-wire system should be adopted, the return wire being carried as near the flow as possible in the vicinity of the compasses.

ADJUSTMENT OF COMPASSES.

28. The compasses should be adjusted with the dynamo not working, after which the vessel's head should be put upon the different courses, with the dynamo running at full-speed, and on each course the indications of the compass should be noted with the dynamo running with open circuit and with all possible combinations of the current switched "on" and "off" all circuits passing near the compasses. These indications should be compared with those obtained with the dynamo stopped, and any serious deflections of the compasses remedied before the vessel sails.

The requirements in paragraphs 3 to 8 inclusive, referring to the quality of the material used, or to the workmanship employed, are embodied as Rules; but as the quality of the material can only be tested at the Cable Makers' works, and as the workmanship of the joints cannot be examined or tested after completion, the guarantee of the Electrical Engineers will be required as to these points.

By order of the Committee,

ANDREW SCOTT,

Secretary.

REFRIGERATING MACHINERY AND APPLIANCES.

On the application of the owners of vessels fitted for carrying refrigerated cargoes, the Committee will authorize their Surveyors to survey the refrigerating machinery and appliances, and in those cases where the following conditions are complied with and a satisfactory report is received from the Surveyor, certificates of these Surveys will be issued and the notation R.M.C. (in red) (i.e. Refrigerating Machinery Certificate) will be made against the vessel's name in the Society's Register Book, and in the special list of vessels fitted with refrigerating appliances. In cases in which the refrigerating machinery and appliances are constructed under the special survey of the Society's Surveyors and to their entire satisfaction, the notation \(\mathbb{R}\).M.C. (in red) will be made in the Register Book. The name of the maker and description and number of the refrigerating machines, whether single or duplex, and the refrigerating power of the machines will be recorded in the special list in the Register Book, as will also the number and capacity of insulated cargo chambers and the nature of the insulation and the method employed for cooling the holds.

1. The insulation must be sound and in good order and of efficient construction. The details of construction showing the amount and nature of the insulating material employed in the various parts are to be reported to the Committee.

Bilge suction and sounding pipes and ballast tank air and sounding pipes, passing through insulated spaces, should be well insulated to prevent their being frozen up. No sluice valves, scuppers or drain pipes are to be fitted which will permit drainage from spaces outside of the insulated chambers into the bilges of the insulated holds.

It is recommended that the wood-work of the insulation over tunnel tops be fastened with screws to facilitate the examination of this part, and that extra strong battens of American Elm be fitted upon it under the hatches. Insulated removable portions are to be arranged in the

bulkhead insulation, where required, to give easy access to sluice valves and bilge suction roses. The bottoms, sides and coamings of all insulated hatches and limbers should be painted to prevent decay.

Thermometer tube flanges and covers should be arranged so that water does not run down and freeze in them when taking the temperature.

Cargo battens should be provided for the floor or deck and the sides of the chambers previous to loading the homeward cargo. Those for the sides of the chambers should be fastened, and should be at least $1\frac{1}{2}$ inches in depth and 2 inches wide, one batten being placed over each frame or ground, the others being intermediately arranged. The battens for the floor and decks should be at least $2'' \times 2''$.

Where the brine system of refrigerating is employed, the brine circulating pipes and tanks should not be galvanized on the inside.

In cases where internally galvanized tanks and cooling pipes have been fitted, the brine cooling and return tanks, if closed, should be provided with two ventilating pipes communicating with the atmosphere. If the tanks are not closed, the cooling room should be efficiently ventilated.

- 2. The refrigerating machinery is to be of approved construction and of sufficient power to maintain the necessary low temperature in the cargo chambers in tropical climates when running 18 hours per day. For cargo capacities of above 70,000 cubic feet the machinery is to be either duplex or in duplicate.
- 3. A sufficient amount of spare gear is to be supplied and stowed where it is readily accessible.

No spare gear will, however, be required in cases where two complete sets of refrigerating machines are fitted *each* being of sufficient power to maintain the necessary low temperature in the cargo chambers in tropical climates when running 18 hours per day, provided all the working parts of these machines are interchangeable. When two similar machines are fitted, each connected to different cargo compartments, one set of spare gear suitable for either machine will suffice.

Where one single dry air machine is fitted to each compartment, the following will be required:—

1 crank shaft with eccentric sheaves, complete, or one half shaft if the halves are interchangeable.

1 piston rod and nuts for steam and air cylinders.

1 set of piston rod and connecting rod brasses.

1 piston, complete, for each steam and air cylinder.

1 cylinder cover for each pattern used in steam and air cylinders.

1 air pump bucket and rod.

1 circulating pump bucket and rod.

1 pair main bearing brasses, complete.

Main and cut-off valves for each steam cylinder.

Balance springs and rings for steam and air slide valves.

False valve face for each pattern fitted in steam cylinders, with screws.

1 eccentric rod for each pattern used.

1 eccentric strap for each pattern used.

1 slide valve spindle and nuts for steam and air cylinders, for each pattern used.

2 main bearing bolts.

1 set of connecting rod and piston rod bolts.

Full set of air valves and seats for air compressor.

1 set of inlet and outlet valves, and 1 set valve faces (if fitted) for air expansion cylinder with screws.

.1 set of valves for air, circulating and feed pumps.

1 set of escape valve springs.

50 suction springs.

50 delivery springs.

50 buffer springs.

6 tubes and 24 ferrules for condenser.

6 tubes for cooler.

6 tubes for air drying chamber.

Assorted bolts, studs and nuts.

1 set of lead lined nuts for air expansion cylinder cover.

A quantity of packings and joint rings.

Where one duplex or two single dry air machines are fitted to each compartment the following will be required:—

1 crank shaft with eccentric sheaves complete, or one half shaft if the halves are interchangeable.

1 piston rod and nuts for steam and air cylinders.

1 set of connecting rod and crosshead brasses.

1 piston for H.P. steam cylinder.

1 piston, complete, for air compressor; and 1 for air expansion cylinder.

1 set of piston springs for each steam cylinder.

1 cylinder cover for each pattern used in air compression and expansion cylinders.

1 air pump bucket and rod.

1 circulating pump bucket and rod.

Main and cut-off slide valves and spindles with nuts complete for H.P. steam cylinder.

Balance springs and rings for steam and air slide valves.

1 H.P. steam cylinder valve and valve face with screws.

1 eccentric sheave, strap, and rod for each pattern used.

1 slide valve spindle and nuts for steam and air cylinders for each pattern used.

2 main bearing bolts.

1 set of connecting rod and piston rod bolts.

Half set of air valves and seats for air compressor.

1 inlet and 1 outlet valve, and half set of valve faces (if fitted) for air expansion cylinder, with screws.

1 set of valves for air, circulating, and feed pumps.

1 set of escape valve springs.

20 suction springs.

40 delivery springs.

40 buffer springs.

6 tubes and 24 ferrules for condenser.

6 tubes for cooler and 6 for air drying chamber.

Assorted bolts, studs and nuts.

 $\frac{1}{2}$ set of lead lined nuts for air expansion cylinder cover. A quantity of packings and joint rings.

Where one single ammonia or carbonic anhydride compression machine is fitted:—

1 crank shaft with eccentric sheaves, complete, or one half shaft if the halves are interchangeable.

Piston and rods complete with nuts for each steam cylinder and gas compressor.

1 air pump bucket and rod.

1 circulating pump bucket and rod.

1 pair main bearing brasses, complete.

1 set of connecting rod and crosshead brasses.

Main and cut-off valves for steam cylinders.

1 valve spindle for each pattern used and nuts complete.

1 eccentric strap and rod for each pattern used.

1 brine pump complete.

- 1 cover for each pattern used.
- 2 main bearing bolts.
- 1 set of connecting rod and piston rod bolts.
- 1 set compressor suction and delivery valves with springs and boxes, complete.
- 1 set of valves for air, circulating, feed, and brine pumps.

Crank shaft for fan engine.

- 1 steam piston and rod, etc., for fan engine, complete.
- 1 pair of connecting rod brasses for fan engines, with bolts, etc., complete.
- 1 set of blocks for making all leather packings used.
- 6 tubes and 24 ferrules for condenser.
- Lengths and bends of piping of each size used, together with flanges, couplings, and screwing apparatus for effecting repairs.
- 1 gas regulating valve.
- 1 distributing and 1 collecting piece with multiple branches for coils for each pattern used. If these pieces are made of forged steel no spare pieces are required.

Sundry valves, cocks, flanges, and fittings.

Assorted bolts, studs, and nuts.

Quantity of leather packings and joint rings.

For ammonia and carbonic anhydride compression machines, the following spare gear will be required, where one duplex or two single machines are fitted to each compartment:—

- 1 crank shaft, or one half shaft if the halves are interchangeable.
- 1 steam piston rod and nut for each pattern used.
- 1 piston for H.P. steam cylinder, with springs, complete.
- 1 set of piston rings for each steam cylinder.
- 1 set of piston rings for each size of compressor.
- 1 compressor piston rod and nuts, complete, for each pattern used.
- 1 air pump bucket and rod.
- 1 circulating pump bucket and rod.
- Main and cut-off slide valves for H.P. steam cylinder.
- Main and cut-off valve spindles and nuts for H.P. steam cylinder.
- 1 eccentric sheave, strap, and rod, for each pattern used.
- 1 brine pump complete.
- 1 cover for each end of gas compressor, except where screwed plugs are used.

- 2 main bearing bolts.
- $\frac{1}{2}$ set of connecting rod and piston rod bolts.
- $\frac{1}{2}$ set compressor suction and 1 delivery valve with springs and box, complete.
- 1 set of valves for air, circulating, feed, and brine pumps.
- 1 steam piston and rod, etc., for fan engine, complete.
- 1 pair of connecting rod brasses for fan engines, with bolts, etc., complete.
- 1 set of blocks and leather for making all leather packings used.
- 6 tubes and 24 ferrules for condenser.
- Lengths and bends of piping of each size used, together with flanges, couplings, and screwing apparatus for effecting repairs.
- 1 gas regulating valve.
- 1 distributing and 1 collecting piece with multiple branches for coils for each pattern used. If these pieces are made of forged steel no spare pieces are required.

Sundry valves, cocks, flanges and fittings.

Assorted bolts, studs and nuts.

A quantity of joint rings.

In cases where an independent circulating water pump is used, and its work *cannot* be performed by the main or auxiliary engines, a duplicate pump complete should be fitted.

In cases where an independent circulating water pump is used, and its work can be performed by the main or auxiliary engines, a pump bucket and rod should be carried, and $\frac{1}{2}$ set of valves for water end.

In cases where an independent surface condenser with air, circulating and feed pumps combined is fitted, and its work *cannot* be performed by the main engines:—

- 1 crank shaft with eccentric sheaves complete.
- 1 piston and rod complete for each pattern used.
- 1 eccentric strap and rod complete for each pattern used.
- 1 slide valve and spindle complete for each pattern
- 1 pump bucket and rod complete for each pattern used.
- 1 set of connecting rod and piston rod bolts and nuts,
- 1 set of valves for air, circulating, and feed pumps.
- 6 condenser tubes and 12 ferrules.

In cases where an independent surface condenser with air, circulating, and feed pumps combined is fitted, and its work can be performed by the main engines:—

- 1 pump bucket and rod complete for each pattern used.
- 1 set of connecting rod and piston rod bolts and nuts.
- 1 set of valves for air, circulating, and feed pumps.
- 6 condenser tubes and 12 ferrules.

Periodical Surveys.

- 4. In the cases of vessels engaged on voyages of more than three months' duration, a complete examination, as detailed in par. 9, is required every voyage. If this examination is made at other than the loading port a further examination is required at the loading port. (See par. 11.)
- 5. In the cases of vessels engaged on voyages of more than two and not more than three months' duration, a complete examination as above detailed is required at each alternate voyage, but at the intermediate voyage a modified examination as described in par. 10 will be sufficient, but the survey at loading port provided for in par. 11 should be held every voyage.
- 6. In vessels engaged on shorter over-sea voyages, the above examinations are to be held at least every three months, alternate examinations being as provided for in pars. 9 and 10, but the survey at loading port provided for in par. 11 should be held every voyage.

In the cases of vessels engaged on voyages of only a few days' duration, the complete examinations are to be held at least every three months, alternate examinations being as provided for in pars. 9 and 10, but the examination of insulation, etc., provided for in par. 11, instead of being held every voyage need only be held at intervals of four or six weeks, as may be approved in each special case.

- 7. If in any case only part of the requisite examinations is held, the certificate will be endorsed with a statement of what is required to complete the survey.
- 8. The date following the record R.M.C. in red indicates the date of the last examination of the Refrigerating Machinery and appliances as above mentioned.

When the periodical Surveys provided for in pars. 4, 5 and 6 are not held, the record R.M.C. will be expunged.

9. The complete periodical Survey required in par. 4 will consist of the following:—

The insulation throughout the holds is to be carefully examined and tested for dryness and fullness by sounding with a hammer and by boring. The test holes are to be afterwards efficiently closed. Special attention is to be paid to the spaces under the snow boxes, trunks and hatches where dampness may accumulate, to the sides under stringers and under decks and to the tunnel tops. All limber hatches are to be removed, the limbers cleared, and the suction pipes and roses, sluices and sounding pipes are to be examined. Hatches, air trunk-ways and thermometer tubes with their connections and fastenings are to be examined, and where trunk-ways pass through watertight bulkheads, the watertight doors are to be examined and worked.

The trunk-ways should be as airtight as practicable and their fastenings should be secure.

The steam pipes, water pipes and connections, the crank shaft and bearings, connecting rods, steam and air cylinders, pistons, slides and valves, compressors and pistons, compressor rods and glands, surface condenser and air or gas coolers, circulating, air, feed and bilge pumps, are to be carefully examined and the condensers and coolers tested if deemed necessary.

The auxiliary machinery, where fitted, is also to be examined.

The spare gear is to be examined.

In dry air machines special attention is to be given to the condition of the air expansion cylinders, their pistons and valves. In other machines special attention is to be given to the condition of the compressors, including the pistons, rods and glands, and to the expansion valve.

The refrigerator coils and their connections and the brine pipes and tanks, where fitted, are to be carefully examined and tested if deemed necessary.

Where the brine may escape to the bilges, the cement is to be examined.

The machinery is to be examined under working conditions, and tested on the snow box or refrigerators, the time and fall of temperature being noted.

It is recommended that the examination of the machinery under working conditions should be made upon the vessel's arrival at a home port, before the cargo is fully discharged. Where brine pipes are fitted they should be examined when under frosted conditions.

10. The examination required at alternate voyages in pars. 5 and 6 will consist of the following:—

The Insulation and Trunkways are to be surveyed in the same manner as is required for the complete examination detailed above. (See par. 9.)

Provided the machinery when tested under working conditions is found to be satisfactory, the following parts only will be required to be examined at this Survey, viz.:—

Steam valves, air pump and circulating pump.

Crank shafts and bearings.

Air and other compressors and valves.

Expansion cylinder and valves in dry air machines.

Condenser water spaces.

Sea injection valves to be opened whenever the vessel is in dry dock.

Brine pipes in holds under frosted conditions.

The spare gear.

11. If the machinery and insulation have been surveyed and passed at a home port, the further survey required at a loading port will consist of an inspection to ascertain that the dunnage battens are in good order and that no damage has been sustained to the insulation prior to the loading of the refrigerated cargo, and also of a test of the refrigerating machinery under working conditions, the temperature in the hold being noted.

If the vessel loads at more than one port, one survey only at a loading port will be required, provided it includes the examination of all insulated spaces.

If there is no Surveyor to the Society available at the loading ports, or if there is not one obtainable from a port within a reasonable distance, this survey may be held at the

port where the outward cargo is discharged. If there is no Surveyor to the Society at either of these ports, the Committee will accept the report of a survey held by a Surveyor appointed by Lloyd's Agent; or (in any case where there is no Lloyd's Agent) the report of a survey by a reliable Surveyor, if available; or (if no such Surveyor is available) a report signed by two competent Engineers of the vessel.

Fees.

12. The following are the charges that will be made for carrying out the above examination in the cases of classed vessels:—

		Durin	g etion.	8	ent ys yage.	
For installations under 80,000 cubic	£	S.	d.	£	s.	d.
feet total capacity	6	0	0	3	0	0
For installations under 120,000 cubic feet total capacity	8	0	0	4	0	0
For installations above 120,000 cubic feet total capacity	10	0	0	5	0	0

As regards Unclassed Vessels the fees for the first survey of Refrigerating Machinery and Appliances will be double the amounts in column No. 1 when the survey is held during construction, and double the amounts in column No. 2 when it is held after the Installation has been fitted. Fees for subsequent surveys will be charged in accordance with column No. 2 as printed.

By order of the Committee,

ANDREW SCOTT,

Secretary.

71, FENCHURCH STREET, LONDON, E.C. 15th December, 1910.

EXTRACTS FROM THE RULES

OF THE LATE

UNDERWRITERS' REGISTRY FOR IRON VESSELS (FOR 1884-85)

(NOW UNITED WITH LLOYD'S REGISTER OF SHIPPING),

SHOWING THE CONDITIONS OF CLASSIFICATION, &c.

REVISION OF CERTIFICATE OR SUSPENSION OF CLASS.

The certificate of class will remain good so long as the vessel, under periodical survey, is found worthy of it. In case of defects reported by the Surveyors not being made good, the class of the vessel will be revised or suspended by the Committee.

REFERENCE IN CASE OF COMPLAINT.

Any dispute shall be referred to three Shipbuilders or Engineers, one to be chosen by the Shipowner, one to be chosen by this Committee, and a third to act as umpire, to be chosen by the other two.

SURVEY FEES.

For surveying vessels periodically to ascertain condition, first visit £1 1 0

For each succeeding visit, when more than one visit is necessary ... 0 10 6

For special surveys special charges will be made, subject to the control of the Committee.

PERIODICAL SURVEYS.

A thorough survey will be required once in every four years for vessels with an A1* or an A1* certificate; and once in every three years for vessels with an A1, A1, A or an A certificate. When vessels are abroad at the time

they become due for survey, they must be examined on their return to the United Kingdom. The Surveyors are at all times to have free access to examine vessels holding a class in this Registry.

Vessels due for Periodical Survey which leave the United Kingdom without being duly surveyed and passed by the Surveyors to this Registry will have their class suspended until such survey has been properly made. Notice of Suspension of Class will be given in the first Supplement issued after the sailing of the vessel.

Vessels remaining abroad for two years after they become due for Periodical Survey will have their Class suspended until they have been re-surveyed.

First Survey.

The vessel to be placed in dry dock. (The bottom may be cleaned, but should not be recoated before survey.) While in dry dock the rudder, rudder pins and gudgeons, and the whole of the bottom outside, are to be thoroughly examined, and in steamers the connections of the sea-cocks and openings in the bottom are to be examined, to see that they are in an efficient condition.

The holds, and, in steamers, the bunkers also, are to be cleared, the loose ceiling in the flat of bottom is to be lifted, and the Surveyor is to satisfy himself that the bottom inside is in good order, and that the cement is in good condition and satisfactorily adhering to the iron.

He is also to examine the decks, beam ends, and the sides of holds and 'tween decks, all fore and aft. In steamers the bilges and limbers under engines and boilers are to be cleaned out, so as to allow these parts to be examined by the Surveyor. In water-ballast steamers the tanks are to be examined externally and, if the Surveyor deems it necessary, they are to be tested under the pressure due to the ballast-trim water-line, and sufficient ceiling removed to enable the Surveyor to satisfy himself of their tightness. In all cases the tanks are to be emptied, and examined inside. In all vessels any repairs that may be needed are to be done, and the vessel cleaned and painted as may be necessary.

Second Survey.

The vessel to be submitted to the same survey as before described for "First Survey," with the following additions:—

A strake of ceiling must be lifted in the bilges to allow an examination of the condition of the iron surfaces there and of the cement.

The windlass must be unhung when the main piece is of wood; and the chain cables must be ranged out for examination. In steamers the water ballast tanks must be tested under the pressure due to ballast-trim water-line.

Third Survey.

The vessel to be submitted to the same survey as before described for "First Survey," with the following additions:—

The whole of the close ceiling must be removed, and all the cement exposed and examined. The vessel must be cleaned and scaled, and, if the Surveyor deems it necessary, the plating and other parts must be drilled as he may direct, to ascertain the thickness. In steamers the water ballast tanks must be tested under the pressure due to ballast-trim water-line.

Fourth Survey.

The vessel to be submitted to the same survey as before described for "First Survey," with the following additions:—

The windlass, if the main piece is of wood, must be unhung, and the chain cables ranged out for examination. In steamers the water ballast tanks must be tested under the pressure due to the ballast-trim water-line.

Fifth Survey.

The vessel must be submitted to the same survey as before described for "Second Survey."

Sixth Survey or Special Survey.

The vessel must be submitted to the same survey as before described for "Third Survey," with the following additions:—

The actual condition and thickness of all the scantlings must be ascertained, the shell plating being drilled on at least three vertical lines in each strake, viz., forward, amidships, and aft, and elsewhere, at the discretion of the Surveyor, as he may direct.

A report of the vessel's condition and scantlings is to be submitted to the Committee, and such part or parts as they may direct are to be renewed, or otherwise strengthened.

After a vessel has passed her sixth survey, and been approved by the Committee she must be submitted to the same series of surveys, commencing with the "First Survey," and at the same periodical intervals as before.

In steamers, whenever the engines or boilers are removed, a survey is to be held on the vessel's bottom in way thereof, and such repairs as are necessary must be effected before the engines or boilers are replaced.

The preceding rules for periodical surveys are not to limit the Surveyor's discretion, if, in his judgment, it is necessary to make a more complete examination at any time; and, before completing the report, the Surveyor must, at every periodical survey, satisfy himself that the vessel and her equipment are in a good and efficient condition.

The "Third Survey" must be complied with before the expiration of thirteen years from the date of launch for vessels with an A1* or A1* certificate, ten years for vessels with an A1 or A1 certificate, and nine years for vessels with an A or A certificate; and the "Sixth Survey" before the expiration of twenty-six years from the date of launch for vessels with an A1* or A1* certificate, twenty years for vessels with an A1 or A1 certificate, and eighteen years for vessels with an A1 or A2 certificate.

EXTRACTS FROM THE RULES of the late UNDERWRITERS' REGISTRY FOR IRON VESSELS (for 1884-85)

(NOW UNITED WITH LLOYD'S REGISTER OF SHIPPING).

EQUIPMENT FOR STEAM VESSELS.

Section 29.—The equipment of Anchors and Chain Cables and Hawsers to be in accordance with Table 14 for Steam Vessels (see below).

The tonnage regulating equipment is to be the gross register tonnage under upper deck, with the addition of three-tenths of the tonnage of erections above upper deck.

TABLE No. 14.—ANCHORS, CHAINS, AND HAWSERS FOR STEAM VESSELS.

		Anchors, with either Iron or Wood Stocks.						Stud-chain Cables.			1 18 8 6		Hawsers and Warps.						
VESSELS		Number.			W	Weight.								8 3				VESSELS	
TONNAGE. Number. See Section 29.	Number.		Number		Во	wers.			£nd	Minimum Size.	Proved to Admiralty Test.	Length.	Stream	Chain.	Tow Rope.	Hawsers.	Warps.	Length.	TONNAGE. See Section 29.
See Section 20.	Bowers	Stream.	Kedges.	Without Stock.	Admiralty Test.	Stream.	Kedge.	Kedge.		Test.		18				6 6		See Section 29.	
Tons. 100 and 150 150 ,, 188 188 ,, 225 225 ,, 263 263 ,, 300 300 ,, 375 375 ,, 450 450 ,, 525 525 ,, 600 600 ,, 675 675 ,, 750 750 ,, 900 900 ,, 1050 1050 ,, 1200	2 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 2 2 2 2 2 2 2 2 2 2	$ \begin{array}{c} \text{Owt.} \\ 3 \\ 4 \\ 5\frac{1}{4} \\ 6 \\ 7\frac{1}{4} \\ 8\frac{1}{4} \\ 10 \\ 12 \\ 13\frac{1}{2} \\ 15\frac{1}{4} \\ 16\frac{3}{4} \\ 18 \\ 21 \\ 23\frac{1}{2} \end{array} $	Tons. 4·9 6·4 7·6 8·2 9·5 10·4 12·0 13·9 15·2 16·7 18·0 19·0 21·6 23·5	Cwt. 1 $1\frac{3}{4}$ 2 $2\frac{1}{2}$ $3\frac{3}{4}$ 3 $4\frac{3}{4}$ 5 6 $6\frac{1}{2}$ 7 8 9 10	Owt 1 $1\frac{1}{4}\frac{1}{4}\frac{1}{4}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}$ 3 $3\frac{1}{4}\frac{1}{4}\frac{1}{2}\frac{1}{2}$ 4 $4\frac{1}{2}\frac{1}{2}$ 5	Owt,	Inches. $\begin{array}{c} 11\\ 1\\ 1\\ 1\\ 6\\ 1\\ 1\\ 6\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\$	Tons. 8·1 11·9 13·8 15·8 18 20·3 22·8 25·4 28·1 31 34 37·2 40·5 44	Fathoms. 120 150 165 165 165 195 210 240 240 240 270	Fatn., 45 45 45 45 45 60 60 60 60 60 75 75	Size. 8 16 9 16 16 16 16 16 16 16 16 16 16 16 16 16	Inches. $5\frac{1}{2}$ 6 6 6 $6\frac{1}{2}$ 7 $7\frac{1}{2}$ 8 $8\frac{1}{2}$ 9 $9\frac{1}{2}$ 10 10 10 10	Inches. $3\frac{1}{2}$ 4 4 5 $5\frac{1}{2}$ 6 $6\frac{1}{2}$ 7 8 8 9 9	Inches	Fath. 90 90 90 90 90 90 90 90 90 90 90 90 90	Tons. 100 and 150 150 , 183 188 , 226 225 , 263 , 300 300 , 375 , 450 450 , 525 525 , 600 600 , 675 , 750 , 900 , 1050 1050 , 120	
1200 ,, 1350 1350 ,, 1500 1500 ,, 1800 1800 ,, 2100 2100 ,, 2400 2400 ,, 2700 2700 ,, 3000 3000 ,, 3450 3450 ,, 3900 3900 ,, 4500 4500 ,, 5250 5250 ,, 6000	3 3 3 3 3 3 3 4 4 4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$ \begin{array}{c} 25\frac{7}{2}\\ 27\frac{3}{4}\\ 30\\ 32\\ 34\\ 36\frac{1}{2}\\ 38\\ 40\\ 41\\ 43\\ 45\\ 47 \end{array} $	25·2 26·9 28·6 30·1 31·6 33·4 34·5 35·7 37·0 38·0 39·2 41	$ \begin{array}{c} 10\frac{1}{2} \\ 11 \\ 12 \\ 13 \\ 13\frac{1}{2} \\ 14 \\ 14\frac{1}{2} \\ 15 \\ 16 \\ 17\frac{1}{2} \\ 19 \\ 21 \end{array} $	$\begin{array}{c} 5\frac{1}{4} \\ 5\frac{1}{2} \\ 6 \\ 6\frac{1}{2} \\ 3\frac{3}{4} \\ 7 \\ 7\frac{1}{4} \\ 7\frac{1}{2} \\ 8 \\ 8\frac{1}{2} \\ 9\frac{1}{2} \\ 10 \\ \end{array}$	$\begin{array}{c} 2\frac{3}{4}\frac{3}{4}\\ 2\frac{1}{4} \\ 2\frac{1}{4} \\ 3\frac{1}{4} \\ 3\frac{1}{4} \\ 3\frac{1}{4} \\ 3\frac{1}{4} \\ 4\frac{1}{2} \\ 4\frac{3}{4} \\ 4\frac{3}{4} \\ 5 \\ \end{array}$	$\begin{array}{c} 1_{16}^{10} \\ 1_{16}^{11} \\ 1_{16}^{11} \\ 1_{16}^{12} \\ 1_{16}^{13} \\ 1_{16}^{14} \\ 1_{16}^{15} \\ 2_{16}^{15} \\ 2_{16}^{16} \\ 2_{16}^{16} \\ 2_{16}^{16} \\ 2_{16}^{16} \\ 2_{16}^{16} \end{array}$	47.5 51.2 55.1 59.1 63.3 67.6 72 76.6 81.3 86.1 91.1	270 270 270 270 270 270 270 270 270 300 300 330	75 75 75 75 75 90 90 90 90 90	$\begin{array}{c} 1\\ 1\\ 1\\ 1\\ \frac{1}{16}\\ 1\\$	10 10 11 11 11 12 12 12 12 12 12 12 12	$\begin{array}{c} 9\frac{1}{2} \\ 10 \\ 10\frac{1}{2} \\ 11 \\ 11 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ $	6 6 6 6 1 7 7 8 8 8 8 9 9	90 90 90 90 90 90 90 90 90 90 90	1200 ", 135 1350 ", 150 1500 ", 180 1800 ", 210 2100 ", 240 2400 ", 270 2700 ", 300 3000 ", 345 3450 ", 390 3900 ", 450 4500 ", 525 5250 ", 600	

Anchors and Chains to be tested to Admiralty proof. A reduction of 15 per cent. will be allowed in the weight of the Third and Fourth Bower.

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING.

STEEL MANUFACTURERS.

The following firms having applied to have the steel produced by them tested by a Surveyor to this Society and their mode of procedure reported upon, their applications have been complied with and the Surveyors' reports found satisfactory by the Committee.

FIRMS IN THE UNITED KINGDOM.

Acme Steel and Foundry Co., Shettleston, near Glasgow. (Steel castings.)

Allan, Edgar, & Co., Lim., Imperial Steel Works, Tinsley, Sheffield. (Steel castings.)

Armstrong (Sir W. G.), Whitworth & Co., Lim., Elswick, Northumberland, and Openshaw, Manchester. (Steel castings.)

Baird, Archibald, & Son, Lim., Hamilton, near Glasgow. (Steel castings.)

Barrow Hæmatite Steel Co., Lim., Barrow-in-Furness.

Beardmore, William, & Co., Lim., Steel Works, Rolling Mills and Foundry, Parkhead, Glasgow; and Steel Works and Rolling Mills, Mossend, Lanarkshire.

Bell Bros., Lim., Port Clarence, Middlesbro'-on-Tees.

Bessemer, H., & Co., Lim., Bessemer Works, Sheffield, Yorkshire; and Bolton, Lancashire.

Blackett, Hutton & Co., Cleveland Steel and Iron Works, Guisborough, Yorkshire. (Steel castings.)

Blaydon Iron Works (The), Blaydon-on-Tyne. (Steel castings.)

Bolckow, Vaughan & Co., Lim., Middlesbro'-on-Tees.

British Mannesmann Tube Co., Lim., Landore, S. Wales. (Weldless rolled or drawn steel hollow pillars and davits.)

Brown, John, & Co., Lim., Sheffield.

Brymbo (The) Steel & Ingot Iron Works, near Wrexham, Denbighshire. (For bars only.)

Butterley Co., Lim., Codnor Park, near Alfreton, Derbyshire.

Caledonian Steel Castings Co., Helen Street, Govan, Glasgow.

Cammell Laird & Co., Lim., Sheffield.

Cargo Fleet Iron Co., Lim., Cargo Fleet Iron Works, near Middlesbro'-on-Tees.

Carntyne Steel Castings Co., Moorpark, Renfrew. (Steel castings.)

Clydebridge Steel Co., Lim., Steel Works and Rolling Mills, Cambuslang, near Glasgow.

Coltness Iron Co., Lim., Melting Furnace and Foundry, Newmains, Lanarkshire.

Colville, David, & Sons, Lim., Steel Works and Rolling Mills (Dalzell Steel and Iron Works), Motherwell, Lanarkshire.

Consett Iron Co., Lim., Blackhill, Durham.

Darlington Forge Co., Lim., Darlington, co. Durham. (Steel castings.)

Dorman, Long & Co., Lim., Middlesbro'-on-Tees, and Port Clarence, co. Durham.

Dudley's (The Earl of) Round Oak Iron and Steel Works, Lim., Brierley Hill, Staffordshire (Sections and Bars.)

Dunlop, J., & Co. (1900), Lim., Steel Works and Rolling Mills, Calderbank, Lanarkshire.

Firth, Thomas, & Sons, Lim., Norfolk Works, Sheffield.

Frodingham Iron & Steel Co., Lim., Frodingham, near Doncaster, Yorkshire. (Sections and Bars.)

Glasgow Iron & Steel Co., Lim., Steel Works and Rolling Mills at Wishaw, Lanarkshire.

Glengarnock Iron and Steel Co., Lim., Glengarnock, Ayrshire. (Sections and Bars.)

Guest, Keen & Nettlefolds, Lim.,

Dowlais (Glamorgan) and Cardiff. (Plates and Bars.)

Castle Works, Tydu, near Newport, Mon. (Rivet and Stay bars.)

London Works, near Birmingham. (Rivet bars only.)

Hadfield's Steel Foundry Co., Lim., Sheffield. (Steel castings.)

Hardie & Gordon, Melting Furnaces and Foundry, Levenbank Foundry, Dalreoch, Dumbarton.

Jackson, P. R., & Co., Lim., Salford Rolling Mills, Manchester.

Jessop, W., & Sons, Lim., Brightside Works, Sheffield.

Jopling, E., & Sons, Pallion, Sunderland. (Steel castings.)

Lanarkshire Steel Co., Lim., Motherwell, Lanarkshire. (Sections and Bars.)

Lancashire & Yorkshire Railway Co., Horwich, Lancashire. (Steel castings.)

Leeds Forge Co., Lim., Leeds.

Lloyd, F. H., & Co., Lim., James Bridge, near Wednesbury, Staffordshire. (Steel castings.)

Lumb, James, & Sons, Lim., Elland, Yorkshire. (Steel castings.)

Monks, Hall & Co., Lim., Warrington. (Rolling Mills for bars.)

Motherwell Iron & Steel Co., Lim., Motherwell, Lanarkshire. (Rolling mills for angles, and round and flat bars.)

Newport Rolling Mills, Lim., Middlesbro'-on-Tees.

Osborn, S., & Co., Clyde Stee! & Iron Works, Sheffield. (Steel castings.)

Palmers Shipbuilding & Iron Co., Lim., Jarrow-on-Tyne.

Park Gate Iron & Steel Co., Lim., Rotherham, Yorkshire.

Patent Shaft & Axletree Co., Lim., Wednesbury, Staffordshire.

Pather Iron & Steel Co., Lim., Wishaw, Lanarkshire. (Rolling Mills.)

Port Talbot Steel Co., Lim., Port Talbot, South Wales.

Raine & Co., Lim., Delta Iron & Steel Works, Derwenthaugh, Newcastle-on-Tyne. (Rivet bars only.)

Rennie's Steel Casting Co., Maukinfauld Road, Tollcross, Glasgow. (Steel castings.)

Renton & Fisher, Lim., Hopetoun Steel Works, Bathgate, N.B. (Steel castings.)

Richmond Iron & Steel Co., Richmond Iron Works, Stockton-on-Tees. (Rolling Mills for Stay and Rivet bars.)

Rogerson, John, & Co., Lim., Wolsingham, co. Durham. (Steel castings.)

Shaw, W., & Co., Middlesbro'-on-Tees. (Steel castings.)

Shelton Iron, Steel & Coal Co., Lim., Stoke-on-Trent.

Skinningrove Iron Co., Lim. (The), Skinningrove, Carlin How, R.S.O., Yorks. (Steel ingots only.)

Smith & McLean, Lim., Rolling Mills at Mossend and Gartcosh, Lanarkshire.

South Durham Steel & Iron Co., Lim., Stockton-on-Tees and West Hartlepool.

Spencer, John, & Sons, Lim., Newburn Steel Works, Newcastle-on-Tyne.

Springfield Steel Co., Lim., Melting Furnace and Foundry, 777, London Road, Glasgow.

Steel Company of Scotland, Lim., Steel Works, Rolling Mills and Foundry at Newton, Glasgow; and Steel Works and Rolling Mills at Blochairn, Glasgow.

Steel, Peech & Tozer, Lim., Sheffield. (Rivet and Stay bars.)

Stewarts & Lloyds, Lim. (Clydesdale Steel and Iron Works), Steel Works and Rolling Mills, Mossend, Lanarkshire.

" , Sun Foundry, Coatbridge, Lanarkshire. (Steel castings.)

Stockton Steel Foundry Co., Lim., Stockton-on-Tees. (Steel castings.)

Swalwell Steel Works, co. Durham. (Steel castings.)

Taylor Bros., Leeds.

Towler, William, & Co., Lim., Globe Foundry, Leeds. (Small steel castings.)

Tyzack, Samuel, & Co., Lim., Monkwearmouth Iron & Steel Works, Sunderland. (Sections and Bars.)

Vickers, Lim., River Don Works, Sheffield; and Barrow-in-Furness.

Waverley Iron & Steel Co., Lim., Coatbridge, Lanarkshire. (Steel angles and bars.)

Weardale Steel, Coal & Coke Co., Lim., Spennymoor, co. Durham.

Wigan Coal & Iron Co., Lim., Wigan, Lancashire. (Sections and Bars.)

Willans & Robinson, Lim., Queen's Ferry, Flintshire. (Steel ingots.)

FOREIGN FIRMS.

ALPHABETICALLY ARRANGED.

In the following list the name of each works is followed by the place of residence of the Surveyor giving attendance thereat.

Acciaierie Italiane, Bolzaneto, Italy. (GENOA.)

Aciéries de Grenelle (E. Plichon), 56, Rue Lourmel, Paris. (Steel castings.) (HAVRE.)

Aciéries de la Louvière (Gustave Boël), La Louvière, Belgium. (Sections and Rivet bars, and Steel castings.) (Antwerp.)

Aciéries de Maromme (E. Breton), Maromme (Seine Inférieure), France. (Steel castings.) (HAVRE.)

Actien-Gesellschaft Charlottenhütte, Niederschelden (Kreis Siegen), Germany. (Steel plates and ingots.) (Düsseldorf.)

Actien-Gesellschaft der Dillinger Hüttenwerke, Dillingen-Saar (Rheinpreussen), Germany. (DÜSSELDORF.)

Aktiebolaget Bofors-Gullspång, Bofors, Sweden. (Melting Furnaces and Foundry at Bofors.) (GOTHENBURG.)

Aktiengesellschaft der Eisen-und Stahlwerke, vormals Georg Fischer, Schaffhausen, Switzerland. (Steel castings.) (Düsseldorf.)

Aktiengesellschaft Lauchhammer, Lauchhammer, Germany. (Steel Foundry at Gröditz.) (Steel castings.) (DÜSSELDORF.)

Alan Wood Iron & Steel Company, Conshohocken and Ivy Rock, Pa. (Blooms, billets and thin plates.) (Philadelphia.)

Althaus, Pletsch & Co., Attendorn, Westphalia, Germany. (Rolling Mills.) (Düsseldorf.)

American Bridge Co., Pencoyd Iron Works, Pencoyd, Pa., U.S.A. (Sections, angles and bars.) (PHILADELPHIA.)

American Iron & Steel Manufacturing Co., Lebanon, Pa., U.S.A. (Rolling Mills for bars only.) (BALTIMORE.)

American Iron & Steel Manufacturing Co., Reading, Pa., U.S.A. (Rolling Mills for bars only.) (Philadelphia.)

Annener Gussstahlwerk, Annen, Westphalia, Germany. (Steel castings.) (Düsseldorf.)

Ansaldo, Gio., Armstrong & Co., Fonderie & Acciaierie, Cornigliano Ligure, Italy. (Steel castings.) (Genoa.)

Avesta Jernverks Aktiebolag, Avesta, Sweden. (Stock-Holm.)

Baldt Steel Co., New Castle, Delaware, U.S.A. (Steel castings.) (Philadelphia.)

Bergische Stahl-Industrie, Remscheid, Germany. (Steel ingots and castings.) (Düsseldorf.)

Bethlehem Steel Co., South Bethlehem, Philadelphia. (Philadelphia.)

Bismarckhütte (Bismarckhütte & Falvahütte), Bismarckhütte, Oberschlesien, Germany. (Also steel castings, and weldless rolled or drawn steel hollow pillars and davits.) (VIENNA.)

Björneborgs Jernverks Aktiebolag, Björneborg, Sweden. (Melting Furnaces and Forge.) (GOTHENBURG.)

Blechwalzwerk Schulz Knaudt Actien Gesellschaft. (Steel Works at Angerort, Germany; Rolling Mills at Essen.) (Düsseldorf.)

Bleckmann, John E., Mürzzuschlag, Austria. (Steel bars.) (Vienna.)

Blohm & Voss, Hamburg, Germany. (Steel castings.) (Hamburg.)

Bochumer Verein für Bergbau & Gussstahlfabrication, Bochum, Germany. (Steel castings.) (DÜSSELDORF.)

Böhler, Gebr., & Co., Aktiengesellschaft, Vienna. (Works at Kapfenberg, Styria.) (Steel castings.) (VIENNA.)

Borsig, A. (Berg und Hütten-Verwaltung), Borsigwerk, Oberschlesien, Germany. (Also Steel castings.) (VIENNA.)

Bremerhütte Actien Gesellschaft, Weidenau, Siegen, Germany. (Steel Works at Geisweid. Rolling Mills at Weidenau.) (Steel plates and ingots.) (DÜSSELDORF.)

Burmeister & Wain's Maskin-og Skibsbyggeri, Aktieselskabet, Copenhagen. (Steel ingots, forgings and castings.) (COPENHAGEN.)

Cambria Steel Co., Johnstown, Pa., U.S.A. (PITTSBURG.)

Carbon Steel Co., Pittsburg, Pa., U.S.A. (PITTSBURG.)

Carnegie Steel Co. (Lim.), Pittsburg, Pa., U.S.A. (including the National Steel Co., and the American Steel Hoop Co.) (PITTSBURG.)

Central Iron & Steel Co., Harrisburg, Pa., U.S.A. (Rolling Mills.) (BALTIMORE.)

Christiania Staalværk, Christiania. (Steel castings.) (Christiania.)

Compagnie des Forges de Chatillon, Commentry et Neuves-Maisons, France. (MARSEILLES.)

Compagnie des Hauts-Fourneaux, Forges et Acièries de la Marine et d'Homecourt, St. Chamond, France. (Marseilles.)

Compagnie des Mines, Fonderies & Forges d'Alais, Tamaris Works, Alais, France. (Bars and Sections.) (MARSEILLES.)

Compagnie Générale des Aciers, Société Anonyme, Thy-le-Château, Belgium. (Steel castings.) (Antwerp.)

Crucible Steel Company of America, Park Works, Pittsburg, Pa., U.S.A. (PITTSBURG.)

Deutsch Luxemburgische Bergwerks-und Hütten-Actien Gesellschaft, Abteilung Dortmunder Union, Dortmund, Germany. (Also Steel castings.) (Düsseldorf.)

Dorémieux Fils & Cie., St. Amand (Nord), France. (Rolling Mills.) (Dunkirk.)

Düsseldorfer Eisen-und Draht-Industrie, Düsseldorf-Oberbilk, Germany. (Düsseldorf.)

Eisen und Stahlwerk Hoesch, Dortmund, Germany. (Düsseldorf.)

Eisenbahn-Bedarfs Actien Gesellschaft, Friedenshütte Oberschlesien, Germany. (VIENNA.)

Eisenhütte Holstein Actiengesellschaft, Rendsburg, Germany. (Hamburg.)

Elektrizitäts-Aktien-Gesellschaft, vormals Kolben & Co., Prague-Vysocan, Bohemia. (Steel castings.) (VIENNA.)

Erie Forge Co., Erie, Pa., U.S.A. (Steel ingots and forgings.) (CLEVELAND, O.)

Fabrique de Fer de Maubeuge, Louvroil (Nord), France. (Dunkirk.)

Federal Steel Co., Chester, Pa., U.S.A. (Steel castings.) (Philadelphia.)

Ferriera di Bolzaneto, near Genoa. (For plates up to $\frac{3}{4}$ in. thickness.) (GENOA.)

Fonderia Milanese di Acciaio, Milan. (Steel castings.) (GENOA.)

Fonderies, Forges et Aciéries de St. Etienne, St. Etienne, France. (MARSEILLES.)

Fonderies d'Acier du Midi, Marseilles. (Steel castings.) (Marseilles.)

Forges de Clabecq, Clabecq, Belgium. (Rolling Mills.)
(ANTWERP.)

Forges de la Loire et du Midi (Messrs. Marrel Frères) Rive de Gier, France. (MARSEILLES.)

Forges & Laminoirs de l'Alliance, Marchienne au Pont, Belgium. (Rolling Mills.) (Antwerp.)

Forges et Laminoirs de St. Victor, Société Anonyme, Marchienne au Pont, Belgium. (Steel bars.) (Antwerp.)

Ganz & Co., Ratibor, Silesia, Germany. (Steel castings.)
(VIENNA.)

Geisweider Eisenwerke Actien Gesellschaft, Geisweid (Kreis Siegen), Germany. (Düsseldorf.)

Gelsenkirchener Bergwerks Actien Gesellschaft, Abteilung Aachener Hütten Verein, Rothe Erde, Aachen, Germany. (DÜSSELDORF.)

Gelsenkirchener Gussstahl und Eisenwerke, vormals Munscheid & Co., Gelsenkirchen, Germany. (Steel castings.) (Düsseldorf.)

Georgs-Marien Bergwerks-und Hütten-Verein, Osnabrück, Germany. (Steel castings.) (Düsseldorf.)

Gewerkschaft Deutscher Kaiser, Hamborn-Bruckhausen am Rhein, Germany. (Düsseldorf.)

Gewerkschaft Grillo, Funke & Co., Gelsenkirchen Schalke, Westphalia, Germany. (Düsseldorf.)

Glasgow Iron Co., Pottstown, Pa. (Rolling Mills for plates.) (Philadelphia.)

Grafenberger Walzwerk, Düsseldorf-Grafenberg, Germany. (Rolling Mills.) (DÜSSELDORF.)

Gruson (Otto) & Co., Magdeburg-Buckau, Germany. (Steel castings.) (Düsseldorf.)

Gussstahl-Werk Witten, Witten a/d Ruhr, Germany. (Düsseldorf.)

Gutehoffnungshütte, Oberhausen, Rheinland, Germany. (Also Steel castings.) (DÜSSELDORF.)

Hagener Gussstahlwerke Actien Gesellschaft, Hagen, Westphalia, Germany. (Steel castings.) (Düsseldorf.)

Hahnsche Werke Actien Gesellschaft, Grossenbaum, near Duisburg, Germany. (*Broad flats and ingots.*) (Düsselder.)

Haniel & Lueg, Düsseldorf-Grafenberg, Germany. (Steel castings.) (Düsseldorf.)

Hauts-Fourneaux, Fonderies Forges & Laminoirs de Meurthe & Moselle (Mr. Fould-Dupont), Usines de Pompey, France. (DÜSSELDORF.)

Henschel & Sohn, Abteilung Henrichshütte, near Hattingen a/d Ruhr, Germany. (Düsseldorf.)

Holtzer, Jacob, & Co., Aciéries d'Unieux, Unieux (Loire), France. (Steel castings.) (MARSEILLES.)

Howaldtswerke, Kiel, Germany. (Steel castings.) (Hamburg.) Illinois Steel Co., Chicago, U.S.A. (PITTSBURG.)

Imperial Steel Works (The), Yawata, Japan. (Nagasaki.) Jaeger, G. & J., G.m.b.h., Elberfeld, Germany. (Steel

castings.) (Düsseldorf.)

Japan Steel Works, Lim. (The), Muroran, Japan. (Steel ingots and forgings.) (NAGASAKI.)

Jones & Laughlin, Lim., Pittsburg, Pa., U.S.A. (PITTSBURG.)

Kawasaki Dockyard Co., Lim., Shiri-ike-mura, Hiogo, Japan. (Steel castings.) (Kobe.)

Kohlswa Jernverks Aktiebolag. (Melting Furnaces and Foundry at Kohlswa, Sweden.) (Sтоскноім.)

Krainische Industrie-Gesellschaft, Assling-Hütte, Carniole, Austria. (Vienna.)

Krupp, Fried., Actien Gesellschaft, Stahlwerk Annen, Annen, Westphalia, Germany. (Steel castings.) (Düssel-DORF.)

Krupp, Fried., Actien Gesellschaft, Essen, Germany. (Also Steel castings.) (Düsseldorf.)

Krupp, Fried., Actien Gesellschaft, Grusonwerk, Magdeburg, Germany. (Steel castings.) (Düsseldorf.)

Krupp, Fried., Actien Gesellschaft—Friedrich Alfred Hütte, Rheinhausen — Friemersheim, Germany. (Bars and Sections only.) (DÜSSELDORF.)

Lackawanna Steel Co., Buffalo, N.Y., U.S.A. (PITTSBURG.)

- Lindener Eisen- & Stahlwerke Aktien-Gesellschaft, Hannover-Linden, Germany. (Steel castings.) (Düsseldorf.)
- Luken's Iron and Steel Company, Coatesville, Pennsylvania, U.S.A. (PHILADELPHIA.)
- Luxemburger Bergwerks-und Saarbrücker Eisenhütten-Actien Gesellschaft, Saarbrücken - Burbach, Germany. (Düsseldorf.)
- Magyar Kiralyi Allamvasutak Gepgyaranak. (Rolling Mills at Zolyom-Brezo; Rolling Mills and Steel Foundry at Diosgyor, Hungary.) (Vienna.)
- Malleable Iron Fittings Co., Branford, Conn. (Steel castings.) (Boston, Mass.)
- Mannesmannröhrenwerke, Abteilung Saarbrücker Gussstahlwerke, Saarbrücken Burbach, Germany. (Steel castings.) (DÜSSELDORF.)
- Mannesmannröhrenwerke, Düsseldorf, Remscheid und Bous, Germany. (Weldless rolled or drawn steel hollow pillars and davits.) (DÜSSELDORF.)
- Michaelsen, Hermann, Eisen-und Stahl-Giesserei, Erdmannstrasse, 23, Altona-Ottensen, Germany. (Steel castings.) (Hamburg.)
- Midvale Steel Co., Philadelphia, Pa., U.S.A. (PHILADEL-PHIA.)
- Motala Verkstads Nya Aktiebolag, Motala Verkstad, Sweden. (Melting Furnaces, Rolling Mills and Forge.) (GOTHENBURG.)
- Neuberg Steel Works, Neuberg, Styria. (VIENNA.)
- Nicopol-Marioopol Mining & Metallurgical Co., Sartana, South Russia. (ODESSA.)
- Nova Scotia Steel & Coal Co. (Lim.) (Steel Works at North Sydney, C.B., and Rolling Mills at New Glasgow, N.S.) (Bars and Sections only.) (Halifax, N.S.)
- Oberbilker Stahlwerk Actien Gesellschaft, Düsseldorf-Oberbilk, Germany. (DÜSSELDORF.)
- Oberschlesische Eisen-Industrie Actien Gesellschaft, Baildonhütte, near Kattowitz, Germany. (VIENNA.)
- Oesterreichisch-Alpine Montangesellschaft, Donawitz, near Leoben. (Vienna.)
- Oesterreichisch-Alpine Montangesellschaft, Zeltweg, Austria. (Vienna.)
- Oesterreichische Berg und Hüttenwerks, Gesellschaft, Teschen, Silesia. (Vienna.)
- Oliver Iron & Steel Co., Pittsburg, Pa., U.S.A. (Rolling Mills for bars.) (PITTSBURG.)
- Penn Steel Casting & Machine Co., Chester, Pa., U.S.A. (Steel castings.) (Philadelphia,)
- Pennsylvania Steel Co., Steelton, near Harrisburg, Pa. (BALTIMORE.)
- "Phœnix" Actien Gesellschaft für Bergbau-und Hütten Betrieb, Ruhrort, Germany. (DÜSSELDORF.)

- " Phœnix " Actien Gesellschaft für Bergbau-und Hütten Betrieb, Abteilung Düsseldorfer Röhren und Eisen-Walzwerke, Düsseldorf-Oberbilk, Germany. (Düsseldorf.)
- "Phœnix" Actien Gesellschaft für Bergbau-und Hütten Betrieb, Abteilung Hoerder Verein, Hoerde, Westphalia, Germany. (Also Steel castings.) (DÜSSELDORF.)
- Phœnix Iron Works, Phœnixville, Pa., U.S.A. (PHILA-DELPHIA.)
- Pittsburg Steel Foundry, Glassport, Pa., U.S.A. (Steel castings and Ingots.) (PITTSBURG.)
- Poldihütte Tiegelgussstahlfabrik, Kladno, near Prague. (Vienna.)
- Prager Eisen Industrie Gesellschaft und Böhmische Montan Gesellschaft, Kladno, near Prague. (VIENNA.)
- Press und Walzwerk Actien Gesellschaft, Düsseldorf-Reisholz, Germany. (DÜSSELDORF.)
- Rheinische Bergbau und Hüttenwesen Actien Gesellschaft. (Steel Works at Duisburg-Hochfeld, Germany. Rolling Mills at Düsseldorf-Oberbilk.) (DÜSSELDORF.)
- Rheinische Stahlwerke, Ruhrort, Germany. (Düsseldorf.)
- Rheinische Stahlwerke, Abteilung Duisburger Eisen-und Stahlwerke, Duisburg, Germany. (DÜSSELDORF.)
- Rimamurany-Salgo-Tarjaner Eisenwerks Actien-Gesell-schaft, Budapest. (Steel Works in Ozd, Hungary.) (VIENNA.)
- Rombacher Hüttenwerke, Rombach (Lothringen), Germany. (Bars and Sections only.) (Düsseldorf.)
- Sandvikens Jernverks Aktiebolag, Sandviken, Sweden. (Steel ingots, forgings, and steel tubes.) (STOCKHOLM.)
- Schichau, F., Elbing, West Prussia, Germany. (Steel castings.) (Danzig.)
- Schneider & Co., Creusot. (MARSEILLES.)
- Skodawerke Actien Gesellschaft, Pilsen, Bohemia. (Steel castings.) (VIENNA.)
- Sociedad Altos Hornos de Vizcaya, Bilbao. (BILBAO.)
- Sociedad Anonima Fabrica de San Francisco del Desierto, Bilbao. (BILBAO.)
- Sociedad Metalurgica Duro-Felguera, La Felguera, Asturias, Spain. (BILBAO.)
- Società degli Alti Forni, Fonderie ed Acciaierie di Terni. Works at Terni. (Naples.)
- Società Ligure Metallurgica, Lim., Sestri Ponente, Italy. (GENOA.)
- Società Siderurgica di Savona (late Tardy & Benech) Savona. (Genoa.)
- Société Anonyme Boulonneries & Laminoirs Gilson, La Croyère (Bois d'Haine), Belgium. (Rolling Mills for Sections.) (Antwerp.)

Société Anonyme d'Athus-Grivegnée, Grivegnée, near Liège, Belgium. (Bars, Sections, and Thin Plates.) (Antwerp.)

Société Anonyme d'Escaut & Meuse, Anzin (Nord), France. (Dunkirk.)

Société Anonyme d'Espérance, Longdoz, Liège. (Rolling Mills.) (Antwerp.)

Société Anonyme de la Fabrique de Fer de Charleroi, Belgium. (Rolling Mills.) (Antwerp.)

Société Anonyme des Aciéries d'Angleur, Renory & Tilleurlez-Liége, Belgium. (Antwerp.)

Société Anonyme des Aciéries & Fonderies d'Art de Haine St. Pierre et Métallurgique Lilloise, Haine St. Pierre, Belgium. (Steel castings.) (Antwerp); and Lesquinlez-Lille (Nord), France. (Steel castings.) (Dunkirk.)

Société Anonyme des Aciéries & Forges de Firminy, Firminy (Loire), France. (Steel castings.) (Marseilles.) Société Anonyme des Aciéries Nantaises, Nantes. (Steel

castings.) (NANTES.)

Société Anonyme des Fonderies et Aciéries de Hirson, Hirson, France. (Steel castings.) (HAVRE.)

Société Anonyme des Forges de la Providence, Hautmont (Nord), France. (Dunkirk.)

Société Anonyme des Forges de Vireux-Molhain, Vireux-Molhain, Ardennes, France. (Bars and Sections only.) (Antwerp.)

Société Anonyme des Forges et Fonderies de Montataire, Montataire, France. (HAVRE.)

Société Anonyme des Forges et Laminoirs de Baume, Haine St. Pierre, Belgium. (Rolling Mills for Bars and Sections.) (Antwerp.)

Société Anonyme des Forges et Tôleries Liégeoises, Jupillelez-Liège. (Antwerp.)

Société Anonyme des Hauts-Fourneaux, Fonderies & Forges de Franche-Comté, Besançon (Doubs), France. (Marseilles.)

Société Anonyme des Hauts-Fourneaux Forges et Aciéries de Denain & d'Anzin, Denain (Nord), France. (Dunkirk.)

Société Anonyme des Tôleries de Louvroil (Nord), France. (Dunkirk.)

Société Anonyme des Usines du Phénix, Châtelineau, Belgium. (Rolling Mills.) (ANTWERP.)

Société Anonyme Usines & Aciéries Leonard-Giot, Marchienne-au-Pont, Belgium. (Steel castings.) (ANTWERP.)

Société des Aciéries de Longwy, Mont St. Martin (Meurthe & Moselle), France. (DÜSSELDORF.)

Société Française des Aciéries de l'Union, Hautmont (Nord), France. (Steel castings.) (DUNKIRK.)

Société Française pour la Fabrication des Tubes, Louvroil (Nord), France. (Steel ingots and steel tubes.) (Dunkirk.)

Société John Cockerill, Seraing, near Liège, Belgium. (Antwerp.)

Stahlwerk Oeking, Actien Gesellschaft, Düsseldorf-Lierenfeld, Germany. (Steel castings.) (DÜSSELDORF.)

Steirische Gussstahlwerke Danner & Co., Iudenburg, Styria. (Steel castings.) (VIENNA.)

Stora Kopparbergs Bergslags Aktiebolag, Falun, Sweden.
(Steel Works at Domnarfvet.) (Sections of all sizes and plates up to $\frac{3}{4}$ in. thick.) (STOCKHOLM.)

Strömmens Verksted, near Christiania. (Steel castings.) (Christiania.)

Strömsnäs Jernverks Aktiebolag, Degerfors, Sweden (Melting Furnaces and Rolling Mills.) (GOTHENBURG.)

Sumitomo Steel Works, Osaka, Japan. (Steel castings.) (Kobe.)

Surahammars Bruks Aktiebolag, Surahammar, Sweden. (Forge and Rolling Mills.) (STOCKHOLM.)

Ternitzer Stahl und Eisenwerk, Ternitz, Austria. (Steel bars and castings.) (VIENNA.)

Thyssen & Co., Mülheim, a/d. Ruhr, Germany. (Düssel-porf.)

Tidewater Steel Company, Chester, Pennsylvania, U.S.A. (Philadelphia.)

Ungarische Berg-und Hüttenwerke und Domänen der priv. österr.-ung. Staats-Eisenbahn-Gesellschaft, Budapest. (Steel Works in Resicza.) (VIENNA.)

Usines & Aciéries Allard, Société Anonyme, Mont-sur-Marchienne, near Charleroi, Belgium. (Steel castings.) (Antwerp.)

Usines de Court St. Etienne (Emile Henricot), Belgium. (Steel castings.) (Antwerp.)

Usines Métallurgiques de Hainaut, Couillet and La Louvière, Belgium. (Antwerp.)

Usines Métallurgiques de la Basse Loire, Trignac, near St. Nazaire. (Nantes.)

Vereinigte Königs- & Laurahütte Act. Ges., für Bergbau & Hüttenbetrieb, Königshütte & Laurahütte, Oberschlesien, Germany. (VIENNA.)

Vereinigte Stahlwerke van der Zypen und Wissener Eisenhütten Actien Gesellschaft, Köln-Deutz, Germany. (Bars and Sections.) (Düsseldorf.)

Wendel & Cie., les Petits-Fils de Fois de, Hayingen, Lothringen, Germany. (DÜSSELDORF.)

Westfälische Stahlwerke, Bochum, Germany. (Steel Foundry and Rolling Mills.) (Düsseldorf.)

Witkowitzer Bergbau & Eisenhütten Gewerkschaft, Witkowitz, Mähren. (VIENNA.)

Worth Bros. Steel Works, Coatesville, Pa. (PHILADELPHIA.)

FOREIGN FIRMS.

ARRANGED ACCORDING TO SURVEYING DISTRICTS.

ANTWERP.

Aciéries de la Louvière (Gustave Boël), La Louvière, Belgium. (Sections and Rivet bars, and Steel castings.)

Compagnie Générale des Aciers Société Anonyme, Thyle-Château, Belgium. (Steel castings.)

Forges de Clabecq, Brussels, Belgium. (Rolling Mills.)

Forges & Laminoirs de l'Alliance, Marchienne-au-Pont, Belgium. (Rolling Mills.)

Forges & Laminoirs de St. Victor, Société Anonyme, Marchienne-au-Pont, Belgium. (Steel bars.)

Société Anonyme Boulonneries & Laminoirs Gilson, La Croyère (Bois d'Haine), Belgium. (Rolling Mills for Sections.)

Société Anonyme d'Athus-Grivegnée, Grivegnée, near Liège, Belgium. (Bars, Sections, and Thin Plates.)

Société Anonyme d'Espérance, Longdoz, Liège. (Rolling Mills.)

Société Anonyme de la Fabrique de Fer de Charleroi, Belgium. (Rolling Mills.)

Société Anonyme des Aciéries d'Angleur, Renory & Tilleur-lez-Liège, Belgium.

Société Anonyme des Aciéries & Fonderies d'Art de Haine St. Pierre et Métallurgique Lilloise, Haine St. Pierre, Belgium. (Steel castings.)

Société Anonyme des Forges de Vireux-Molhain, Vireux-Molhain, Ardennes, France. (Bars and Sections only.)

Société Anonyme des Forges et Laminoirs de Baume, Haine St. Pierre, Belgium. (Rolling Mills for Bars and Sections.)

Société Anonyme des Forges et Tôleries Liègeoises, Jupille-lez-Liège, Belgium.

Société Anonyme des Usines du Phénix, Châtelineau, Belgium. (Rolling Mills.)

Société Anonyme Usines & Aciéries Leonard-Giot, Marchienne-au-Pont, Belgium. (Steel castings.)

Société John Cockerill, Seraing, near Liège.

Usines & Aciéries Allard, Société Anonyme, Mont-sur-Marchienne, near Charleroi, Belgium. (Steel castings.) Usines de Court St. Etienne (Emile Henricot), Belgium.

(Steel castings.)

Usines Métallurgiques de Hainaut, Couillet and La Louvière, Belgium.

BALTIMORE, MD.

American Iron & Steel Manufacturing Co., Lebanon, Pa., U.S.A. (Rolling Mills for bars only.)

Central Iron & Steel Co., Harrisburg, Pa., U.S.A. (Rolling Mills.)

Pennsylvania Steel Co., Steelton, Harrisburg, Pa., U.S.A.

BILBAO.

Sociedad Altos Hornos de Vizcaya, Bilbao.

Sociedad Anonima Fabrica de San Francisco del Desierto, Bilbao.

Sociedad Metalurgica Duro-Felguera, La Felguera, Asturias, Spain.

BOSTON, MASS.

Malleable Iron Fittings Co., Branford, Conn., U.S.A. (Steel castings.)

CHRISTIANIA.

Christiania Staalværk. (Steel castings.) Strömmens Verksted, near Christiania. (Steel castings.)

CLEVELAND, O.

Erie Forge Co., Erie, Pa., U.S.A. (Steel ingots and forgings.)

COPENHAGEN.

Burmeister & Wain's Maskin-og Skibsbyggeri, Aktie-selskabet, Copenhagen. (Steel ingots, forgings and castings.)

DANZIG.

Schichau, F., Elbing, West Prussia. (Steel castings.)

DUNKIRK.

Dorémieux Fils & Cie., St. Amand (Nord), France (Rolling Mills.)

Fabrique de Fer de Maubeuge, Louvroil (Nord), France. Société Anonyme d'Escaut & Meuse, Anzin (Nord), France.

Société Anonyme des Aciéries & Fonderies d'Art de Haine St. Pierre et Métallurgique Lilloise, Lesquinlez-Lille (Nord), France. (Steel castings.)

Société Anonyme des Forges de la Providence, Hautmont (Nord), France.

Société Anonyme des Hauts-Fourneaux Forges et Aciéries de Denain & d'Anzin, Denain (Nord), France.

Société Anonyme des Tôleries de Louvroil (Nord), France.

Société Française des Aciéries de l'Union, Hautmont (Nord), France. (Steel castings.)

Société Française pour la Fabrication des Tubes, Louvroil (Nord), France. (Steel ingots and steel tubes.)

DÜSSELDORF.

Actien-Gesellschaft Charlottenhütte, Niederschelden (Kreis Siegen), Germany. (Steel plates and ingots.)

Actien-Gesellschaft der Dillinger Hüttenwerke, Dillingen-Saar (Rheinpreussen), Germany.

Aktiengesellschaft der Eisen-und Stahlwerke, vormals Georg Fischer, Schaffhausen, Switzerland. (Steel castings.)

Aktiengesellschaft Lauchhammer, Lauchhammer, Germany. (Steel Foundry at Gröditz.) (Steel castings.)

Althaus, Pletsch & Co., Attendorn, Westphalia, Germany. (Rolling Mills.)

Annener Gussstahlwerk, Annen, Westphalia, Germany. (Steel castings.)

Bergische Stahl-Industrie, Remscheid, Germany. (Steel ingots and castings.)

Blechwalzwerk Schulz Knaudt Actien Gesellschaft, (Steel Works at Angerort, Germany; Rolling Mills at Essen.)

Bochumer Verein für Bergbau & Gussstahlfabrication, Bochum, Germany. (Steel castings.)

Bremerhütte Actien Gesellschaft, Weidenau, Siegen, Germany. (Steel Works at Geisweid. Rolling Mills at Weidenau.) (Steel plates and ingots.)

Deutsch Luxemburgische Bergwerks-und Hütten-Actien Gesellschaft, Abteilung Dortmunder Union, Dortmund, Germany. (Also Steel castings.)

Düsseldorfer Eisen-und Draht-Industrie, Düsseldorf-Oberbilk, Germany.

Eisen und Stahlwerk Hoesch, Dortmund, Germany.

Geisweider Eisenwerke Actien Gesellschaft, Geisweid (Kreis Siegen), Germany.

Gelsenkirchener Bergwerks Actien Gesellschaft, Abteilung Aachener Hütten Verein, Rothe Erde, Aachen, Germany.

Gelsenkirchener Gussstahl und Eisenwerke, vormals Munscheid & Co., Gelsenkirchen, Germany. (Steel castings.)

Georgs-Marien Bergwerks- und Hütten-Verein, Osnabrück, Germany (Steel castings.)

Gewerkschaft Deutscher Kaiser, Hamborn-Bruckhausen am Rhein, Germany.

Gewerkschaft Grillo, Funke & Co., Gelsenkirchen-Schalke, Westphalia, Germany.

Grafenberger Walzwerk, Düsseldorf - Grafenberg, Germany. (Rolling Mills.)

Gruson (Otto) & Co., Magdeburg-Buckau, Germany. (Steel castings.)

Gussstahl-Werk Witten, Witten a/d Ruhr, Germany.

Gutehoffnungshütte, Oberhausen, Rheinland, Germany. (Also Steel castings.)

DÜSSELDORF-continued.

Hagener Gussstahlwerke Actien Gesellschaft, Hagen, Westphalia, Germany. (Steel castings.)

Hahnsche Werke Actien Gesellschaft, Grossenbaum, near Duisburg, Germany. (Broad flats and ingots.)

Haniel & Lueg, Düsseldorf-Grafenberg, Germany. (Steel castings.)

Hauts-Fourneaux, Fonderies, Forges & Laminoirs de Meurthe & Moselle (Mr. Fould-Dupont), Usines de Pompey, France.

Henschel & Sohn, Abteilung Henrichshütte, near Hattingen a/d Ruhr, Germany.

Jaeger, G. & J., G.m.b.h., Elberfeld, Germany. (Steel castings.)

Krupp, Fried., Actien Gesellschaft, Stahlwerk Annen, Annen, Westfalen, Germany. (Steel castings.)

Krupp, Fried., Actien Gesellschaft, Essen, Germany. (Also Steel castings.)

Krupp, Fried., Actien Gesellschaft, Grusonwerk, Magdeburg, Germany. (Steel castings.)

Krupp, Fried., Actien Gesellschaft—Friedrich Alfred Hütte, Rheinhausen — Friemersheim, Germany. (Bars and Sections only.)

Lindener Eisen- & Stahlwerke Aktien- Gesellschaft, Hannover-Linden, Germany. (Steel castings.)

Luxemburger-Bergwerks und Saarbrücker Eisenhütten-Actien-Gesellschaft, Saarbrücken-Burbach, Germany.

Mannesmannröhrenwerke, Abteilung Saarbrücker Gussstahlwerke, Saarbrücken-Burbach, Germany. (Steel castings.)

Mannesmannröhrenwerke, Düsseldorf, Remscheid und Bous, Germany. (Weldless rolled or drawn Steel hollow pillars and davits.)

Oberbilker Stahlwerk Actien Gesellschaft, Düsseldorf-Oberbilk, Germany.

"Phœnix" Actien Gesellschaft für Bergbau-und Hütten Betrieb, Ruhrort, Germany.

"Phœnix" Actien Gesellschaft für Bergbau-und Hütten Betrieb, Abteilung Düsseldorfer Röhren und Eisen-Walzwerke, Düsseldorf-Oberbilk, Germany.

"Phœnix" Actien Gesellschaft für Bergbau-und Hütten Betrieb, Abteilung Hoerder Verein, Hoerde, Westphalia, Germany. (Also Steel castings.)

Press und Walzwerk Actien Gesellschaft, Düsseldorf-Reisholz, Germany.

Rheinische Bergbau und Hüttenwesen Actien Gesellschaft. (Steel Works at Duisburg-Hochfeld, Germany; Rolling Mills at Düsseldorf-Oberbilk.)

Rheinische Stahlwerke, Ruhrort, Germany.

Rheinische Stahlwerke, Abteilung Duisburger Eisen und Stahlwerke, Duisburg, Germany.

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DÜSSELDORF-continued.

Rombacher Hüttenwerke, Rombach (Lothringen), Germany. (Bars and Sections only.)

Société des Aciéries de Longwy, Mont St. Martin (Meurthe & Moselle), France.

Stahlwerk Oeking Actien Gesellschaft, Düsseldorf-Lierenfeld, Germany. (Steel castings.)

Thyssen & Co., Mülheim, a.d. Ruhr, Germany.

Vereinigte Stahlwerke van der Zypen und Wissener Eisenhütten Actien Gesellschaft, Köln-Deutz, Germany. (Bars and Sections.)

Wendel & Cie., les Petits-Fils de Fois de Hayingen, Lothringen, Germany.

Westfälische Stahlwerke, Bochum, Westphalia, Germany. (Steel Foundry and Rolling Mills.)

GENOA.

Acciaierie Italiane, Bolzaneto, Italy.

Ansaldo, Gio., Armstrong & Co., Fonderie & Acciaierie, Cornigliano Ligure, Italy. (Steel castings.)

Ferriera di Bolzaneto, near Genoa. (For plates up to $\frac{3}{4}$ in. thickness.)

Fonderia Milanese di Acciaio, Milan. (Steel castings.) Società Ligure Metallurgica (Lim.), Sestri Ponente, Italy.

Società Siderurgica di Savona (late Tardy & Benech), Savona.

GOTHENBURG.

Aktiebolaget Bofors-Gullspång, Bofors, Sweden. (Melting Furnaces and Foundry at Bofors.)

Björneborgs Jernverks Aktiebolag, Björneborg, Sweden. (Melting Furnaces and Forge.)

Strömsnäs Jernverks Aktiebolag, Degerfors, Sweden. (Melting Furnaces and Rolling Mills.)

Motala Verkstads Nya Aktiebolag, Motala Verkstad, Sweden. (Melting Furnaces, Rolling Mills and Forge.)

HALIFAX, N.S.

Nova Scotia Steel & Coal Co. (Lim.) (Steel Works at North Sydney, C.B., and Rolling Mills at New Glasgow, N.S.) (Bars and Sections only.)

HAMBURG.

Blohm & Voss. (Steel castings.)

Eisenhütte Holstein Actiengesellschaft, Rendsburg, Germany.

Howaldtswerke, Kiel. (Steel castings.)

Michaelsen, Hermann, Eisen-und Stahl-Giesserei, Erdmannstrasse, 23, Altona-Ottensen. (Steel castings.)

HAVRE.

Aciéries de Grenelle (E. Plichon), 56, Rue Lourmel, Paris. (Steel castings.)

Aciéries de Maromme (E. Breton), Maromme (Seine Inférieure), France. (Steel castings.)

Société Anonyme des Fonderies et Aciéries de Hirson, Hirson, France. (Steel castings.)

Société Anonyme des Forges et Fonderies de Montataire, Montataire, France.

KOBE.

Kawasaki Dockyard Co., Lim., Shiri-ike-mura, Hiogo, Japan. (Steel castings.)

Sumitomo Steel Works, Osaka, Japan. (Steel castings.)

MARSEILLES.

Compagnie des Forges de Chatillon, Commentry et Neuves-Maisons, France.

Compagnie des Hauts-Fourneaux, Forges et Aciéries de la Marine et d'Homecourt, St. Chamond, France.

Compagnie des Mines, Fonderies & Forges d'Alais, Tamaris Works, Alais, France. (Bars and Sections.)

Fonderies, Forges et Aciéries de St. Etienne, St. Etienne, France.

Fonderies d'Acier du Midi, Marseilles. (Steel castings.)
Forges de la Loire et du Midi (Messrs. Marrel Frères),
Rive de Gier, France.

Holtzer, Jacob, & Cie., Aciéries d'Unieux, Unieux, (Loire), France. (Steel castings.)

Schneider & Co., Creusot.

Société Anonyme des Aciéries & Forges de Firminy, Firminy (Loire), France. (Steel castings.)

Société Anonyme des Hauts-Fourneaux, Fonderies & Forges de Franche-Comté, Besançon (Doubs), France.

NAGASAKI.

The Imperial Steel Works, Yawata, Japan.

The Japan Steel Works, Lim., Muroran, Japan. (Steel ingots and forgings.)

NANTES.

Société Anonyme des Aciéries Nantaises, Nantes. (Steel castings.)

Usines Métallurgiques de la Basse Loire, Trignac, near St. Nazaire.

NAPLES.

Società degli Alti Forni, Fonderie ed Acciaierie di Terni, Works at Terni,

ODESSA.

Nicopol-Marioopol Mining & Metallurgical Co., Sartana, South Russia.

PHILADELPHIA, PA.

Alan Wood Iron & Steel Company, Conshohocken and Ivy Rock, Pa., U.S.A. (Blooms, billets and thin plates.)

American Bridge Co., Pencoyd Iron Works, Pencoyd, Pa., U.S.A. (Sections, angles and bars.)

American Iron & Steel Manufacturing Co., Reading, Pa., U.S.A. (Rolling Mills for bars only.)

Baldt Steel Co., New Castle, Delaware. (Steel castings.)
Bethlehem Steel Co., South Bethlehem, Philadelphia,
Pa., U.S.A.

Federal Steel Co., Chester, Pa., U.S.A. (Steel castings.)Glasgow Iron Co., Pottstown, Pa., U.S.A. (Rolling Mills for plates.)

Luken's Iron & Steel Company, Coatesville, Pa., U.S.A. Midvale Steel Co., Philadelphia, Pa., U.S.A.

Penn Steel Casting & Machine Co., Chester, Pa., U.S.A. (Steel castings.)

Phœnix 1ron Works, Phœnixville, Pa., U.S.A. Tidewater Steel Company, Chester, Pa., U.S.A.

Worth Bros. Steel Works, Coatesville, Pa., U.S.A.

PITTSBURG, PA.

Cambria Steel Co., Johnstown, Pa., U.S.A. Carbon Steel Co., Pittsburg, Pa., U.S.A.

Carnegie Steel Co., Lim., Pittsburg, Pa., U.S.A. (including the National Steel Co., and the American Steel Hoop Co.).

Crucible Steel Company of America, Park Works, Pittsburg, Pa., U.S.A.

Illinois Steel Co., Chicago, U.S.A.

Jones & Laughlin (Lim.), Pittsburg, Pa., U.S.A.

Lackawanna Steel Co., Buffalo, N.Y., U.S.A.

Oliver Iron & Steel Co., Pittsburg, Pa., U.S.A.

Pittsburg Steel Foundry, Glassport, Pa., U.S.A. (Castings and Ingots.)

STOCKHOLM.

Avesta Jernverks Aktiebolag, Avesta, Sweden.

Kohlswa Jernverks Aktiebolag. (Melting Furnaces and Foundry at Kohlswa, Sweden.)

Sandvikens Jernverks Aktiebolag, Sandviken, Sweden. (Steel ingots, forgings, and steel tubes.)

Stora Kopparbergs Bergslags Aktiebolag, Falun, Sweden. (Steel Works at Domnarfvet.) (Sections of all sizes and plates up to \(\frac{3}{4}\) ins. thick.)

Surahammars Bruks Aktiebolag, Surahammar, Sweden. (Forge and Rolling Mills.)

VIENNA.

Bismarckhütte (Bismarckhütte and Falvahütte), Bismarckhütte, Oberschlesien, Germany. (Also steel castings, and weldless rolled or drawn steel hollow pillars and davits.)

Bleckmann, John E., Mürzzuschlag, Austria. (Steel bars.)

Böhler, Gebr., & Co., Aktiengesellschaft, Vienna. (Works at Kapfenberg, Styria.) (Steel castings.)

Borsig, A. (Berg und Hütten-Verwaltung), Borsigwerk, Oberschlesien, Germany. (Also Steel castings.)

Eisenbahn-Bedarfs Actien Gesellschaft, Friedenshütte Oberschlesien, Germany.

Elektrizitäts-Aktien-Gesellschaft, vormals Kolben & Co., Prague-Vysocan, Bohemia. (Steel castings.)

Ganz & Co., Ratibor, Silesia, Germany. (Steel castings.)

Krainische Industrie-Gesellschaft, Assling-Hütte, Carniole, Austria.

Magyar Kiralyi Allamvasutak Gepgyaranak. (Rolling Mills at Zolyom-Brezo; Rolling Mills and Steel Foundry at Diosgyor, Hungary.)

Neuberg Steel Works, Neuberg, Styria.

Oberschlesische Eisen-Industrie Actien Gesellschaft, Baildonhütte, near Kattowitz, Germany.

Oesterreichisch-Alpine Montangesellschaft, Donawitz, near Leoben.

Oesterreichisch-Alpine Montangesellschaft, Zeltweg, Austria.

Oesterreichische Berg und Hüttenwerks Gesellschaft, Teschen, Silesia.

Poldihütte Tiegelgussstahlfabrik, Kladno, near Prague.

Prager Eisen Industrie Gesellschaft und Böhmische Montan Gesellschaft, Kladno, near Prague.

Rimamurany - Salgo - Tarjaner Eisenwerks Actien-Gesellschaft, Budapest. (Steel Works in Ozd, Hungary.)

Skodawerke - Actien Gesellschaft, Pilsen, Bohemia. (Steel castings.)

Steirische Gussstahlwerke Danner & Co., Iudenburg, Styria. (Steel castings.)

Ternitzer Stahl und Eisenwerk, Ternitz, Austria. (Steel bars and castings.)

Ungarische Berg-und Hüttenwerke und Domänen per priv. österr.-ung. Staats - Eisenbahn - Gesellschaft, Budapest. (Steel Works in Resicza.)

Vereinigte Königs- & Laurahütte Act. Ges., für Bergbau & Hüttenbetrieb, Königshütte & Laurahütte, Oberschlesien, Germany.

Witkowitzer Bergbau & Eisenhütten Gewerkschaft, Witkowitz, Mähren.

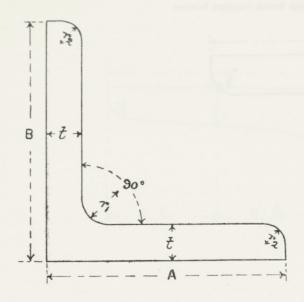
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BRITISH STANDARD SECTIONS.

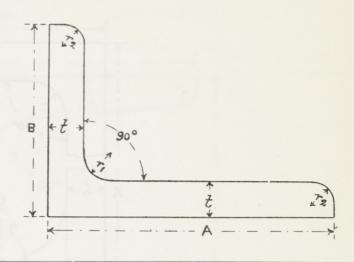
EQUAL ANGLES.

UNEQUAL ANGLES.

(NOTE;-The Section marked thus * is additional to the British Standard Sections.)



Size.		hickness a Standard		Mini-	Maxi-	Radii.		
A × B	Mini- mum.	Mean.	Maxi- mum.	mum thick- ness rolled.	mum thick- ness rolled.	Root.	Toe.	
	t	t	t	1011041	Tomour	r_1	r_2	
Inches.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch	
1×1	125	_	.250	.125	.300	.175	.125	
$1\tfrac{1}{4} \times 1\tfrac{1}{4}$.125		.250	.125	.300	200	150	
$1\tfrac{1}{2} \times 1\tfrac{1}{2}$.125	_	.250	.125	*350	·200	.150	
$1\tfrac{3}{4} \times 1\tfrac{3}{4}$.175	TT	.300	.175	.375	.225	.150	
2×2	.175	_	.300	.175	•400	.250	.175	
$2\tfrac{1}{4}\!\times\!2\tfrac{1}{4}$.175	-	.300	175	·450	.250	.175	
$2\tfrac{1}{2} \times 2\tfrac{1}{2}$.250	.375	.500	200	•500	275	.200	
$2\tfrac{3}{4} \times 2\tfrac{3}{4}$	•250	*375	.500	.225	.525	.275	.200	
3×3	.250	.375	.500	•250	:525	.300	.200	
$3\tfrac{1}{2} \times 3\tfrac{1}{2}$.300	•425	.500	•275	.575	.325	.225	
4×4	.300	.425	•500	.300	.625	.350	.250	
$4\tfrac{1}{2} \times 4\tfrac{1}{2}$.375	000	.500	.325	:650	.400	.275	
5×5	.375	(m)	.500	.350	.700	.425	.300	
6 × 6	•450	7	.625	.425	.775	.475	.325	
7 × 7	.500	-	.675	.475	.850	.550	.375	
8 ×8	.550	_	.750	.550	.950	.600	.425	

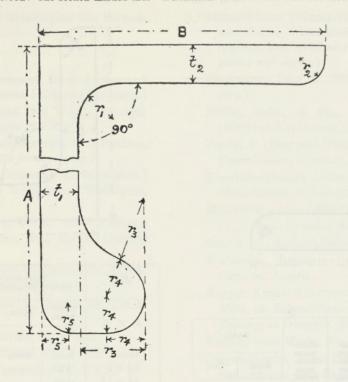


Size.	Correct	hickness a Standard	t Profile.	Mini-	Maxi-	Ra	dii.
A × B.	Mini- mum.	Mean.	Maxi- mum.	mum thickness rolled.	mum thickness rolled.	Roct.	Toe.
	t	t	t			r_1	7.2
Inches.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
$1\frac{1}{4} \times 1$	125		.250	125	.300	.175	125
$1\frac{1}{2} \times 1\frac{1}{4}$.125	-	.250	.125	*325	.200	.150
$1\frac{3}{4} imes 1\frac{1}{2}$.175	_	.300	·150	*350	.225	.150
$2 \times 1\frac{1}{2}$.175	-	.300	.175	.375	.225	.150
$2\frac{1}{2} \times 2$.175		.300	175	·450	.250	.175
3×2	250	.375	.200	.500	•500	.275	.200
$3 \times 2\frac{1}{2}$	250	.375	.500	.225	.525	.275	.200
$3\frac{1}{2} \times 2\frac{1}{2}$.250	.375	.500	.250	.525	.300	.200
$3\frac{1}{2} \times 3$	250	.375	.500	.250	.550	.325	.225
$4 \times 2\frac{1}{2}$.250	.375	.500	.250	.550	.325	.225
4 ×3	.300	.425	.500	.275	.575	.325	.225
$4 \times 3\frac{1}{2}$.300	.425	.500	.275	.600	.350	.250
$4\frac{1}{2} \times 3$.300	.425	.500	.275	.600	.350	.250
$4\frac{1}{2} \times 3\frac{1}{2}$.300	.425	.500	.300	.625	.350	.250
5×3	.300	.425	.500	.300	.625	*350	.250
$5 \times 3\frac{1}{2}$.375	-	.500	.325	.625	*375	.250
5 × 4	.375	_	.500	*325	.650	·400	.275
$5\frac{1}{2} \times 3$.375	_	.500	.325	.625	*375	.250
$5\frac{1}{2} \times 3\frac{1}{2}$.375	_	.500	.325	.650	·400	.275
6×3	.375	100	.500	.350	.675	.400	.275
$6 \times 3\frac{1}{2}$.375		.500	.350	.675	.400	.275
6×4	.375	_	.500	.350	.700	.425	.300
$*6\frac{1}{2} \times 3$.375	_	.500	.350	.700	.425	.300
$6\frac{1}{2} \times 3\frac{1}{2}$.375	-	.500	*350	.700	.425	.300
$6\frac{1}{2} \times 4\frac{1}{2}$.550	-	.400	.750	.450	.325
$7 \times 3\frac{1}{2}$	_	.525	-	.375	.725	.425	.300
7 × 4		.550	_	.400	.750	.450	.325
$8 \times 3\frac{1}{2}$.575	-	•400	.750	.475	*325
8 ×4	_	.625	_	.425	.775	.475	*325
9 ×4	_	.650	-	.450	.825	.500	*350
10 ×4	_	.675	-	.475	·850	.550	•375
			1	1			

BRITISH STANDARD SECTIONS.

BULB ANGLES.

(NOTE:-The Section marked thus * is additional to the British Standard Sections

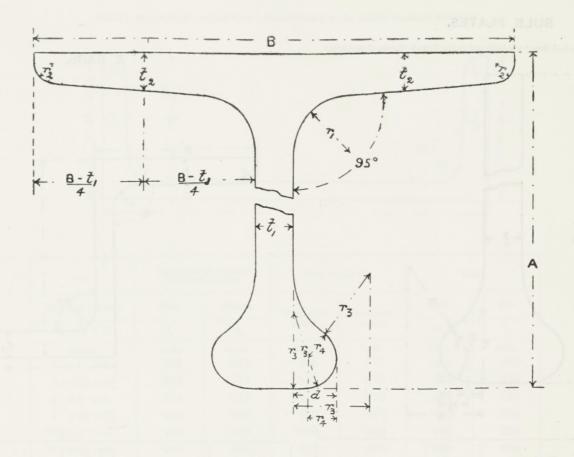


Size.	Thickness at Correct Standard Profile.			ickness.			Radii.				
002 000	Web Flange.		Maximum	Minimum	L oat	Bag-	908: 78				
A×B	t_1	t_2	rolled.	rolled.	r_1	r ₂	r_3	24	r5		
Inches.	1	nch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.		
5 × 3		325	.525	*325	.350	•250	.600	.350	.300		
$5\frac{1}{2} \times 3$		350	.550	'350	*375	.250	.650	.375	.325		
6 × 3		375	.575	*375	•400	.275	.675	•400	*325		
$6 \times 3\frac{1}{2}$		375	.575	.375	.400	.275	.675	•400	*325		
$6\frac{1}{2} \times 3$		375	.575	.375	•425	.275	.700	.425	*350		
$6\frac{1}{2} \times 3\frac{1}{2}$		400	.600	•400	.425	.275	.700	.425	.350		
7 ×3	·400		.600	·400	.450	.300	.750	.450	.375		
$7 \times 3\frac{1}{2}$.425		.625	.425	·450 ·	*300	.750	.450	.375		
$7\frac{1}{2} \times 3$		425	.625	.425	.475	*325	*800	.475	.400		
$7\frac{1}{2} \times 3\frac{1}{2}$		425	.625	*425	.475	*325	.800	.475	.400		
8 × 3		425	.625	•425	.500	.325	*825	.500	*400		
$8 \times 3\frac{1}{2}$		450	.650	•450	.500	.325	.825	.500	*400		
$8\frac{1}{2} \times 3$		450	.650	.450	.525	*350	.850	.525	.425		
$8\frac{1}{2} \times 3\frac{1}{2}$.475	.675	.475	.525	*350	.850	.525	.425		
9 × 3		.475	.675	.475	.550	*350	.900	.550	*450		
$9 \times 3\frac{1}{2}$	1 000	.475	.675	.475	.550	.350	.900	.550	.450		
$9\frac{1}{2} \times 3\frac{1}{2}$	1 100	.500	.700	.500	.550	.375	.950	.550	.475		
$10^{2} \times 3\frac{1}{2}$	060	.525	.725	.525	.575	.400	.975	.575	.500		
$10\frac{1}{2} \times 3\frac{1}{2}$		•525	.725	.525	.575	.400	.975	.575	.500		
$11 \times 3\frac{1}{2}$		•550	.750	.550	.625	425	1.050	.625	.525		
$*11\frac{1}{2} \times 3\frac{1}{2}$.575	.775	.575	.650	•450	1.100	.650	.550		
$12 \times 3\frac{1}{2}$	1 3 3 3 3	.575	.775	.575	.675	.450	1.125	.675	.550		
12 × 4		.600	.800	.600	.675	•450	1.125	.675	.550		

Where the thickness of Bulb Angle is greater than the Standard thickness, the flange and web will not be of the same thickness; generally for each '05 inch increase in the thickness of the web the thickness of the flange will be increased '025 inch.

BRITISH STANDARD SECTIONS.

BULB TEES.



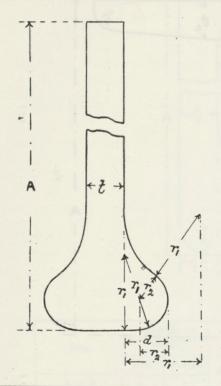
Size.	Thickness at correct Standard profile.		Web thickness.				Ra	dii.	
	Web.	Flange.	Maximum rolled.	Minimum rolled.					
A × B	t_1	t_2	rolled.	roned.	d	r_1	r_2	$r_{\rm s}$	r_4
Inches.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
7×5	.425	.425	.500	.350	. 450	.600	.200	.800	*300
$8 \times 5\frac{1}{2}$	·450	•450	.525	.375	.500	.675	.225	.900	*325
$9 \times 5\frac{1}{2}$	•475	•500	.550	·400	•575	.750	.250	1.000	.375
10×6	.500	.550	.575	•425	625	.825	.275	1.100	•400
$11 \times 6\frac{1}{2}$	•550	•600	.625	·475	.675	.900	.300	1.200	.450
$12 \times 6\frac{1}{2}$.575	.650	.650	.500	.725	.975	.325	1.300	.475

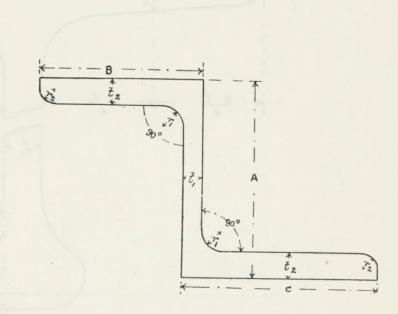
The standard thickness of flange of Bulb Tees is to be measured at a distance half way between the extreme edges of the flanges and the nearer side of the web.

BRITISH STANDARD SECTIONS.

BULB PLATES.

(NOTE:-The Section marked thus * is additional to the British Standard Sections.)





Z BARS.

Size.	Thickness at Correct Standard Profile.	Thiel	kness.		Radii.		
A	t	Maximum rolled.	Minimum rolled.	d	r_1	r ₂	
Inches.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	
*5	250	.350	200	.350	.550	•200	
6	.300	•400	.250	·400	.700	•250	
7	*350	•450	.275	•450	.800	·300 .	
8	•400	•525	•325	.500	.900	*325	
9	•450	•575	.350	•575	1.000	·375	
10	•500	625	*375	.625	1.100	. 400	
11	•550	.700	.425	.675	1.200	*450	
12	.600	.750	•450	.725	1.300	•475	

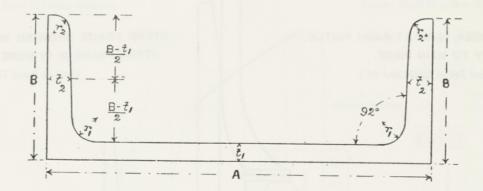
Size.	Thickness at Correct Standard Profile.		Web thickness.		Radii.	
Web and Flanges.	Web.	Flanges.	Maximum rolled.	Minimum rolled.	Root.	Toe.
A × B × C	t_1	t_2	Tolled.	Torred.	r_1	r_2
Inches.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch
$5 \times 3 \times 3$	*350	•450	•550	•350	*375	.250
$6 \times 3\frac{1}{2} \times 3\frac{1}{2}$.375	.475	.575	.375	·425	.300
$7 \times 3\frac{1}{2} \times 3\frac{1}{2}$	•400	*500	.600	•400	·450	*300
$8 \times 3\frac{1}{2} \times 3\frac{1}{2}$	·425	•525	·625	.425	·450	*325
$9 \times 3\frac{1}{2} \times 3\frac{1}{2}$	·450	•550	•650	·450	·475	*350
$10 \times 3\frac{1}{2} \times 3\frac{1}{2}$.475	.575	.675	.475	•500	*350

When the thickness of Zed bar is greater than the Standard thickness, the increase in thickness of flanges and web will not be the same; generally, for each '05 inch increase the thickness of the web, the flange will be increased '025 inch.

BRITISH STANDARD SECTIONS.

CHANNELS.

(Note:-The Sections marked thus * are additional to the British Standard Sections.)

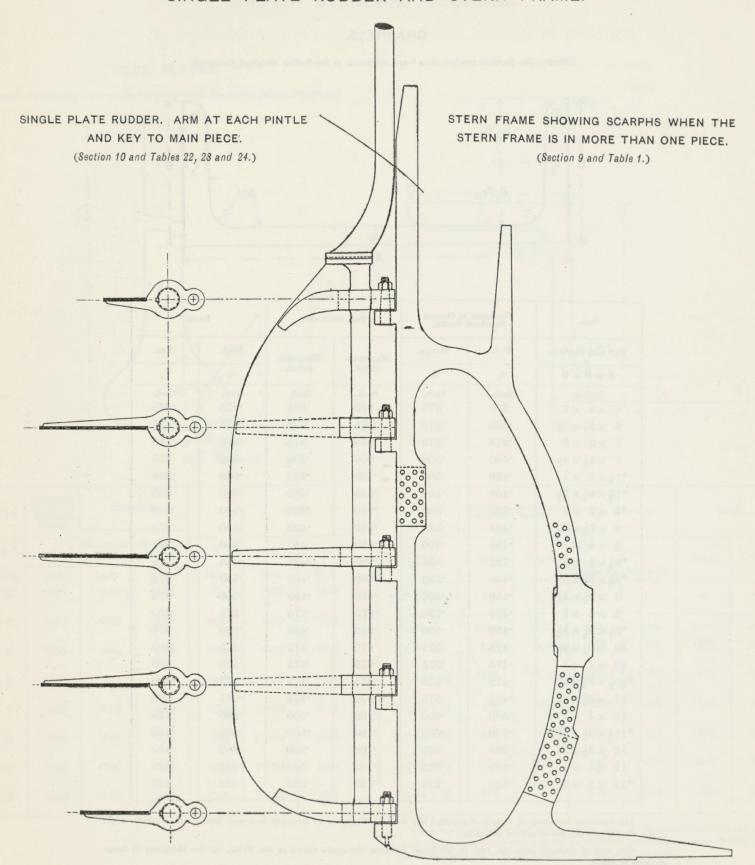


Size.	Thickness at Correct Standard Profile.		Web th	Web thickness.		Radii.	
Web and Flanges.	Web.	Flange.	Maximum	Minimum	Root.	Toe.	
$A \times B \times B$	t_1	t_2	rolled.	rolled.	r_1	r_2	
Inches.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	
6 ×3 ×3	.375	*475	.575	.375	.475	*325	
$6 \times 3\frac{1}{2} \times 3\frac{1}{2}$.375	•475	.575	.375	.475	.325	
7 ×3 ×3	.375	.475	.575	.375	.475	*325	
$7 \times 3\frac{1}{2} \times 3\frac{1}{2}$	·400	.500	.600	.400	.500	.350	
$*7\frac{1}{2} \times 3 \times 3$.400	.500	.600	•400	.500	.350	
$*7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2}$	•400	.500	.600	.400	.500	.350	
*8 ×3 ×3	•400	.500	.600	.400	.500	.350	
$8 \times 3\frac{1}{2} \times 3\frac{1}{2}$.425	.525	.625	•425	.525	.375	
8 ×4 ×4	*450	•550	.650	*450	.550	.375	
$*8\frac{1}{2} \times 3 \times 3$.425	. 525	.625	•425	.525	.375	
$*8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2}$. 450	.550	.650	*450	.550	.375	
$9 \times 3\frac{1}{2} \times 3\frac{1}{2}$	*450	•550	.650	.450	.550	.375	
$9 \times 4 \times 4$.475	.575	.675	.475	.575	.400	
$*9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2}$	*450	•550	•650	*450	.550	.375	
$10 \times 3\frac{1}{2} \times 3\frac{1}{2}$	475	•575	.675	•475	.575	.400	
10 ×4 ×4	.475	.575	.675	.475	.575	.400	
$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2}$.475	.575	.675	.475	.575	.400	
$11 \times 3\frac{1}{2} \times 3\frac{1}{2}$.475	•575	.675	.475	.575	.400	
11 ×4 ×4	•500	*600	.700	.500	.600	.425	
$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2}$.500	.600	.700	•500	.600	.425	
$12 \times 3\frac{1}{2} \times 3\frac{1}{2}$.500	.600	.700	.500	.600	.425	
12 ×4 ×4	.525	.625	.725	.525	.625	.425	
15 ×4 ×4	.525	.625	.725	.525	.625	.425	

The Standard thickness of flanges of Channel bar is to be measured at distances half-way between the extreme edges of the flanges and the nearer side of the web.

The web of Channel bars can vary in thickness between the limits shown in the Table, but the thickness of flange remains constant.

SINGLE PLATE RUDDER AND STERN FRAME.



COUPLINGS OF RUDDER HEADS.

Horizontal Coupling of Rudder Head.

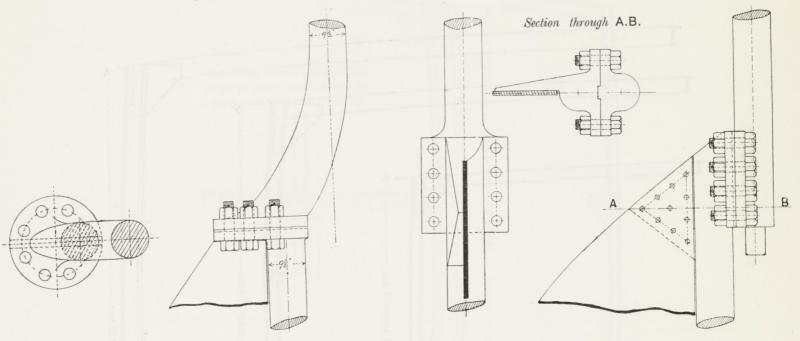
(Section 10 and Table 23.)

Rudder Head 9½ inches diameter

Vertical Coupling of Rudder Head.

(Section 10 and Table 23.)

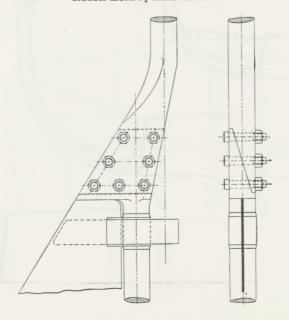
Rudder Head $9\frac{1}{2}$ inches diameter.



Scarphed Coupling of Rudder Head.

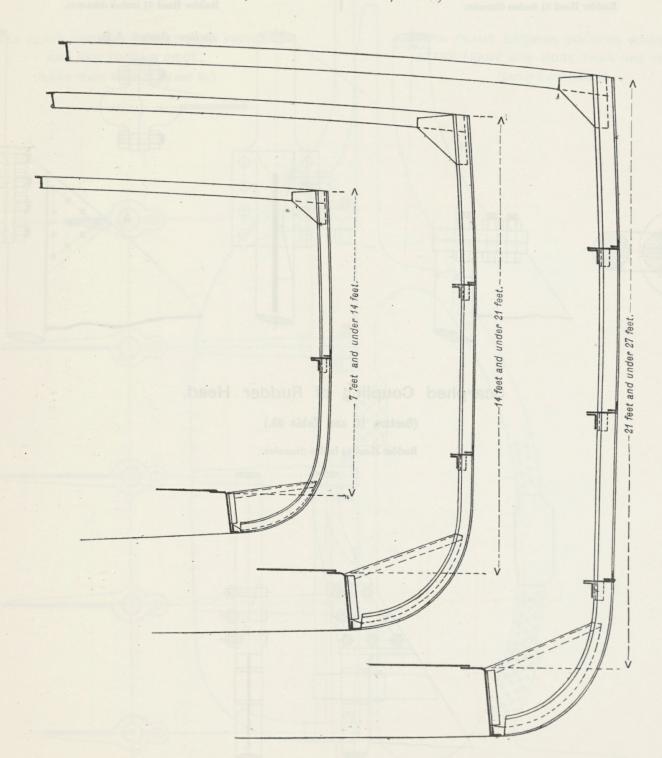
(Section 10 and Table 23.)

Rudder Head $9\frac{1}{2}$ inches diameter.



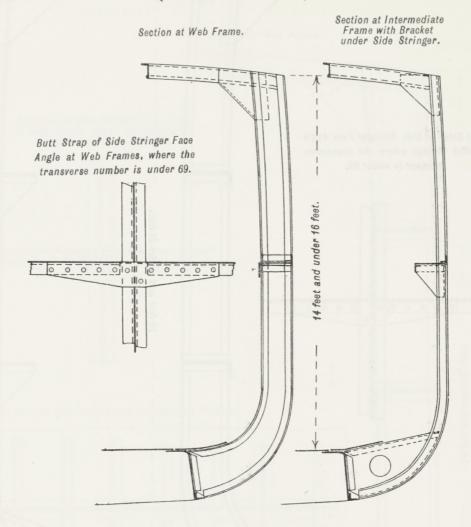
ARRANGEMENT OF SIDE STRINGERS.

(Section 15 and Tables 2, 3 & 7.)

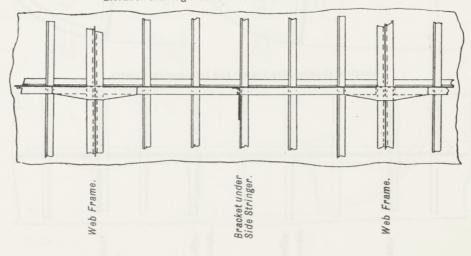


ARRANGEMENT OF WEB FRAMES AND SIDE STRINGERS.

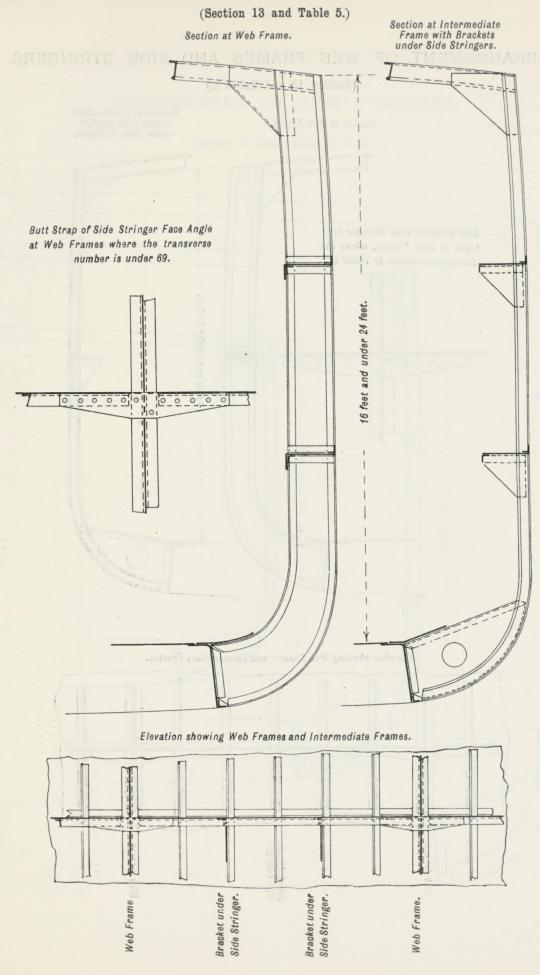
(Section 13 and Table 5.)



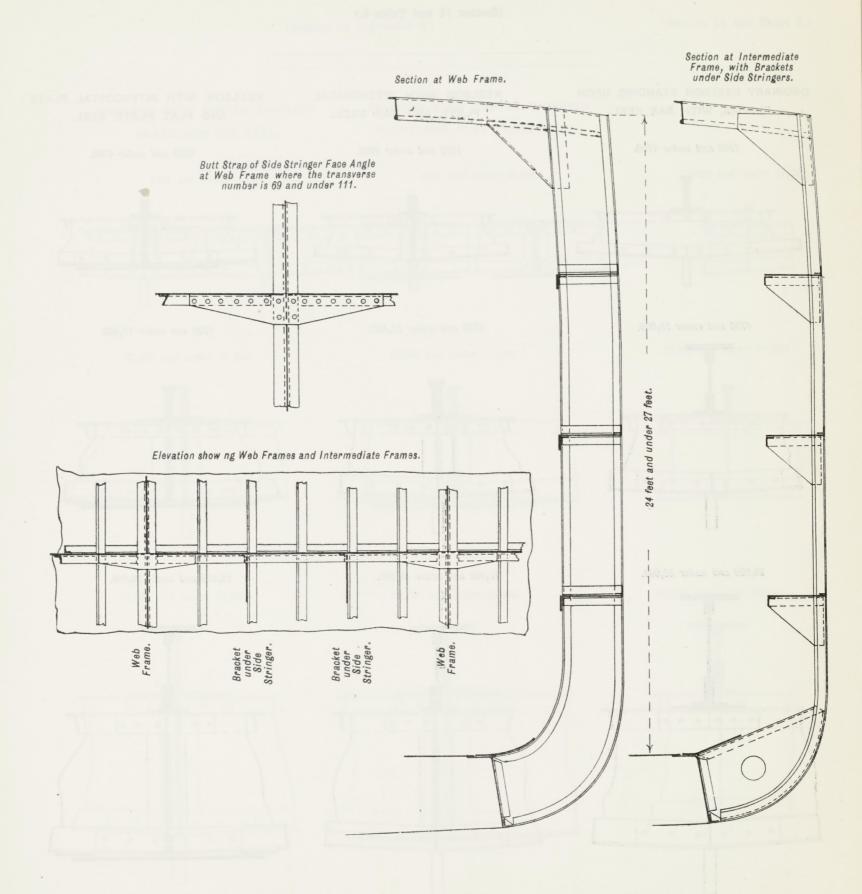
Elevation showing Web Frames and Intermediate Frames.



ARRANGEMENT OF WEB FRAMES AND SIDE STRINGERS.



(Section 13 and Table 5.)

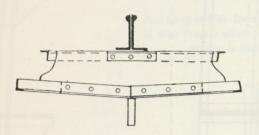


MIDDLE LINE KEELSONS.

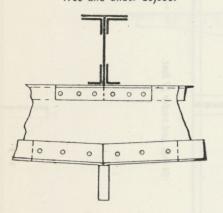
(Section 14 and Table 6.)

ORDINARY KEELSON STANDING UPON FLOORS, WITH BAR KEEL.

1200 and under 4700.



4700 and under 26,000.



26,000 and under 36,000.

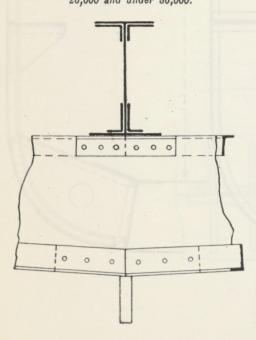
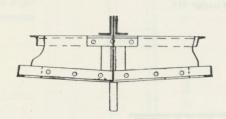
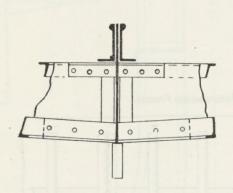


PLATE AND BAR KEEL.

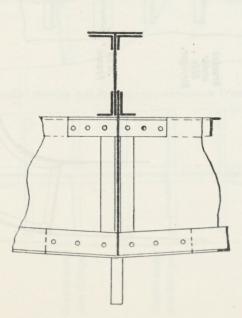
1200 and under 4700.



4700 and under 12,400.

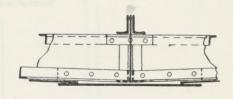


12,400 and under 36,000.

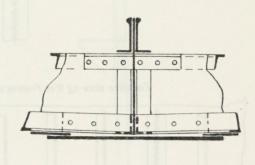


KEELSON WITH INTERCOSTAL PLATE AND FLAT PLATE KEEL.

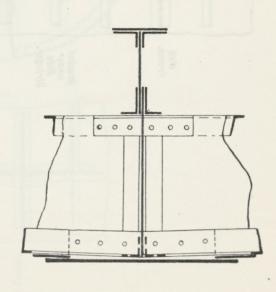
1200 and under 4700.



4700 and under 12,400.



12,400 and under 36,000.



MIDDLE LINE KEELSONS.

SIDE KEELSONS.

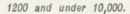
(Section 14 and Table 6.)

(Section 14 and Table 6.)

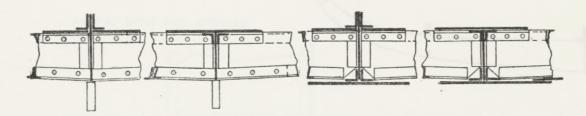
PLATE AND BAR KEEL.

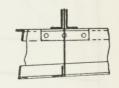
KEELSON WITH CENTRE THROUGH
PLATE AND FLAT PLATE KEEL.

1200 and under 10,000.



1200 and under 17,200.

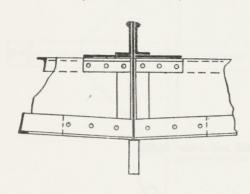


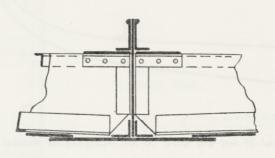


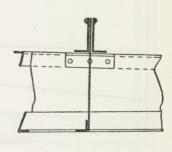
10,000 and under 17,200.

10,000 and under 17,200.

17,200 and under 21,000.



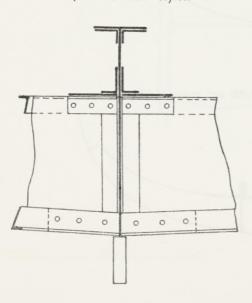


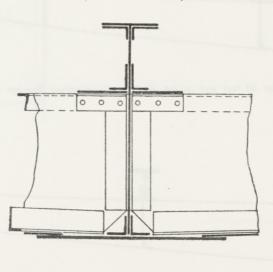


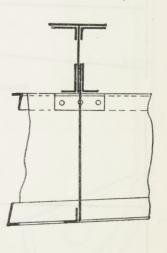
17,200 and under 36,000.

17,200 and under 36,000.

21,000 and under 36,000.



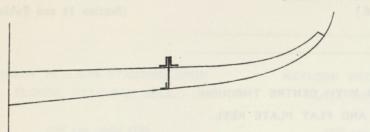




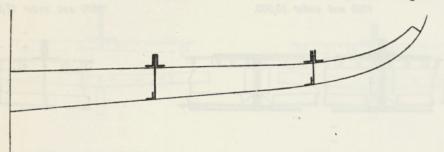
SIDE AND BILGE KEELSONS.

(Section 14 and Table 6.)

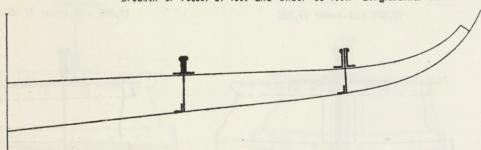
Breadth of Vessel under 27 feet.



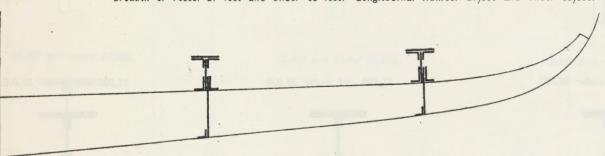
Breadth of Vessel 27 feet and under 50 feet.—Longitudinal Number under 17,200.



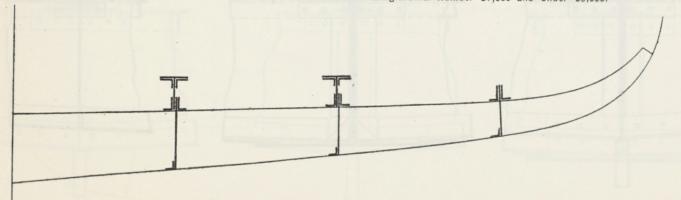
Breadth of Vessel 27 feet and under 50 feet.—Longitudinal Number 17,200 and under 21,000.



Breadth of Vessel 27 feet and under 50 feet.—Longitudinal Number 21,000 and under 36,000.



Breadth of Vessel 50 feet and under 54 feet.—Longitudinal Number 21,000 and under 36,000.

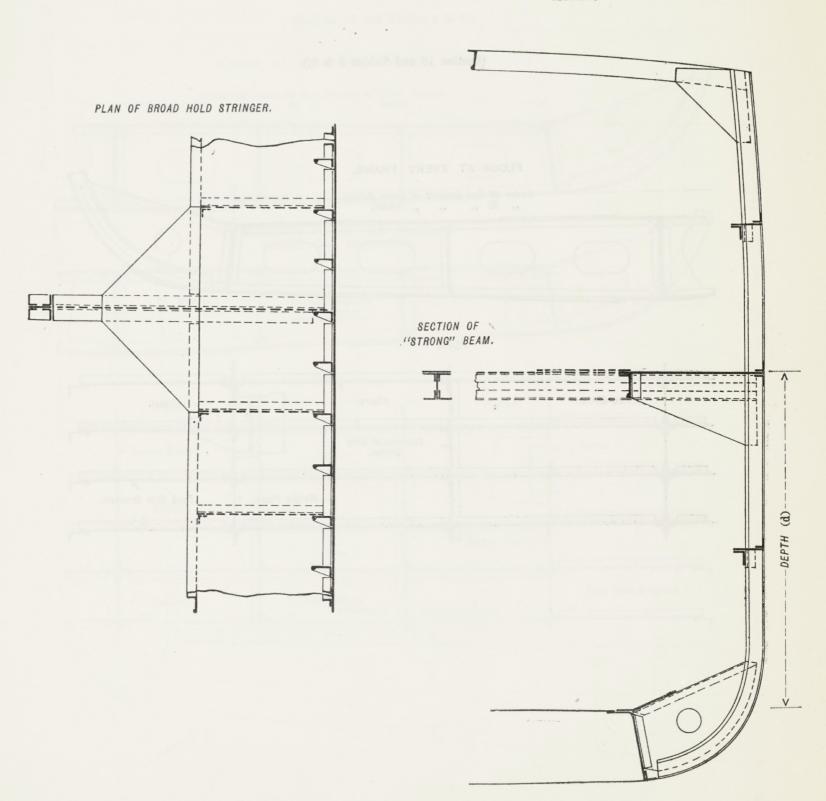


WIDELY SPACED BEAMS IN HOLD.

(Section 21 and Table 12.)

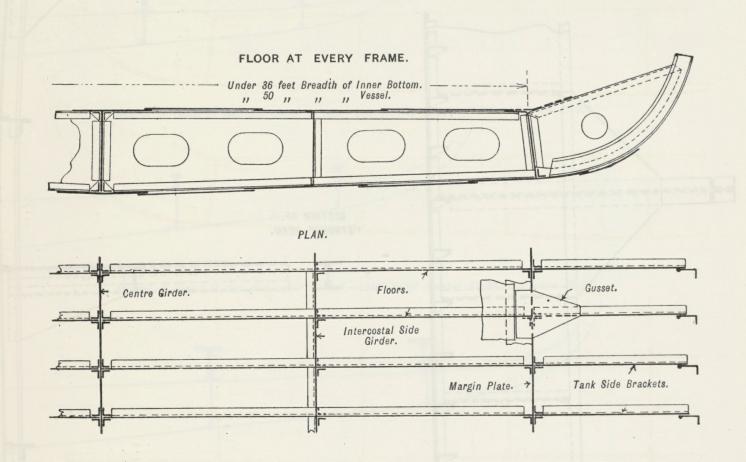
SKETCH SHOWING BROAD HOLD STRINGER, FACE BAR, BRACKETS SUPPORTING STRINGER, "STRONG" HOLD BEAMS AND GUSSET PLATE.

SECTION.



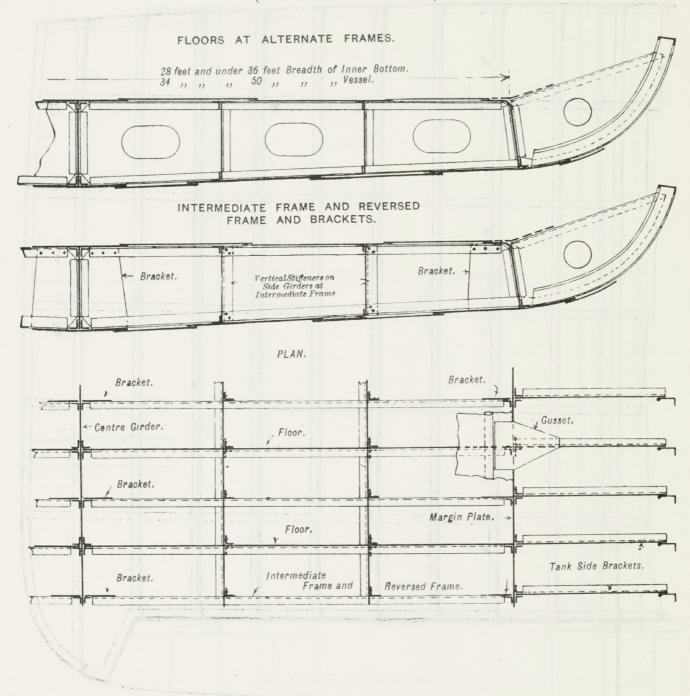
CELLULAR DOUBLE BOTTOMS.

(Section 16 and Tables 8 & 9.)



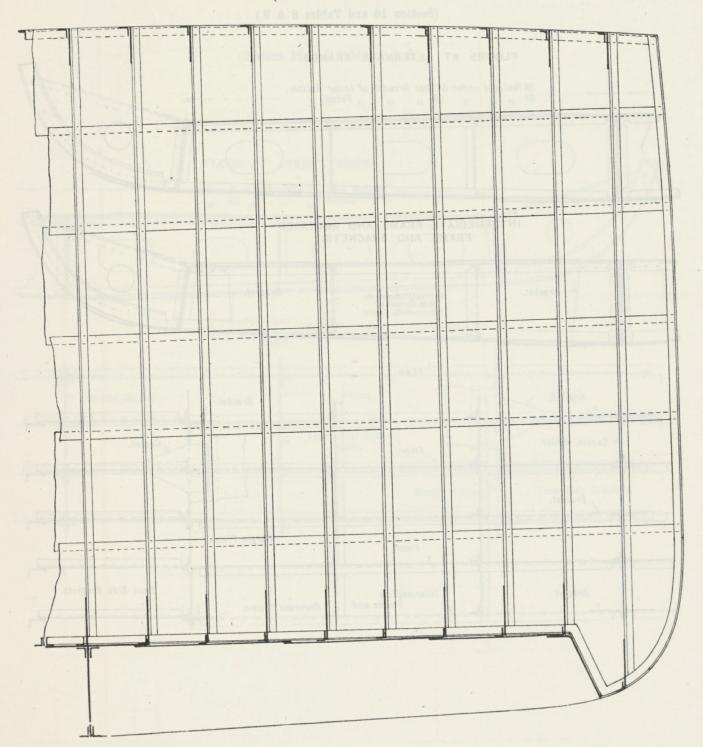
CELLULAR DOUBLE BOTTOMS.

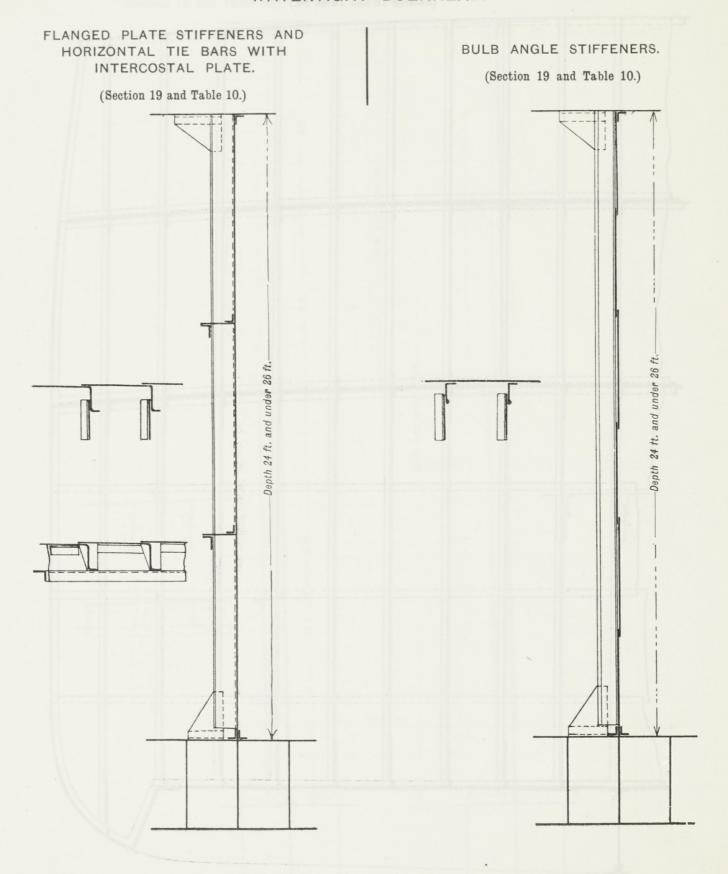
(Section 16 and Tables 8 & 9.)



ARRANGEMENT OF BULB ANGLE STIFFENERS SPACED 30 INCHES APART AND BRACKETED AT HEAD AND HEEL.

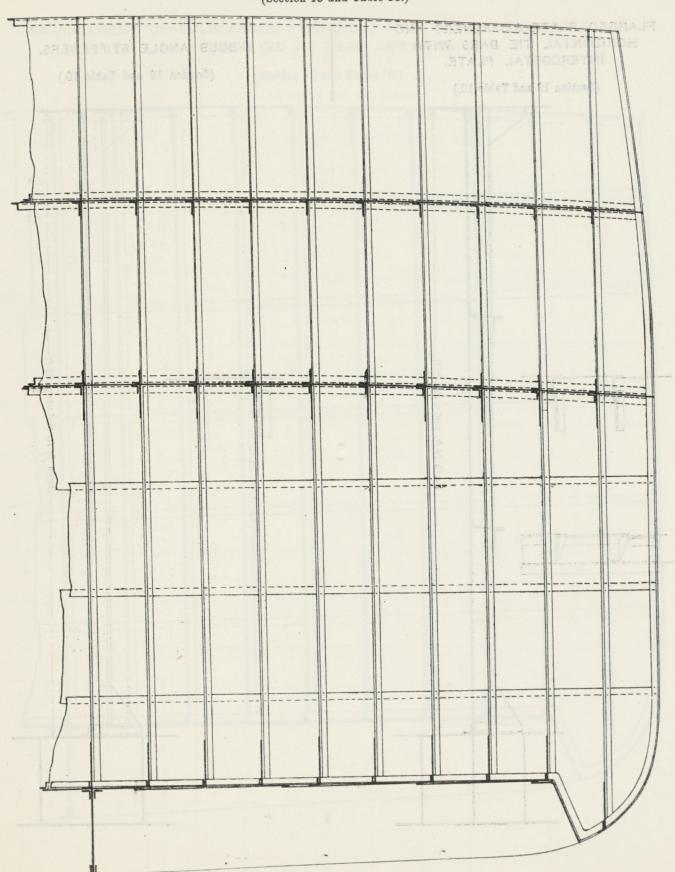
(Section 19 and Table 10.)





ARRANGEMENT OF VERTICAL STIFFENERS SPACED 30 INCHES APART IN HOLD AND 'TWEEN DECKS.

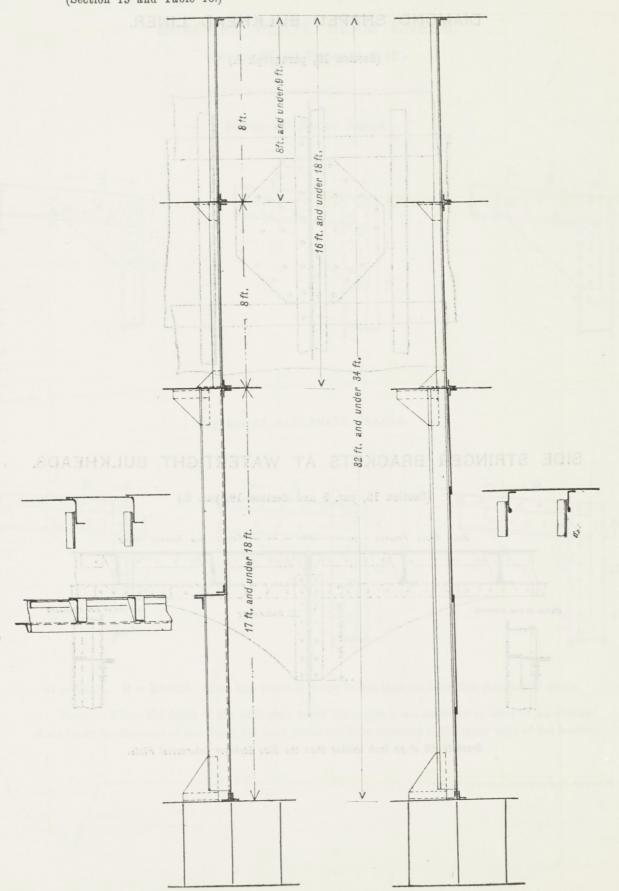
(Section 19 and Table 10.)



FLANGED PLATE STIFFENERS AND HORIZONTAL TIE BAR WITH INTERCOSTAL PLATE IN HOLD. (Section 19 and Table 10.)

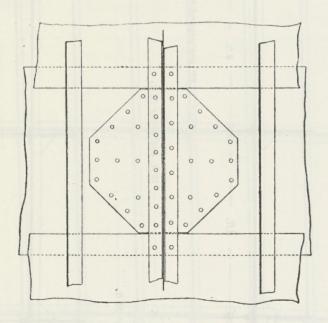
STIFFENERS IN HOLD AND 'TWEEN DECKS.

(Section 19 and Table 10.)



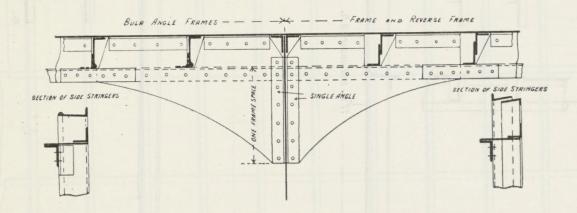
DIAMOND SHAPED BULKHEAD LINER.

(Section 19, paragraph 6.)



SIDE STRINGER BRACKETS AT WATERTIGHT BULKHEADS.

(Section 15, par. 3 and Section 19, par. 6.)

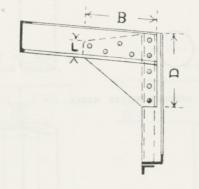


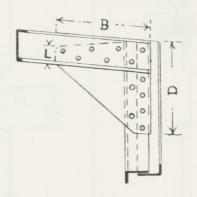
Brackets '06 of an inch thicker than the Side Stringer Intercostal Plate.

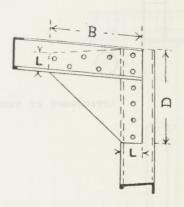
BRACKET PLATE BEAM KNEES.

(Section 20 and Tables 11 & 12.)

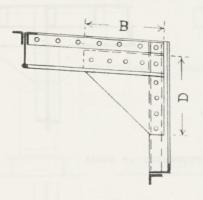
BEAMS AT EVERY FRAME.

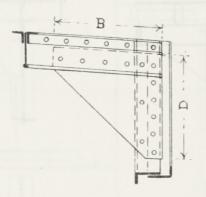


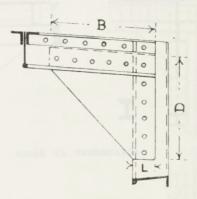




BEAMS AT ALTERNATE FRAMES.





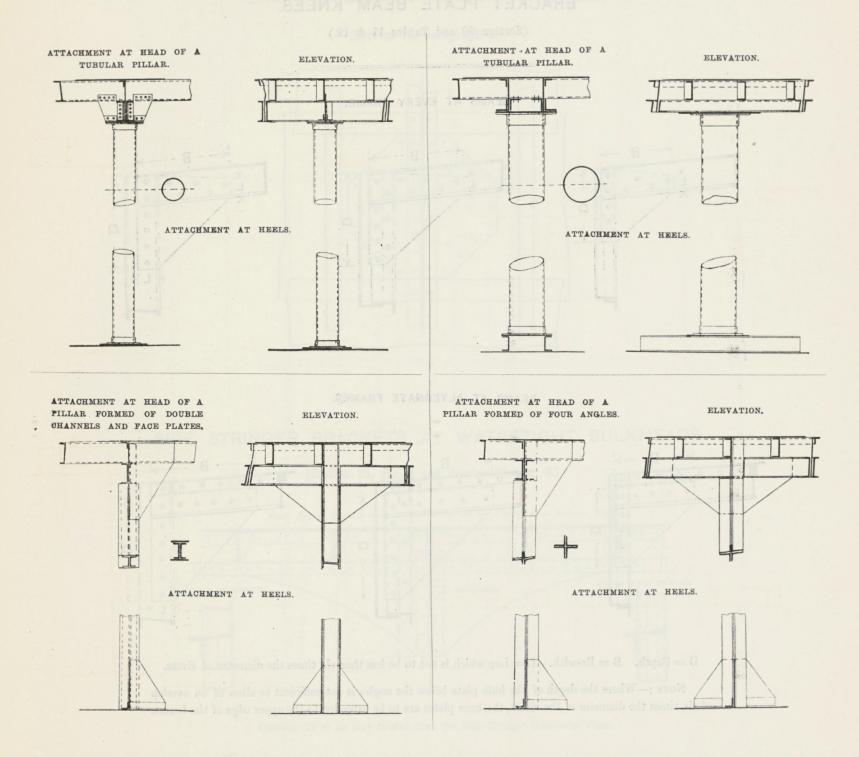


D = Depth. B = Breadth. L = Lap which is not to be less than six times the diameter of rivets.

Note:—Where the depth of the bulb plate below the angles is not sufficient to allow of an overlap of six times the diameter of the rivets, the knee plates are to be extended to the upper edge of the beams.

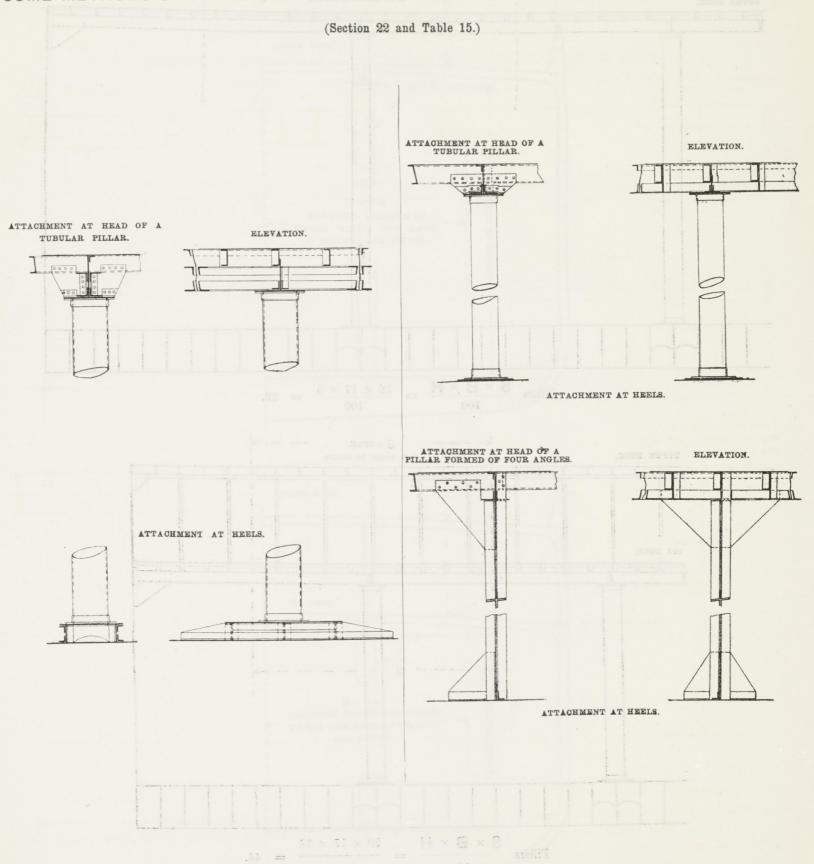
SOME METHODS OF ATTACHING THE WIDELY SPACED PILLARS AT HEADS AND HEELS.

(Section 22 and Table 15.)

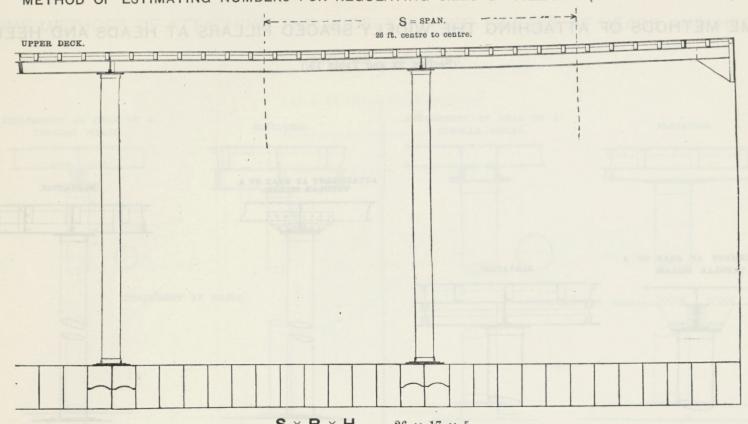


- 1. Pillars and girders of other form will be admitted provided the same are of equivalent strength to those given in Tables 15 and 16.
- Where no seating is fitted, widely spaced hold pillars are to be stepped when practicable at an intersection of floors and intercostals; but in cases wherein this cannot be done, intercostal brackets are to be fitted on each side of the floors beneath the pillars.
- 3. For Scantlings of widely spaced Pillars, and Girders at heads of same, see Tables 15 and 16.

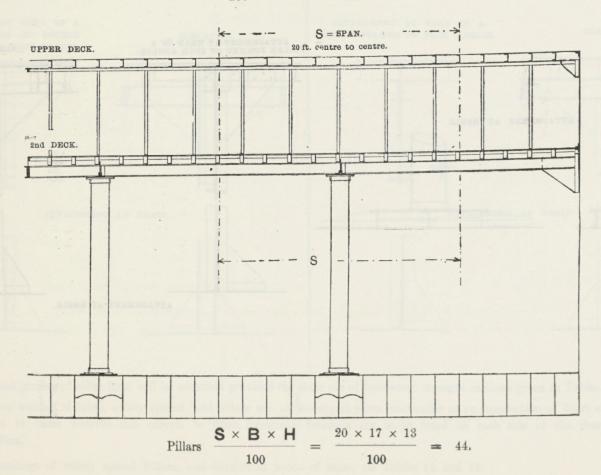
SOME METHODS OF ATTACHING THE WIDELY SPACED PILLARS AT HEADS AND HEELS.



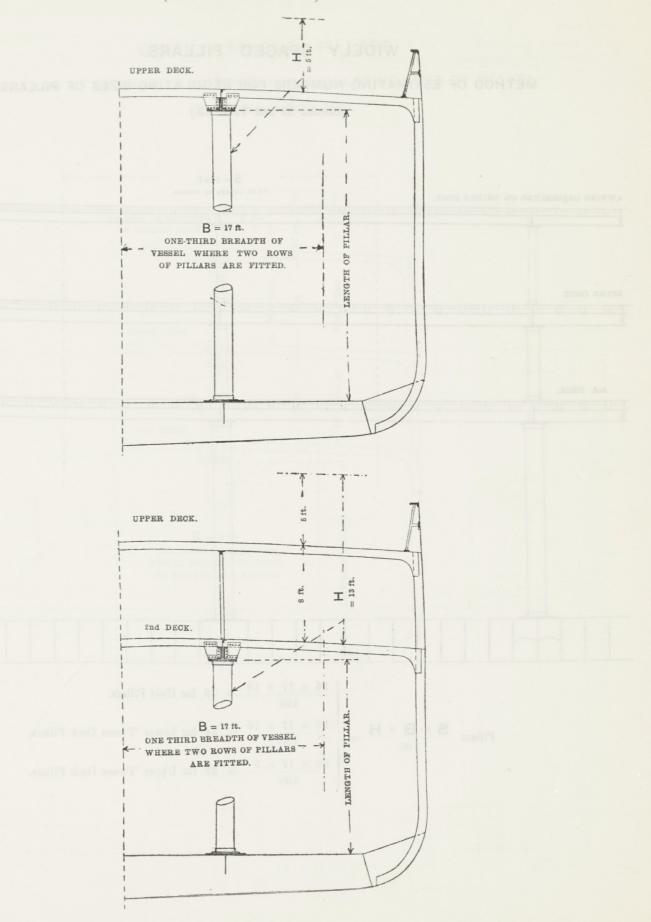
METHOD OF ESTIMATING NUMBERS FOR REGULATING SIZES OF PILLARS. (Section 22 and Table 15.)



Pillars
$$\frac{\mathsf{S} \times \mathsf{B} \times \mathsf{H}}{100} = \frac{26 \times 17 \times 5}{100} = 22.$$



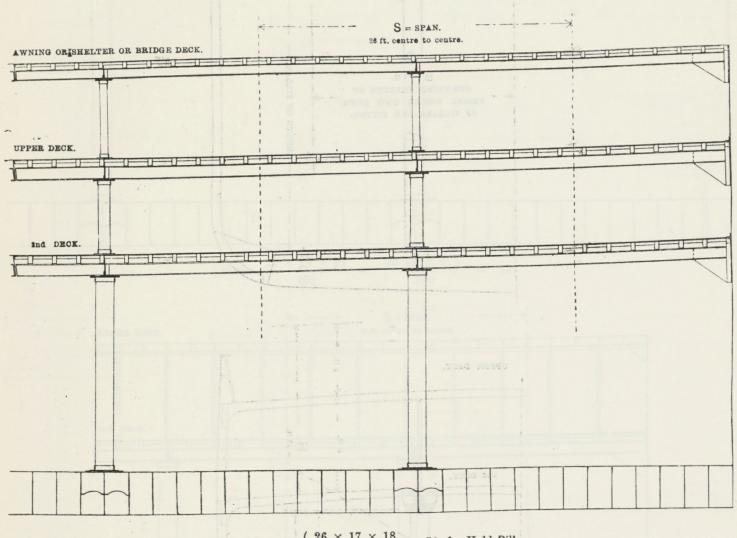
METHOD OF ESTIMATING NUMBERS FOR REGULATING SIZES OF PILLARS. (Section 22 and Table 15.)



WIDELY SPACED PILLARS.

METHOD OF ESTIMATING NUMBERS FOR REGULATING SIZES OF PILLARS.

(Section 22 and Table 15.)

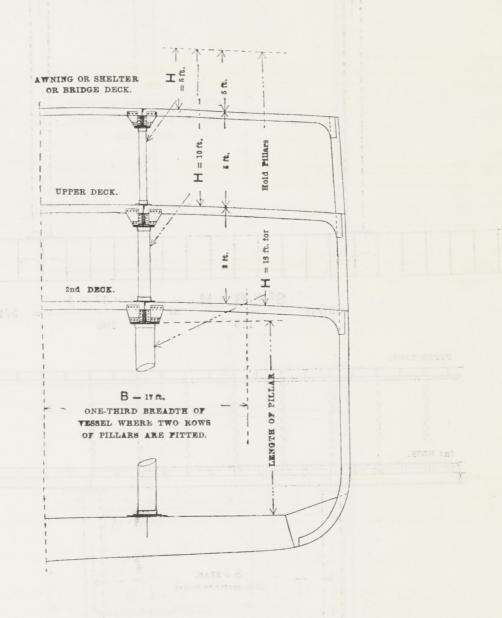


$$Pillars \quad \frac{\textbf{S} \times \textbf{B} \times \textbf{H}}{100} = \begin{cases} \frac{26 \times 17 \times 18}{100} = 79 \text{ for Hold Pillars.} \\ \frac{26 \times 17 \times 10}{100} = 44 \text{ for Lower 'Tween Deck Pillars.} \\ \frac{26 \times 17 \times 5}{100} = 22 \text{ for Upper 'Tween Deck Pillars.} \end{cases}$$

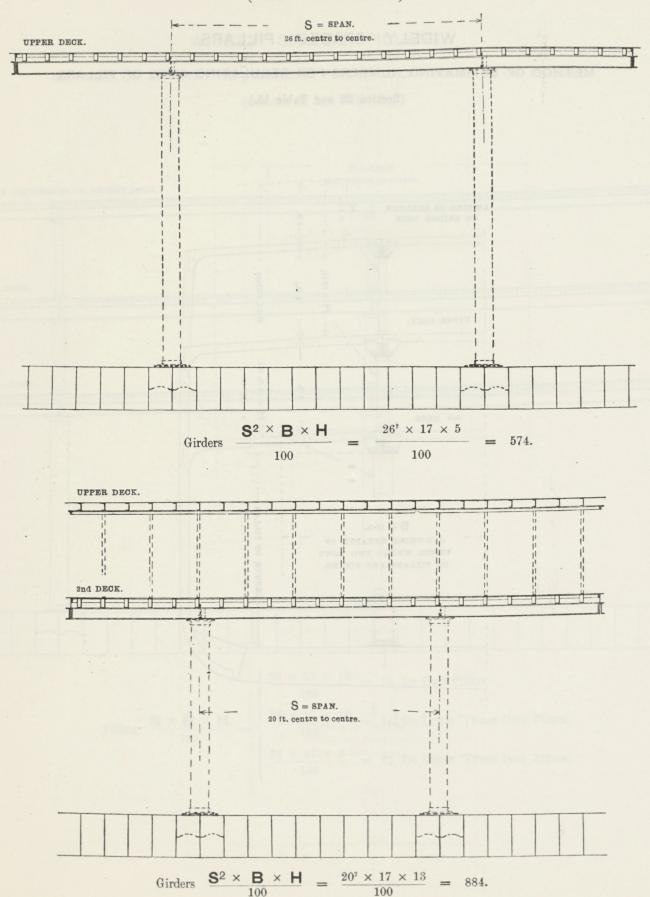
WIDELY SPACED PILLARS.

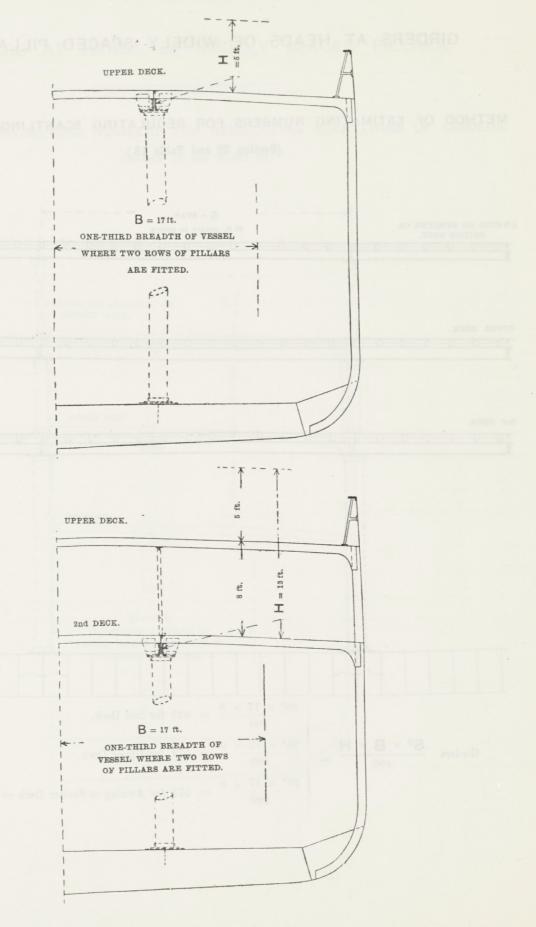
METHOD OF ESTIMATING NUMBERS FOR REGULATING SIZES OF PILLARS.

(Section 22 and Table 15.)



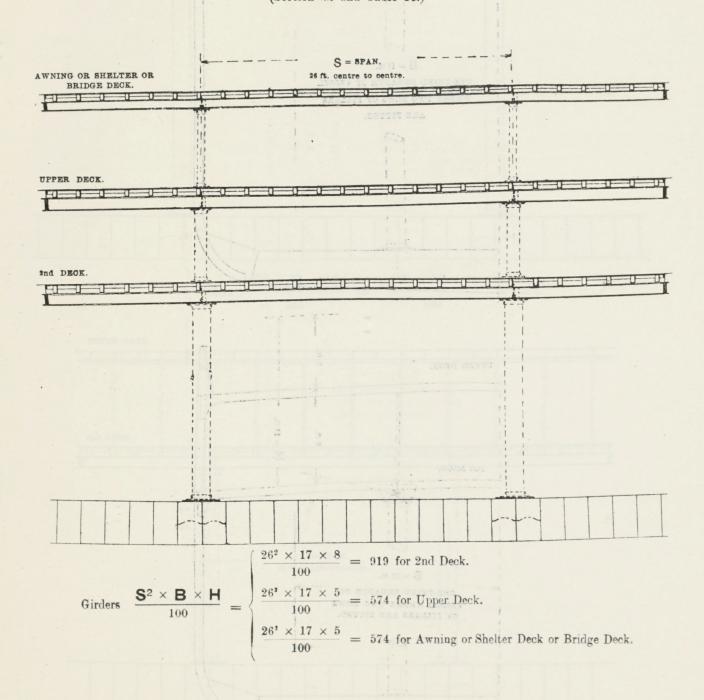
GIA. SP X B X H _ SO X 17 X 18 _ 884



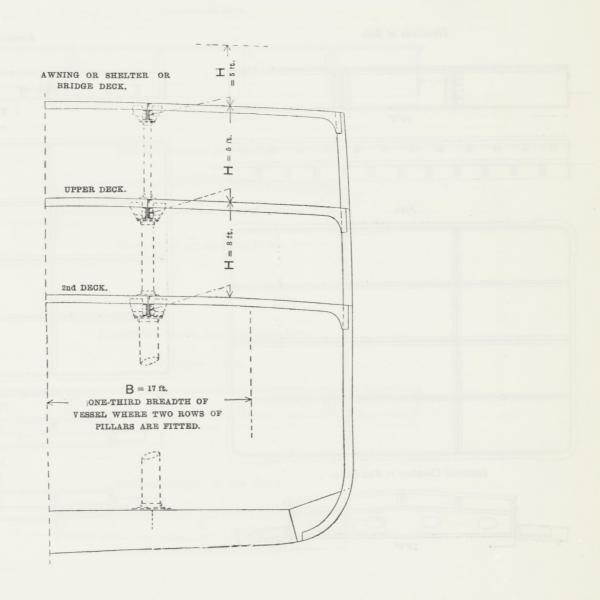


METHOD OF ESTIMATING NUMBERS FOR REGULATING SCANTILINGS OF GIRDERS.

GIRDERS AT HEADS OF WIDELY SPACED PILLARS.



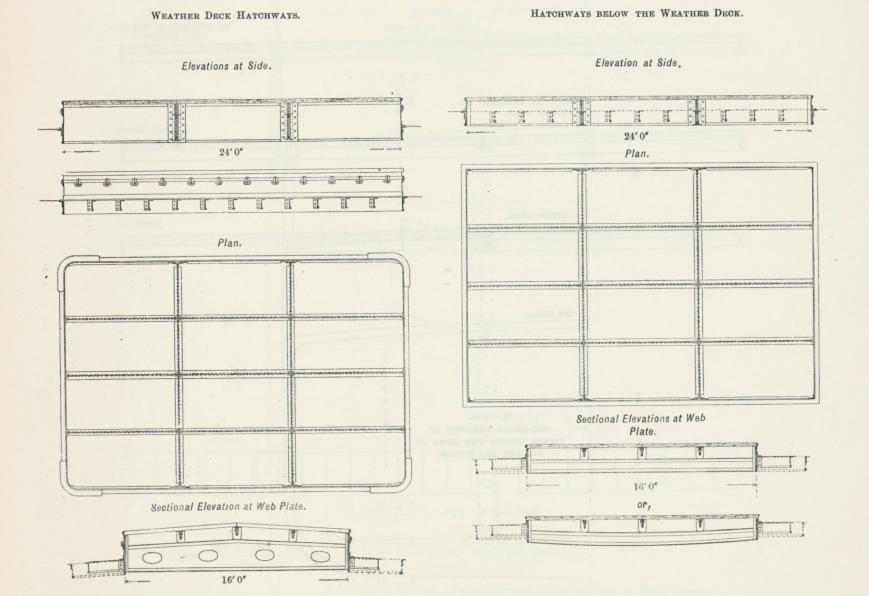
GIRDERS AT HEADS OF WIDELY SPACED PILLARS.



HATCHWAYS.

(Section 32.)

WEB PLATE BEAMS WITH FORE AND AFTERS.



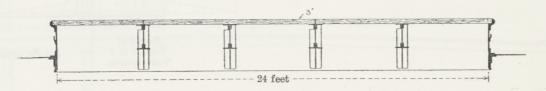
HATCHWAYS.

(Section 32.)

WEB PLATE BEAMS WITHOUT FORE AND AFTERS.

WEATHER DECK HATCHWAYS.

Elevation at Side.



Sectional Elevation at Web Plates.

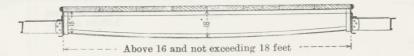


HATCHWAYS BELOW THE WEATHER DECK.

Elevation at Side.

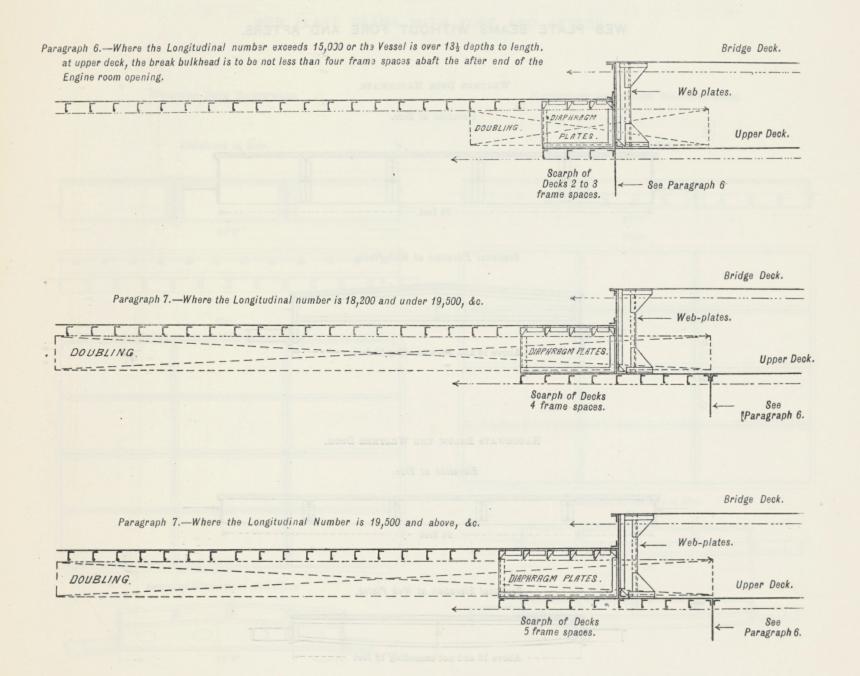


Sectional Elevation at Web Plates.



STRENGTHENING AT BREAK OF RAISED QUARTER DECK.

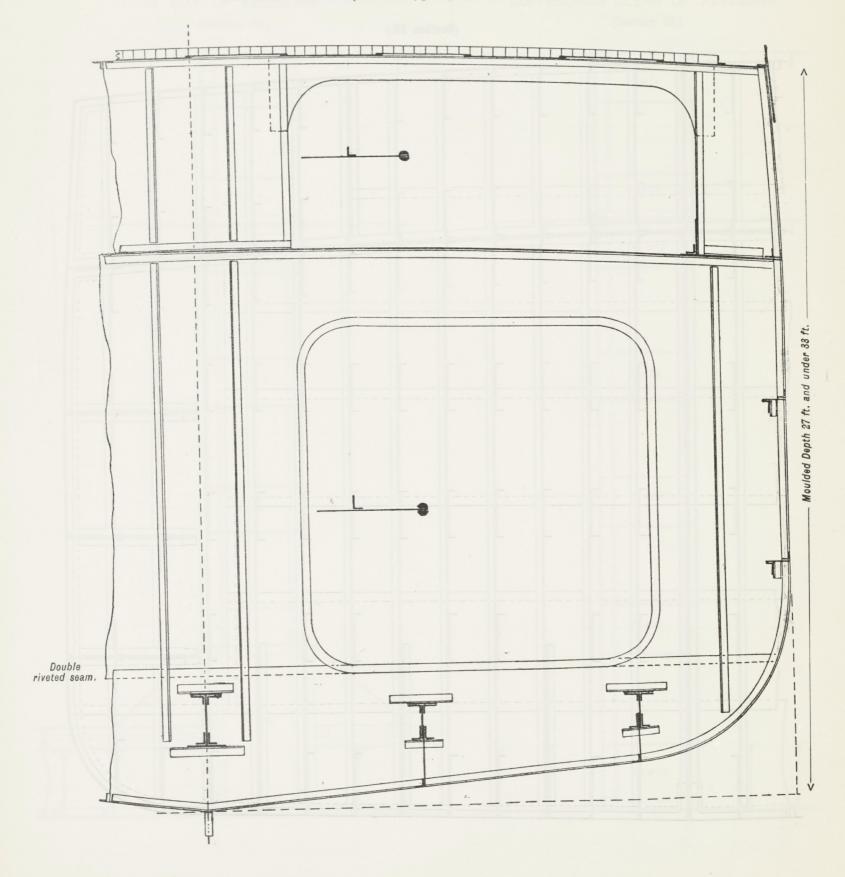
(Section 46, paragraphs 4, 5, 6 and 7.)



PARTIAL BULKHEAD IN SAILING VESSELS.

WHERE THE MOULDED DEPTH IS 27 FEET AND UNDER 33 FEET.

(Section 47, paragraph 4.)

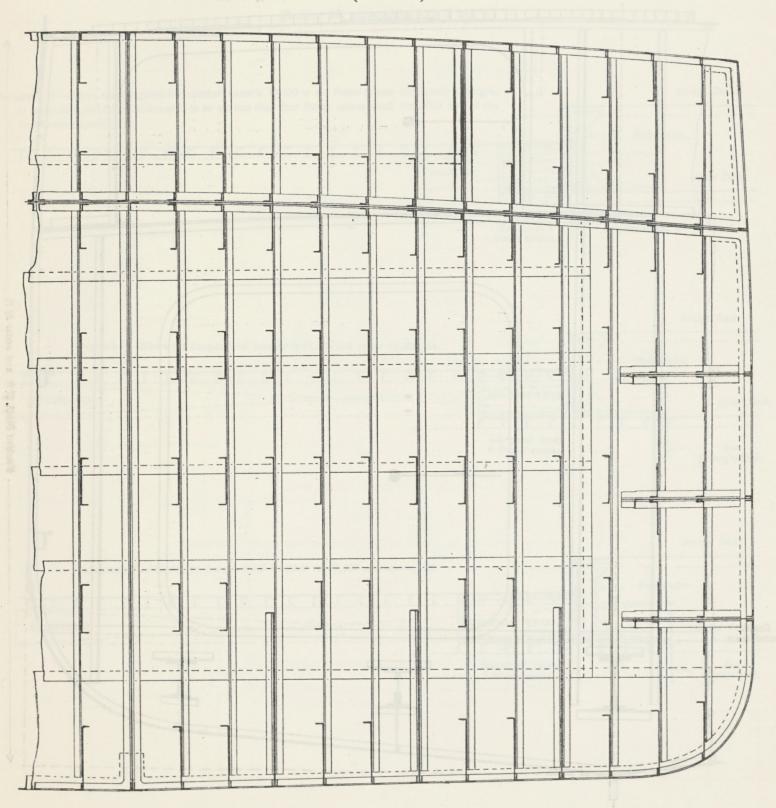


VESSELS INTENDED TO CARRY OIL IN BULK.

COFFERDAM BULKHEADS.

ARRANGEMENT OF STIFFENING INSIDE COFFERDAMS.

(Section 59.)

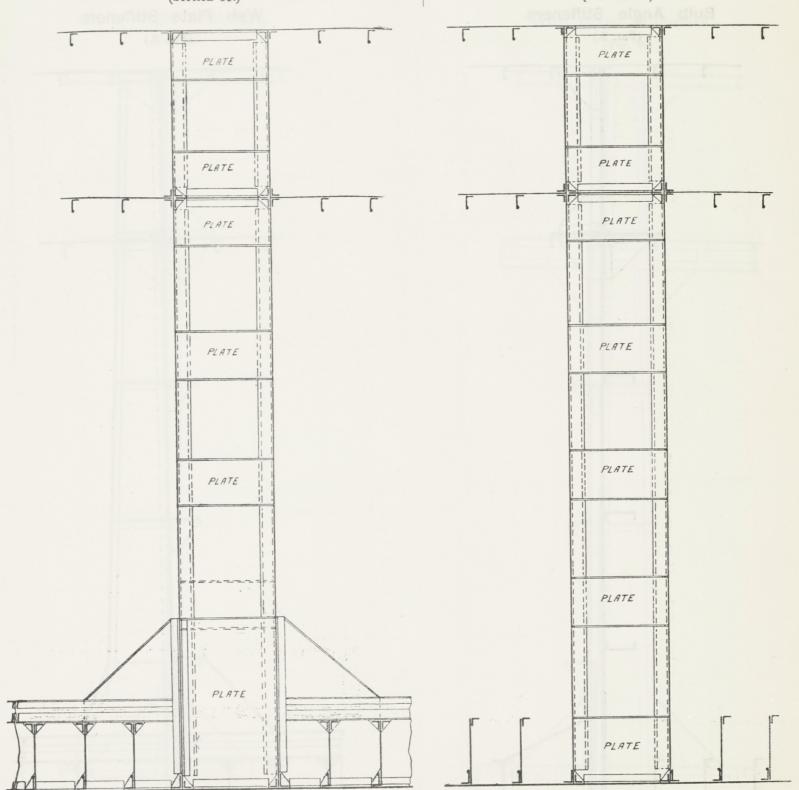


COFFERDAM BULKHEADS.

ARRANGEMENT OF STIFFENING INSIDE COFFERDAMS
IN WAY OF KEELSONS.

(Section 59.)

ARRANGEMENT OF STIFFENING INSIDE COFFERDAMS CLEAR OF KEELSONS.
(Section 59.)

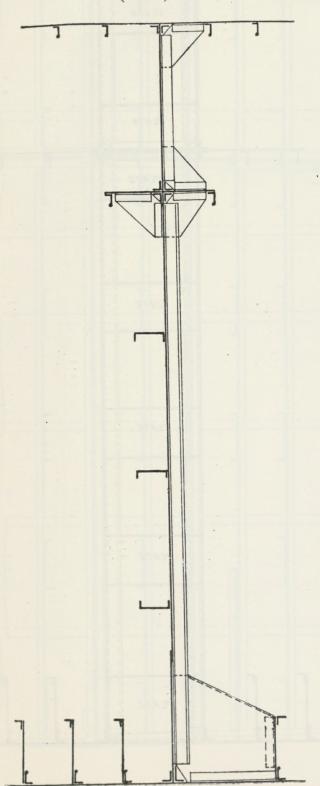


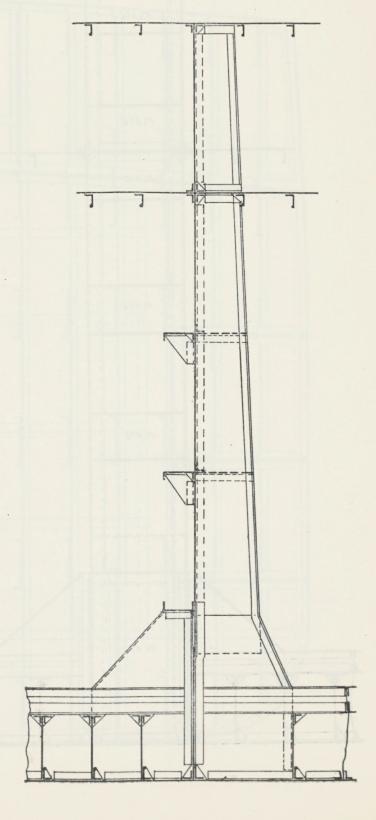
TRANSVERSE BULKHEAD.

(Section 58 and Table 35.)

Bulb Angle Stiffeners.
(Par. 5.)

Web Plate Stiffeners. (Par. 8.)

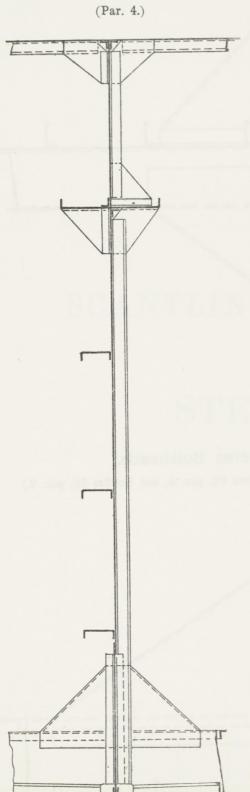




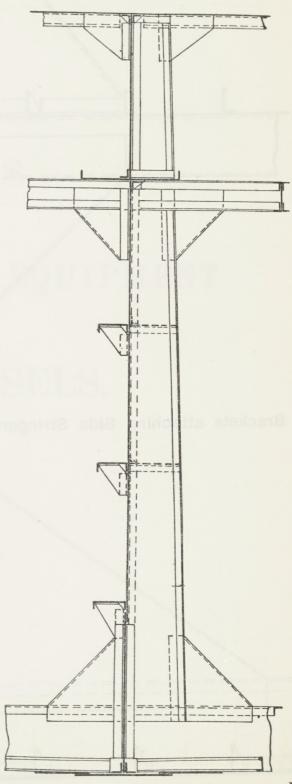
MIDDLE LINE BULKHEAD.

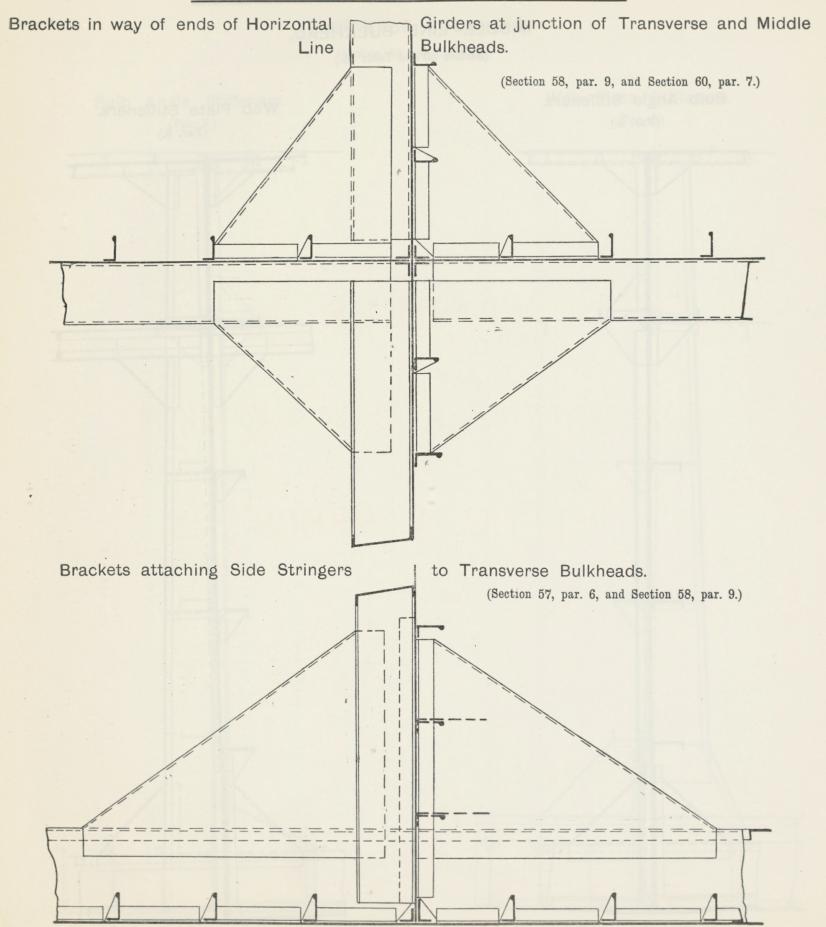
(Section 60 and Table 35.)

Bulb Angle Stiffeners.



Web Plate Stiffeners. (Par. 5.)





TABLES

OF

SCANTLINGS AND EQUIPMENT

FOR

STEEL VESSELS.

TABLES SCANTLINGS AND EQUIPMENT

LONGITUDINAL NUMBER. L × (B + D).	KEELS.	STEMS.	STERN- POSTS WITHOUT APER- TURES.	STERN : WI APERT	TH		LONGITUDINAL NUMBER. L × (B + D).	KEI	ELS.	STI	EMS.	PO: WIT:	ERN- STS HOUT ER- RES.	Pro		WIT	URES		
2100 and 2700	Inches. $6 \times 1 \pm$	Inches. $5\frac{1}{2} \times 1\frac{1}{2}$	Inches. $5\frac{1}{4} \times 1\frac{1}{4}$	Inches. $5\frac{1}{2} \times 2\frac{1}{2}$	Inches. 5×21	-	$16300_{\mathrm{under}}^{\mathrm{\ and\ }}17500$		thes. $ imes 2\frac{5}{9}$		thes. $ imes 2\frac{3}{8}$		thes. $ imes 2\frac{5}{8}$		nches.		$7\frac{1}{2}$	iches.	
2700 and 3350						-	$17500_{\mathrm{under}}^{\mathrm{and}}18900$		-				$\times 2\frac{5}{8}$			$\frac{5}{2}$	8		
3350 and 4000						-	18900 and 20500										30	×	_
4000 and 4650						-	20500 and 22300										81/2	×	6
4650 and 5300						D. Colonial Co.	$22300_{ m under}^{ m and} 24300$			_							$8\frac{1}{2}$	×	$6\frac{1}{2}$
5300 _{under} 5950	$7 \times 1\frac{5}{8}$	$6 \times 1\frac{5}{8}$	$6 \times 1\frac{5}{8}$	$6 \times 3\frac{1}{2}$	$\frac{1}{5\frac{3}{4} \times 3\frac{1}{2}}$	- ALEXANDER COLOR	$24300_{ m under}^{ m and} 26500$	11	$\times 2\frac{3}{4}$	10	$\times 2\frac{1}{2}$	10	$\times 2\frac{3}{4}$	10	×	$6\frac{1}{2}$	9	×	$6\frac{1}{2}$
$\overline{5950_{\mathrm{under}}^{\mathrm{and}}}$ 6600	$7\frac{1}{4} \times 1\frac{3}{4}$	$6\frac{1}{4} \times 1\frac{5}{8}$	$6\frac{1}{4} \times 1\frac{3}{4}$	$6\frac{1}{4} \times 3\frac{3}{4}$	$5\frac{3}{4} \times 3\frac{3}{4}$	ONE TAX DESCRIPTION OF TAX DESCR	$26500_{\rm under}^{\rm and} 28900$	11	$\times 2\frac{7}{8}$	10	$\times 2\frac{5}{8}$	10	$\times 2\frac{7}{8}$	10	×	7	9	×	7
6600 and 7250	$7\frac{1}{4} \times 1\frac{7}{8}$	$6\frac{1}{4} \times 1\frac{3}{4}$	$6\frac{1}{4} \times 1\frac{7}{8}$	$6\frac{1}{4} \times 4$	$5\frac{3}{4} \times 4$		$28900_{\mathrm{under}}^{\mathrm{and}}31500$	$11\frac{1}{2}$	$\times 2\frac{7}{8}$	10	$\times 2\frac{3}{4}$	10	$\times 3$	10	X	$7\frac{1}{2}$	9	×	$7\frac{1}{2}$
7250 and 7900	$7\frac{1}{4} imes 1\frac{7}{8}$	$6\frac{1}{4} \times 1\frac{3}{4}$	$6\frac{1}{4} \times 1\frac{7}{8}$	$6\frac{1}{4} \times 4\frac{1}{4}$	$5\frac{3}{4} \times 4\frac{1}{4}$		31500 and 34300	$11\frac{1}{2}$	$\times 3$	$10\frac{1}{2}$	$\times 2\frac{3}{4}$	$10\frac{1}{2}$	$\times 3$	$10\frac{1}{2}$	X	$7\frac{1}{2}$	9	×	$7\frac{1}{2}$
7900 and 8550	$7\frac{1}{4} \times 2$	$6\frac{1}{4} \times 1\frac{7}{8}$	$6\frac{1}{4} \times 2$	$6\frac{1}{4} \times 4\frac{1}{2}$	$5\frac{3}{4} \times 4\frac{1}{2}$		34300 and 37300	12	$\times 3$	$10\frac{1}{2}$	$\times 2\frac{3}{4}$	$10\frac{1}{2}$	$\times 3\frac{1}{8}$	101	X	8	9	×	8
8550 and 9200	$7\frac{1}{2} \times 2\frac{1}{8}$	$6\frac{1}{2} \times 1\frac{7}{8}$	$6\frac{1}{2} \times 2\frac{1}{8}$	$6\frac{1}{2} \times 4\frac{1}{2}$	$6 \times 4\frac{1}{2}$	ACT CHARLES OF THE CHARLES	$37300_{\mathrm{under}}^{\mathrm{and}}40500$	MANUAL MA		$10\frac{1}{2}$	$\times 2\frac{7}{8}$	$10\frac{1}{2}$	$\times 3\frac{1}{4}$	$10\frac{1}{2}$	X	$8\frac{1}{2}$	9	×	81/2
9200 and 9850	$7\frac{1}{2} \times 2\frac{1}{4}$	$6\frac{1}{2} \times 2$	$6\frac{1}{2} \times 2\frac{1}{4}$	$6\frac{1}{2} \times 4\frac{3}{4}$	$6 \times 4\frac{3}{4}$		$40500_{ m under}^{ m and} 43900$	CONTROL ADDRESS OF	8911	11	$\times 2\frac{7}{8}$	11	$\times 3\frac{1}{4}$	11	X	81/2	$9\frac{1}{2}$	X	81/2
9850 and 10500	$7\frac{3}{4} \times 2\frac{1}{4}$	$6\frac{3}{4} \times 2$	$6\frac{3}{4} \times 2\frac{1}{4}$	$6\frac{3}{4} \times 4\frac{3}{4}$	$6 \times 4^{\frac{3}{4}}$		$43900_{\mathrm{under}}^{\mathrm{and}}47500$			11	$\times 3$	11	$\times 3\frac{3}{8}$	11	×	9	$9\frac{1}{2}$	×	9
10500 and 11150	$7\frac{3}{4} \times 2\frac{3}{8}$	$6\frac{3}{4} \times 2\frac{1}{8}$	$\frac{1}{8}6\frac{3}{4} \times 2\frac{3}{8}$	$6\frac{3}{4} \times 5$	6 ×5		47500 and 51300	-		11	$\times 3\frac{1}{8}$	11	$\times 3\frac{1}{2}$	11	×	$9\frac{1}{2}$	$9\frac{1}{2}$	X	$9\frac{1}{2}$
11150 and 11800	$8 \times 2\frac{3}{8}$	7 ×2	$\frac{1}{8}7 \times 2\frac{3}{8}$	7 × 5	$6\frac{1}{4} \times 5$		51300_{under} 55300	-	<u>a</u> ve a	$11\frac{1}{2}$	$\times 3\frac{1}{8}$	$11\frac{1}{2}$	$\times 3\frac{1}{2}$	11	X	$9\frac{1}{2}$	10	×	$9\frac{1}{2}$
11800 and 12500	$8\frac{1}{4} \times 2\frac{3}{8}$	$7\frac{1}{4} \times 2$	$7\frac{1}{4} \times 2\frac{1}{8}$	$7\frac{1}{4} \times 5$	$6\frac{1}{2} \times 5$	AND	55300_{under} 59700	-		$11\frac{1}{2}$	$\times 3\frac{1}{8}$	$11\frac{1}{2}$	$\times 3\frac{5}{8}$	11	X	10	10	X	10
12500 and under 13300	$8\frac{1}{4} \times 2\frac{1}{2}$	$7\frac{1}{4} \times 2$	$7\frac{1}{4}7\frac{1}{4} \times 2\frac{1}{2}$	$7\frac{1}{4} \times 5\frac{1}{4}$	$6\frac{1}{2} \times 5\frac{1}{4}$	and the second	$59700_{ m under}^{ m and}64500$	CHARLES AND		$11\frac{1}{2}$	$\times 3\frac{1}{4}$	$11\frac{1}{2}$	$\times 3\frac{3}{4}$	12	×	10	$10\frac{1}{2}$	X	10
13300 and 14200	$8\frac{1}{2} \times 2\frac{1}{2}$	$7\frac{1}{2}$	$\frac{1}{4}7\frac{1}{2}\times2\frac{1}{2}$	$7\frac{1}{2}7\frac{1}{2} \times 5\frac{1}{4}$	$6\frac{3}{4} \times 5\frac{1}{4}$	and an owner of the latest designation of th	$64500_{ m under}^{ m and}69700$	The second second		12	$\times 3\frac{1}{4}$	12	$\times 3\frac{3}{4}$	12	×	$10\frac{1}{2}$	$10^{\frac{1}{2}}$	X	$10^{\frac{1}{2}}$
$14200_{\mathrm{under}}^{\mathrm{and}}15200$	$8\frac{1}{2} \times 2\frac{1}{2}$	$7\frac{1}{2} \times 2$	$\frac{3}{8}$ $7\frac{1}{2}$ \times $2\frac{1}{5}$	$7\frac{1}{2} \times 5\frac{1}{2}$	$\frac{1}{2}6\frac{3}{4} \times 5\frac{1}{2}$	-	$69700_{\rm under}^{\rm and}75300$	The state of the s		12	$\times 3\frac{3}{8}$	12	$\times 3\frac{7}{8}$	12	X	$10\frac{1}{2}$	11	X	$10^{\frac{1}{2}}$
15200 and under 16300	9 ×2	588 ×2	$\frac{3}{8}8 \times 2$	8×5	$\frac{1}{2}7 \times 5\frac{1}{2}$		75300 and s1000 under 81000	The state of the s		12	$\times 3\frac{1}{2}$	12	×4	12	X	11	11	X	11

The sectional area of the sole piece of stern frame is to be increased 15 per cent. beyond the sectional area of the propeller post.

The thickness of the sides of the boss of the propeller post is to be not less than three-fifths that required by the Table for the propeller post.

In high powered single screw vessels the dimensions of the stern frame will require to be increased to the satisfaction of the Committee.

TRANSVERSE	FRAME	AT HOT AT THE AT	FRAMING IN		(d) AT MIDDLE BOTTOMS, AND FR TO TOP OF LOWES	ROM TOP OF MAI		WAY OF DOUBLE	BOTTOMS,
NUMBER.	SPACING.		PEAKS.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
B + D				7 and under 8	8 and under 9	9 and under 10	10 and under 11	11 and under 12	12 and under 13
mbet.		-0 140 0 10	- 0 0 10 NO.	<			STRINGER. —		>
Feet.	inches.		inches.	inches.	inches.	inches.	inches.	inches.	inches.
23 and 25	20	Frames Reversed frames			$ \begin{array}{c cccc} 2 & 2\frac{1}{2} \times 2\frac{1}{2} \times \cdot 22 \\ 2 & 2\frac{1}{4} \times 2\frac{1}{4} \times \cdot 22 \\ & & 2\frac{1}{4} \times 2\frac{1}{4} \times \cdot 22 \end{array} $			0 1 × 18 0 28	9700,25
25 and 27	20	Frames Reversed frames Depth of framing			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				AP 0000
27 and 29	$20\frac{1}{2}$	Frames Reversed frames Depth of framing.	4 .4	44 44	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			-	
29 and 31	$20\frac{1}{2}$	Frames			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				
31 and 33	21	Frames			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
33 and 35	21	Frames Reversed frames Depth of framing	4		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			-	
35 and 37	$21\frac{1}{2}$	Frames			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
37 and 39	$21\frac{1}{2}$	Frames Reversed frames Depth of framing			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
39 and 42	22				$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
42 and 45	22				$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
.45 and 48	$22\frac{1}{2}$	Frames Reversed frames Depth of framing			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-			_
48 and 51	$22\frac{1}{2}$	Frames Reversed frames Depth of framing			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
51 and 54	23	Reversed frames Depth of framing	$\begin{array}{ccc} 3 & \times 3 & \times \cdot 30 \\ & & 3\frac{1}{2} \end{array}$	$3 \times 3 \times \cdot 3$ $3\frac{1}{2}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$3\frac{1}{2} \times 3 \times \cdot 30$ $4\frac{1}{2}$	$3\frac{1}{2} \times 3 \times \cdot 32$ $4\frac{1}{2}$	4 × 3 × ·32 5	4 × 3 × · 34 5
54 and 57	23				$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
57 and 60	$23\frac{1}{2}$	Frames Reversed frames Depth of framing	_	-	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			_	_

NUMBER.	FRAME SPACING.		Feet.	Feet.		See SKETCH	ON PAGE 21.	FOOT LOWEST	
B + D			13 and under 14	14 and under 15		Feet.	Feet. 17 and under 18	Feet.	Feet.
			10 under 14	14 under 19	10 under 10	10 under 17	17 under 18	18 and under 19	19 and under 20
			ONE SIDE STRINGER.	<		TWO SIDE	STRINGERS.—		
Feet.	inches.		inches.	inches.	inches.	inches.	inches.	inches.	inches.
23 and 25 under	20	Reversed frames Depth of framing						Manual Age	10 has 20
25 and 27	20	Frames Reversed frames Depth of framing						Second Of	150 150 30
27 and 29	$20\frac{1}{2}$	Frames Reversed frames Depth of framing						amoral (of	de lin te
29 and 31	$20\frac{1}{2}$		$ \begin{array}{ c c c c c } \hline 3\frac{1}{2} \times 3 & \times \cdot 28 \\ 2\frac{1}{2} \times 2\frac{1}{2} \times \cdot 28 \\ & & & & & \\ 3\frac{1}{2} \end{array} $					Secretary (OC)	10 48 18
31 and 33	21		$2\frac{1}{2} \times 2\frac{1}{2} \times \cdot 30$	$3\frac{1}{2} \times 3 \times \cdot 30$ $3 \times 2\frac{1}{2} \times \cdot 30$ $3\frac{1}{2}$				ASSESSED TO SESSED TO SESS	
33 and 35 under 35	2.1				$\begin{array}{cccccccccccccccccccccccccccccccccccc$			1000	
35 and 37	$21\frac{1}{2}$				$\begin{array}{cccc} 4 & \times 3 & \times \cdot 30 \\ 3\frac{1}{2} \times 3 & \times \cdot 30 \\ & & 4\frac{1}{2} \end{array}$				100
37 and 39	$21\frac{1}{2}$		$3 \times 3 \times \cdot 30$		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				to the te
39 and 42	22				$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
42 and 45	22							$4\frac{1}{2} \times 3 \times 36$ $4\frac{1}{2} \times 3 \times 36$ 6	
$45_{ m under}^{ m and}$ 48	$22\frac{1}{2}$							$\begin{array}{ccc} 4\frac{1}{2} \times 3 & \times \cdot 38 \\ 4\frac{1}{2} \times 3 & \times \cdot 38 \\ 6 \end{array}$	
48 and 51	$22\frac{1}{2}$							$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
51 and 54	23							$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
54 and 57	23			$4\frac{1}{2} \times 3 \times \cdot 36$		AM .		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
57 and 60	$23\frac{1}{2}$		$4\frac{1}{2} \times 3 \times \cdot 36$	$\begin{array}{ccc} 4\frac{1}{2} \times 3 & \times \cdot 38 \\ 4\frac{1}{2} \times 3 & \times \cdot 38 \end{array}$		$4\frac{1}{2} \times 3 \times \cdot 40$	$5 \times 3 \times \cdot 40$	5 × 3 × · 42 5 × 3 × · 42	

TRANSVERSE	FRAME				GIN PLATE IN		BOTTOMS, TO T	WAY OF SINGLE	
NUMBER.	SPACING.		Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
B + D	81 .		20 and under 21	21 and under 22	22 and under 23	23 and under 24	24 and under 25	25 and under 26	26 and under 27
			TWO SIDE STRINGERS.	<			STRINGERS. — —		
Feet.	inches		inches.	inches.	inches.	inches.	inches.	inches.	inches.
23 and 25 under	20	Frames Reversed frames Depth of framing							de 255,82
25 and 27	20	Frames							
27 and 29	$20\frac{1}{2}$	Frames Reversed frames Depth of framing							PE IGES, TE
29 and 31	$20\frac{1}{2}$	Frames Reversed frames Depth of framing							
31 and 33	21	Frames Reversed frames Depth of framing				8 x 24 000 x (2 x 24 000 x			te Little is
33 and 35	21	Frames Reversed frames Depth of framing		10000					
85 and 37	$21\frac{1}{2}$	Frames Reversed frames Depth of framing							
37 and 39	$21\frac{1}{2}$	Frames							
39 and 42	22	Frames Reversed frames Depth of framing						Description (SE)	21.27.0
42 and 45	22	Frames Reversed frames Depth of framing					12 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		43,75,9
45 and 48	$22\frac{1}{2}$		$ \begin{array}{cccc} 4\frac{1}{2} \times 3 & \times \cdot 40 \\ 5 & \times 3 & \times \cdot 40 \\ 6\frac{1}{2} \end{array} $			3 A B B B B B B B B B B B B B B B B B B	Bakil A complete		
48 and 51	$22\frac{1}{2}$			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$					ma_SE_as
$51_{ m under}^{ m and}$ 54	23			$5 \times 3 \times \cdot 42$ $5\frac{1}{2} \times 3 \times \cdot 42$ $7\frac{1}{2}$				ACCEPTED TO THE PERSON OF THE	*0.55.00
$54_{ m under}^{ m and}$ 57	23	Reversed frames Depth of framing	$5\frac{1}{2} \times 3 \times \cdot 42$ $7\frac{1}{2}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$5\frac{1}{2} \times 3 \times \cdot 46$	$\begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 46 \\ 8\frac{1}{2} \end{array}$			100,55,40
57 and 60	$23\frac{1}{2}$			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					

TRANSVERSE	FRAME		FRAMING IN	SINGLE B	OTTOMS, AND FR	OM TOP OF MAR	GIN PLATE IN	S AT CENTRE IN WAY OF DOUBLE & SKETCH ON PAGE	BOTTOMS,
NUMBER.	SPACING.+		PEAKS.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
B + D				7 and under 8	8 and under 9	9 and under 10	10 and under 11	11 and under 12	12 and under 13
				<		ONE SIDE	STRINGER.——		
Feet.	inches.	The second second	inches.	inches.	inches.	inches.	inches.	inches.	inches.
		Frames	$4\frac{1}{2} \times 3 \times \cdot 32$	$4\frac{1}{2} \times 3 \times \cdot 32$	$4\frac{1}{2} \times 3 \times \cdot 32$	$4\frac{1}{2} \times 3 \times \cdot 34$	$4\frac{1}{2} \times 3 \times \cdot 34$	$4\frac{1}{2} \times 3 \times \cdot 36$	$4\frac{1}{2} \times 3 \times \cdot 3$
60 and 63	$23\frac{1}{2}$		$3 \times 3 \times \cdot 32$	$3 \times 3 \times \cdot 32$	-	$3\frac{1}{2} \times 3 \times \cdot 34$	$4 \times 3 \times \cdot 34$	$4 \times 3 \times 36$	$4\frac{1}{2} \times 3 \times \cdot 3$
		Depth of framing	4½	$\frac{4\frac{1}{2}}{2}$	5	5	$\frac{5\frac{1}{2}}{2}$	$5\frac{1}{2}$	6
63 and 66	24							$5 \times 3 \times 36$ $4 \times 3 \times 36$	
obunder oo	21	Depth of framing.	5	5	5	$5\frac{1}{2}$	$5\frac{1}{2}$	6	6
		Frames			$5 \times 3 \times \cdot 34$	5 × 3 × · 36	5 × 3 × ·36	$5 \times 3\frac{1}{2} \times \cdot 38$	$5 \times 3\frac{1}{2} \times \cdot 3$
$66_{\mathrm{under}}^{\mathrm{and}}$ 69	24							$4 \times 3\frac{1}{2} \times \cdot 38$	
		Depth of framing	5	5	$5\frac{1}{2}$	$5\frac{1}{2}$	6	6	$6\frac{1}{2}$
and	,							$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 38$	
69 and 72	$24\frac{1}{2}$		1	3% 7	$3 \times 3\frac{1}{2} \times \cdot 36$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 36$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 38$	$4 \times 3\frac{1}{2} \times \cdot 38$	$4 \times 3\frac{1}{2} \times \cdot 40$
		Depth of framing	$\frac{5\frac{1}{2}}{5\frac{1}{2}}$	$5\frac{1}{2}$	$5\frac{1}{2}$	6	6	$6\frac{1}{2}$	$6\frac{1}{2}$
72 and 75	$24\frac{1}{2}$		$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 34$ $3 \times 3\frac{1}{2} \times \cdot 34$					$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$ $4 \times 3\frac{1}{2} \times \cdot 40$	
Lunder 19	242	Depth of framing.	5 1 3 4		$\frac{5\overline{2}}{6}$	$\frac{55}{6}$ \times $\frac{55}{6}$ \times .50	$6\frac{1}{2} \times 6\frac{1}{2} \times 60$	$6\frac{1}{6}$	7
Part of the		Frames	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 36}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 36}$		$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 38$	$\frac{5\frac{1}{3} \times 3\frac{1}{2} \times \cdot 38}{5\frac{1}{3} \times \frac{3}{3} \times \cdot 38}$	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40}$	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40}$	$5\frac{1}{3} \times 3\frac{1}{3} \times \cdot 4$
75 and 78	25		$3 \times 3\frac{1}{2} \times \cdot 36$					$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	
		Depth of framing	$5\frac{1}{2}$ **		6	$6\frac{1}{2}$	$6\frac{1}{2}$	7	7
and.	,		$6 \times 3\frac{1}{2} \times \cdot 36$					$6 \times 3\frac{1}{2} \times \cdot 42$	
78 and 81	$25\frac{1}{2}$		$3 \times 3\frac{1}{2} \times \cdot 36$		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 38$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$4 \times 3\frac{1}{2} \times \cdot 40$	$4 \times 3\frac{1}{2} \times \cdot 42$	$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 4$
		Depth of framing	6 ~		$\frac{6\frac{1}{2}}{2}$	$6\frac{1}{2}$	7	7	$\frac{7\frac{1}{2}}{2}$
81 and 84	26		$6 \times 3\frac{1}{2} \times \cdot 38$ $3 \times 3\frac{1}{2} \times \cdot 38$					$6 \times 3\frac{1}{2} \times \cdot 42$ $4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	
orunder or	20	Depth of framing.	6		61	7	7	$7\frac{1}{2}$	$7\frac{1}{2}$
		Frames	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 38$		$\frac{6\frac{1}{2} \times 3\frac{1}{3} \times \cdot 40}{6\frac{1}{2} \times 3\frac{1}{3} \times \cdot 40}$	$\frac{6\frac{1}{5} \times 3\frac{1}{5} \times \cdot 42}{6\frac{1}{5} \times 3\frac{1}{5} \times \cdot 42}$	$\frac{6\frac{1}{3} \times 3\frac{1}{3} \times \cdot 42}{6\frac{1}{3} \times 3\frac{1}{3} \times \cdot 42}$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 4$
84 and 87	$26\frac{1}{2}$		$3 \times 3\frac{1}{2} \times \cdot 38$					$4 \times 3\frac{1}{2} \times \cdot 44$	
		Depth of framing	$6\frac{1}{2}$ **		7	7	$7\frac{1}{2}$	$7\frac{1}{2}$	8
o= and oo	0=		$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$					$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	
87 and 90	27	Reversed frames Depth of framing	$3 \times 3\frac{1}{2} \times \cdot 40$		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$\begin{array}{c} 4 \times 3\frac{1}{2} \times \cdot 42 \\ 71 \end{array}$	$4 \times 3\frac{1}{2} \times \cdot 44$	$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$
			$\frac{6\frac{1}{2}}{7 \times 91 \times 40}$		7 7 91 7 11	$\frac{7}{2}$	$\frac{7}{2}$	$\frac{\circ}{7 \times 3\frac{1}{2} \times \cdot 46}$	7 × 21 × .16
90 and 93	$27\frac{1}{2}$		$7 \times 3\frac{1}{2} \times \cdot 40$ $3 \times 3\frac{1}{2} \times \cdot 40$					$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	
under	- 2	Depth of framing	7		$7\frac{1}{2}$	8	8	$8\frac{1}{2}$	81
		Frames	$7 \times 3\frac{1}{2} \times \cdot 42$		$7 \times 3\frac{1}{2} \times \cdot 46$	$7 \times 3\frac{1}{2} \times \cdot 46$	$7 \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$
93 and 96	28	Reversed frames	$3 \times 3\frac{1}{2} \times \cdot 42$		$4 \times 3\frac{1}{2} \times \cdot 46$	$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$5 \times 3\frac{1}{2} \times \cdot 48$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$
		Depth of framing.	7	100	8	$8\frac{1}{2}$	$8\frac{1}{2}$	9	9
oc and	001		$7 \times 3\frac{1}{2} \times \cdot 42$					$7 \times 3\frac{1}{2} \times \cdot 48$	
96 and 99	$28\frac{1}{2}$	Reversed frames Depth of framing	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$		1	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$6 \times 3\frac{1}{2} \times \cdot 48$	$\begin{array}{cc} 6 & \times 3\frac{1}{2} \times \cdot 48 \\ & & \\ 0 & & \end{array}$	$6\frac{10}{2} \times 3\frac{10}{2} \times 48$
			$\frac{7\frac{1}{2}}{7 \times 3\frac{1}{2} \times \cdot 44}$		8½	7 × 31 × ·19	$\frac{32}{7 \times 3\frac{1}{2} \times .48}$	$\frac{3\frac{1}{2}}{7 \times 3\frac{1}{2} \times \cdot 48}$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$
99 and 102	29		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	The broad	d flange of the			$7 \times 3\frac{1}{2} \times \cdot 48$	
		Depth of framing	$7\frac{1}{2}$		me is to be	10	$10\frac{1}{2}$	$10\frac{1}{2}$	11
		Frames	$7 \times 3\frac{1}{2} \times \cdot 44$		fore and aft			$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	
102 and 105	$29\frac{1}{2}$	Reversed frames	$4 \times 3\frac{1}{2} \times \cdot 44$	direction.		$8 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 50$	1
		Depth of framing	8	The later of the first		11	11	11	$11\frac{1}{2}$

[†] The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships; and from the collision bulkhead to one-fifth the vessel's length from stem the spacing is not to exceed 27 inches unless the frames are doubled to the height of the lowest tier of beams.

								1000 00	ntinuation.)
TRANSVERSE	FRAME) AT MIDDLE OF		WAY OF DOUBLE		WAY OF SINGL	E BOTTOMS, TIER OF
B + D	SPACING.†		Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
11 140301			13 and under 14	14 and under 15	15 and 16	16 and under 17	17 and under 18	18 and under 19	19 and under 20
			ONE SIDE STRINGER.	<		TWO SIDE S	TRINGERS — —		
Feet.	inches.		inches,	inches.	inches.	inches.	inches.	inehes.	inches.
60 and 63	23 1	Frames Reversed frames		$\begin{array}{cccc} 4\frac{1}{2} \times 3 & \times \cdot 38 \\ 5 & \times 3 & \times \cdot 38 \end{array}$					
undo.		Depth of framing	6	$6\frac{1}{2}$	$6\frac{1}{2}$	7	7	$7\frac{1}{2}$	$7\frac{1}{2}$
63 and 66	24	Frames Reversed frames	· ·	$5 \times 3 \times \cdot 40$ $4\frac{1}{2} \times 3 \times \cdot 40$					
ounder ou	24	Depth of framing	$6\frac{1}{2}$	$6\frac{1}{2} \wedge 5 \wedge 40$	7	7	$7\frac{1}{2} \wedge 3\frac{1}{2} \wedge 42$	$ \begin{array}{c} 5\overline{2} \times 5\overline{2} \times 4z \\ 7\frac{1}{2} \end{array} $	$7\frac{1}{2}$
aa and aa		Frames		$5 \times 3\frac{1}{2} \times \cdot 40$			- 44	est.	~ ~
66 and 69	24	Reversed frames Depth of framing	$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$ $6\frac{1}{2}$	$5 \times 3\frac{1}{2} \times \cdot 40$	$\begin{array}{c} 5 \times 3\frac{1}{2} \times \cdot 42 \\ 7 \end{array}$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$ $7\frac{1}{9}$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $7\frac{1}{2}$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $7\frac{1}{2}$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdots$
		Frames	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40}$	$\frac{\cdot}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42}$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44}$	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44}$	$\frac{\cdot 2}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44}$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdots$
69 and 72	$24\frac{1}{2}$	Reversed frames	$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$4\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$5 \times 3\frac{1}{2} \times \cdot 42$	$5 \times 3\frac{1}{2} \times \cdot 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdots$
		Depth of framing	$\frac{7}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42}$	$\frac{7}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42}$	$\frac{7\frac{1}{2}}{5\frac{1}{2}\times3\frac{1}{2}\times\cdot44}$	$\frac{7\frac{1}{2}}{5\frac{1}{2}\times3\frac{1}{2}\times\cdot44}$	$\frac{8}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44}$	$\frac{8}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}$	$\frac{8}{5\frac{1}{2} \times 3\frac{1}{2} \times \cdots}$
72 and 75	$24\frac{1}{2}$	Reversed frames		$5 \times 3\frac{1}{2} \times \cdot 42$	-				20 20
		Depth of framing	7	$\frac{7\frac{1}{2}}{51 \cdot 41 \cdot 41}$	$\frac{7\frac{1}{2}}{1}$	8	8	8	$\frac{8\frac{1}{2}}{2}$
75 and 78	25	Frames Reversed frames		$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $5 \times 3\frac{1}{2} \times \cdot 44$				20 20	
	Dayx	Depth of framing	$7\frac{1}{2}$	$7\frac{1}{2}$	8	8	8	$8\frac{1}{2}$	$8\frac{1}{2}$
78 and 81	$25\frac{1}{2}$			$6 \times 3\frac{1}{2} \times \cdot 44$ $5 \times 3\frac{1}{2} \times \cdot 44$					
Ounder OI	202	Depth of framing	$\frac{4_{\overline{2}} \wedge 5_{\overline{2}} \wedge 4_{\overline{4}}}{7_{\overline{2}}^{1}} .$	$\begin{array}{c} 3 \times 3\overline{2} \times 44 \\ 8 \end{array}$	8	$8\frac{1}{2} \wedge 8\frac{1}{2} \wedge 40$	$8\frac{1}{2}$	$\begin{array}{c} 6 \times 3\frac{1}{2} \times 48 \\ 8\frac{1}{2} \end{array}$	$6\overline{2} \times 3\overline{2} \times 4$
and -				$6 \times 3\frac{1}{2} \times \cdot 46$					
81 and 84	26	Reversed frames Depth of framing	$5 \times 3\frac{1}{2} \times \cdot 44$	$5 \times 3\frac{1}{2} \times \cdot 46$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$\begin{array}{cc} 6 & \times 3\frac{1}{2} \times \cdot 48 \\ & & \\ 8\frac{1}{2} & & \end{array}$	$6 \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdots$
			$\frac{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}$	$\frac{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}{6 \times 3}$	$\frac{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}$	$\frac{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}$	$\frac{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}$	$\frac{3}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}$	$\frac{3\frac{1}{2}}{6\frac{1}{2}\times 3\frac{1}{2}\times 4}$
84 and 87	$26\frac{1}{2}$	Reversed frames		$5 \times 3\frac{1}{2} \times \cdot 46$					
		Depth of framing	$\frac{8}{61 \times 31 \times 46}$	$\frac{8\frac{1}{2}}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}$	$\frac{8\frac{1}{2}}{6\frac{1}{2} \times 3\frac{1}{2} \times .48}$	$\frac{9}{6^{\frac{1}{2}} \times 3^{\frac{1}{2}} \times .48}$	$\frac{9}{6\frac{1}{2} \times 3\frac{1}{2} \times .48}$	$\frac{9\frac{1}{2}}{6\frac{1}{2} \times 3\frac{1}{2} \times .48}$	$\frac{10}{7 \times 21 \times 1}$
87 and 90	27			$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$					
		Depth of framing	$8\frac{1}{2}$	81/2	9	$9\frac{1}{2}$	$9\frac{1}{2}$	10	$10\frac{1}{2}$
90 and 93	$27\frac{1}{2}$			$7 \times 3\frac{1}{2} \times \cdot 48$ $5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$					
- under	2	Depth of framing	$8\frac{1}{2}$.	9	$9\frac{1}{2}$	10	$10\frac{1}{2}$	11	11
93 and 96	90	Frames		$7 \times 3\frac{1}{2} \times \cdot 48$					-
90 under 90	28	Reversed frames Depth of framing	$\begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 48 \\ 9\frac{1}{2} \end{array}$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 10	$7 \times 3\frac{1}{2} \times \cdot 48$ $10\frac{1}{9}$	$8 \times 3\frac{1}{2} \times 48$	$8 \times 3\frac{1}{2} \times \cdot 50$	$8 \times 3\frac{1}{2} \times 50$ $11\frac{1}{2}$	$8 \times 3\frac{1}{2} \times \cdot 5$ $11\frac{1}{2}$
1				$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$			and and		$8 \times 3\frac{1}{2} \times \cdot 5$
96 and 99	$28\frac{1}{2}$		1	$8 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 50$	$8 \times 3\frac{1}{2} \times \cdot 50$	1	1	-,
	1.	Depth of framing	$\frac{10\frac{1}{2}}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 52}$	$\frac{11}{7 \times 3\frac{1}{2} \times \cdot 50}$	$\frac{11}{7 \times 3\frac{1}{2} \times \cdot 52}$	$\frac{11\frac{1}{2}}{7 \times 3\frac{1}{2} \times \cdot 52}$	$\frac{11\frac{1}{2}}{8 \times 3\frac{1}{2} \times \cdot 52}$	$\frac{11\frac{1}{2}}{8 \times 3\frac{1}{2} \times \cdot 54}$	$\frac{12\frac{1}{2}}{8 \times 3\frac{1}{2} \times \cdot 5}$
99 and under 102	29	Reversed frames		$8 \times 3\frac{1}{2} \times \cdot 50$				$8 \times 3\frac{1}{2} \times .54$	8 × 4 × · 5
	12900	Depth of framing	11	$\frac{11\frac{1}{2}}{7 \times 91 \times 59}$	$\frac{11\frac{1}{2}}{9 \times 91 \times 59}$	$\frac{11\frac{1}{2}}{9 \times 91 \times .54}$	$\frac{12\frac{1}{2}}{2}$	$12\frac{1}{2}$	$12\frac{1}{2}$
02 and 105	$29\frac{1}{2}$			$7 \times 3\frac{1}{2} \times \cdot 52$ $8 \times 4 \times \cdot 52$					
	104	Depth of framing.	$11\frac{1}{2}$	$11\frac{1}{2}$	$12\frac{1}{2}$	$12\frac{1}{2}$	$12\frac{1}{2}$	hammed I con	

[†] The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships; and from the collision bulkhead to one-fifth the vessel's length from stem the spacing is not to exceed 27 inches unless the frames are doubled to the height of the lowest tier of beams.

(Concluded.)

TRANSVERSE	FRAME			AT MIDDLE OF OM TOP OF MAR	LENGTH FROM GIN PLATE IN T BEAMS AT SI			WAY OF SINGLE OP OF LOWEST	
	SPACING.+		Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet
B + D			20 and under 21	21 and under 22	22 and under 23	23 and under 24	24 and under 25	25 and under 26	26 and under 27
			TWO SIDE STRINGERS.	<		THREE SIDE	STRINGERS.——		
Feet.	inches.		inches.	inches.	inches.	inches.	inches.	inches.	inches.
and an	1				$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$				
60 and 63	$23\frac{1}{2}$	Reversed frames Depth of framing	$5\frac{1}{2} \times 3 \times \cdot 44$	$5\frac{1}{2} \times 3 \times \cdot 46$	$6 \times 3\frac{1}{2} \times \cdot 46$ $8\frac{1}{2}$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$ 10	$\begin{array}{c} 8 \times 3\frac{1}{2} \times \cdot 48 \\ 11 \end{array}$	
		Frames	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$6 \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$7 \times 3\frac{1}{2} \times \cdot 5$
63 and 66	24		$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$6 \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 50$	$8 \times 3\frac{1}{2} \times \cdot 5$
		Depth of framing	8	8	$8\frac{1}{2}$	$\frac{9\frac{1}{2}}{1}$	$\frac{10\frac{1}{2}}{1}$	11	$\frac{11\frac{1}{2}}{1}$
ac and ac	24				$6 \times 3\frac{1}{2} \times \cdot 48$				
66 and 69	24	Depth of framing	$5\frac{1}{2} \times 3\frac{1}{2} \times 46$	$6 \times 3\frac{1}{2} \times \cdot 46$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times 30$ $11\frac{1}{2}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
		Frames	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}{5\frac{1}{2} \times \frac{1}{2} \times \cdot 46}$	$\frac{6}{6} \times 3\frac{1}{5} \times \cdot 48$	$\frac{3}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}$	$\frac{10}{7 \times 3\frac{1}{2} \times \cdot 48}$	$\frac{11}{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50}$		
69 and 72	$24\frac{1}{2}$				$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$				
	-	Depth of framing	$8\frac{1}{2}$	$8\frac{1}{2}$	$9\frac{1}{2}$	$10\frac{1}{2}$	11	$11\frac{1}{2}$	$12\frac{1}{2}$
3				~	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	~ ~	-		
72 and 75	$24\frac{1}{2}$		$6 \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 48$	1	1	- 1
		Depth of framing	$\frac{8\overline{2}}{c}$	9	10		$\frac{11\frac{1}{2}}{7 \times 91 \times 59}$	$\frac{11\frac{1}{2}}{0 \times 01 \times 50}$	$\frac{12\frac{1}{2}}{2}$
75 and 78	25				$7 \times 3\frac{1}{2} \times \cdot 48$ $7 \times 3\frac{1}{2} \times \cdot 48$				
ounder o	20	Depth of framing	9	$9\frac{1}{9}$	$10\frac{1}{2}$	11	$11\frac{1}{2}$	$12\frac{1}{2}$	$12\frac{1}{2}$
		Frames	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 50$	$7 \times 3\frac{1}{2} \times \cdot 52$	$8 \times 3\frac{1}{2} \times \cdot 54$	$8 \times 3\frac{1}{2} \times \cdot 5$
$78_{\mathrm{under}}^{\mathrm{and}}$ 81	$25\frac{1}{2}$		$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 48$	$8 \times 3\frac{1}{2} \times \cdot 50$	$8 \times 4 \times \cdot 52$	$8 \times 3\frac{1}{2} \times \cdot 54$	
		Depth of framing	$9\frac{1}{2}$	10	11	$\frac{11\frac{1}{2}}{1}$	$\frac{11\frac{1}{2}}{1}$	$\frac{12\frac{1}{2}}{1}$	$\frac{12\frac{1}{2}}{2}$
on and on	9.0			20	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$		AND	-	
81 and 84	26	Depth of framing	$7 \times 3\frac{1}{2} \times 40$	$7 \times 3\frac{1}{2} \times 48$ $10\frac{1}{2}$	$8 \times 3\frac{1}{2} \times \cdot 50$	$8 \times 3\frac{1}{2} \times 32$ $11\frac{1}{2}$	$8 \times 3\frac{1}{2} \times 32$ $12\frac{1}{5}$	$12\frac{1}{9}$	$13\frac{1}{2}$
		Frames	$7 \times 3\frac{1}{2} \times \cdot 48$	- 4	$\frac{11}{7 \times 3\frac{1}{2} \times \cdot 50}$	4	4	4	
84 and 87	$26\frac{1}{2}$				$8 \times 3\frac{1}{2} \times \cdot 50$				
		Depth of framing	$10\frac{1}{2}$	11	$11\frac{1}{2}$	$11\frac{1}{2}$	$12\frac{1}{2}$	$12\frac{1}{2}$	$13\frac{1}{2}$
and					$7 \times 3\frac{1}{2} \times \cdot 52$				
87 and 90	27	Reversed frames Depth of framing			$8 \times 3\frac{1}{2} \times \cdot 52$ $11\frac{1}{2}$	$8 \times 3\frac{1}{2} \times \cdot 52$ $12\frac{1}{2}$	$ \begin{array}{c} 8 \times 4 \times \cdot 54 \\ 12\frac{1}{2} \end{array} $	$\begin{array}{c} 9 \times 4 \times \cdot 54 \\ 13\frac{1}{2} \end{array}$	$10 \times 4 \times \cdot 5$ $14\frac{1}{2}$
			$\frac{11}{7 \times 3^{\frac{1}{2}} \times \cdot 50}$	$\frac{11}{7 \times 2 \times 52}$	$\frac{11\overline{2}}{8 \times 3\frac{1}{2} \times \cdot 52}$				
90 and 93	$27\frac{1}{2}$		-	And And	$8 \times 3\frac{1}{2} \times \cdot 52$	and and	Au .	_	
under	-	Depth of framing	$11\frac{1}{2}$	$11\frac{1}{2}$	$12\frac{1}{2}$	$12\frac{1}{2}$	$13\frac{1}{2}$	$14\frac{1}{2}$	$14\frac{1}{2}$
				-	$8 \times 3\frac{1}{2} \times \cdot 54$	24	200		
93 and 96	28		,	-	$8 \times 4 \times \cdot 54$	1	,		
		Depth of framing	$\frac{11\frac{1}{2}}{2}$	$\frac{12\frac{1}{2}}{2}$	$\frac{12\frac{1}{2}}{2}$	$13\frac{1}{2}$	$14\frac{1}{2}$		
96 and 99	$28\frac{1}{2}$			$\begin{array}{ccc} 8 & \times 3\frac{1}{2} \times \cdot 54 \\ 8 & \times 4 & \times \cdot 54 \end{array}$					
under 00	202	Depth of framing	$\begin{array}{c c} & \lambda & 5\frac{1}{2} & \lambda & 54 \\ & 12\frac{1}{2} & \\ \end{array}$	$12\frac{1}{2}$	$13\frac{1}{2}$				
		Frames							
$99_{\mathrm{under}}^{\mathrm{and}}102$	29	Reversed frames		1 72				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
		Depth of framing.							
102 and under 105	$29\frac{1}{2}$	Frames Reversed frames							
102 under 100	292	Depth of framing							

[†] The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships; and from the collision bulkhead to one-fifth the vessel's length from stem the spacing is not to exceed 27 inches unless the frames are doubled to the height of the lowest tier of beams.

FRAMES formed of SINGLE ANGLES or BULB ANGLES.

RANSVERSE	Spacing of	ese ve	FRAMES IN	DEPTH (d) AND FROM TOR			TTOMS, TO TOP OF LOW!	OF SINGLE BOTTOMS, EST TIER OF BEAMS,
NUMBER B + D	Frames.		PEAKS.	Feet.	Feet.	Feet.	Feet.	Feet.
				7 and under 8	8 and under 9	9 and under 10	10 and under 11	11 and under 12
				<		one side stringe	ER	
Feet.	inches.		inches.	inches.	inches.	inches.	inches.	inches.
23 and under 25	20	٨	$3\frac{1}{2} \times 2\frac{1}{2} \times \cdot 24$	$3\frac{1}{2} \times 2\frac{1}{2} \times \cdot 24$	$3\frac{1}{2} \times 2\frac{1}{2} \times \cdot 26$	$4 \times 2\frac{1}{2} \times \cdot 26$	$4 \times 2\frac{1}{2} \times \cdot 28$	
25 and under 27	20		$3\frac{1}{2} \times 2\frac{1}{2} \times \cdot 26$	$3\frac{1}{2} \times 2\frac{1}{2} \times \cdot 26$	$4 \times 2\frac{1}{2} \times \cdot 26$	$4 \times 2\frac{1}{2} \times \cdot 28$	$4 \times 2\frac{1}{2} \times \cdot 30$	$4 \times 2\frac{1}{2} \times \cdot 32$
27 and under 29	$20\frac{1}{2}$		$4 \times 2\frac{1}{2} \times \cdot 26$	$4 \times 2\frac{1}{2} \times \cdot 26$	$4 \times 2\frac{1}{2} \times \cdot 28$	$4 \times 2\frac{1}{2} \times \cdot 30$	$4 \times 2\frac{1}{2} \times \cdot 32$	$4 \times 2\frac{1}{2} \times \cdot 34$
29 and under 31	$20\frac{1}{2}$		$4 \times 2\frac{1}{2} \times \cdot 28$	$4 \times 2\frac{1}{2} \times \cdot 28$	$4 \times 2\frac{1}{2} \times \cdot 30$	$4 \times 2\frac{1}{2} \times \cdot 32$	$4 \times 2\frac{1}{2} \times \cdot 34$	$4 \times 3 \times \cdot 34$
31 and under 33	21		$4 \times 2\frac{1}{2} \times \cdot 30$	$4 \times 2\frac{1}{2} \times \cdot 30$	$4 \times 2\frac{1}{2} \times 32$	$4 \times 2\frac{1}{2} \times \cdot 34$	4 × 3 × ·34	$4\frac{1}{2} \times 3 \times 34$
33 and 35 under 35	21		$4 \times 2\frac{1}{2} \times \cdot 32$	$4 \times 2\frac{1}{2} \times \cdot 32$	$4 \times 2\frac{1}{2} \times \cdot 34$	4 × 3 × · 34	$4\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times \cdot 36$
35 and under 37	$21\frac{1}{2}$	ES.	$4 \times 2\frac{1}{2} \times \cdot 34$	$4 \times 2\frac{1}{2} \times \cdot 34$	4 × 3 × · 34	$4\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 36$	5 × 3 × · 36
37 and under 39	$21\frac{1}{2}$	ANGLES	4 × 3 × · 34	4 × 3 × · 34	$4\frac{1}{2} \times 3 \times \cdot 34$	$4\frac{1}{2} \times 3 \times 36$	5 × 3 × · 36	5 × 3 × · 38
39 and under 42	22		$4\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times \cdot 34$	$4\frac{1}{2} \times 3 \times 36$	5 × 3 × · 36	5 × 3 × ·38	$5\frac{1}{2} \times 3 \times 38$
2 and under 45	22		$4\frac{1}{2} \times 3 \times 36$	$4\frac{1}{2} \times 3$, $\times \cdot 36$	5 × 3 × · 36	5 × 3 × ·38	$5\frac{1}{2} \times 3 \times \cdot 38$	$5\frac{1}{2} \times 3 \times \cdot 40$
45 and under 48	$22\frac{1}{2}$		5 × 3 × · 36	5 × 3 × ·36	5 × 3 × ·38	$5\frac{1}{2} \times 3 \times \cdot 38$	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 36$
8 and under 51	$22\frac{1}{2}$		5 × 3 × · 38	5 × 3 × ·38	$5\frac{1}{2} \times 3 \times \cdot 38$	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times \cdot 38$
of and under 54	23		$5\frac{1}{2} \times 3 \times 38$	$5\frac{1}{2} \times 3 \times 38$	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times 38$	6 × 3 × ·38
54 and under 57	23	\ \	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 36$	$.5\frac{1}{2} \times 3 \times .38$	6 ×3 ×·38	6 × 3 × · 40
7 and do	$23\frac{1}{2}$	^	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times \cdot 38$	6 × 3 × · 38	6 × 3 × ·40	$6\frac{1}{2} \times 3 \times 40$
o and under 63	$23\frac{1}{2}$	ES.	$5\frac{1}{2} \times 3 \times 38$	$5\frac{1}{2} \times 3 \times \cdot 38$	6 × 3 × · 38	6 ×3 ×·40	$6\frac{1}{2} \times 3 \times \cdot 40$	$6\frac{1}{2} \times 3 \times \cdot 42$
3 and under 66	24	ULB ANGLES	6 × 3 × · 38	6 × 3 × · 38	6 × 3 × ·40	$6\frac{1}{2} \times 3 \times \cdot 40$	$6\frac{1}{2} \times 3 \times \cdot 42$	7 × 3 × ·42
6 and under 69	24	B	6 × 3 × ·40	6 × 3 × ·40	$6\frac{1}{2} \times 3 \times \cdot 40$	$6\frac{1}{2} \times 3 \times \cdot 42$	$7 \times 3 \times \cdot 42$	$7 \times 3\frac{1}{2} \times \cdot 44$
9 and vander 72	$24\frac{1}{2}$	\ \	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$7 \times 3\frac{1}{2} \times \cdot 42$	$7 \times 3\frac{1}{2} \times \cdot 44$	$7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$

^{*} The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships.

FRAMES formed of SINGLE ANGLES, BULB ANGLES or CHANNELS.

B + D	OF FRAMES.*		Feet	Feet.	Feet.	Feet.	eet.
0 1 0			12 and under 13	13 and under 14	$14 ^{ m and}_{ m under} 15$	15 and under 16	16 and under 17
			< SIDE	STRINGER>	<	-TWO SIDE STRINGERS.	
Feet. 23 and 25	inches.	^	inches.	inches	inches.	inches.	inches.
25 and 27	20						oe re dimi
27 and 29	$20\frac{1}{2}$		4 × 3 × ·34				400 00 300
29 and 31	$20\frac{1}{2}$	ró	$4\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 36$			\$00 10 £5,0
31 and 33	21	ANGLES	$4\frac{1}{2} \times 3 \times 36$	5 × 3 × ·36	· 5 × 3 × ·38		10 100 100,10
33 and 35	21		5 × 3 × · 36	5 × 3 × ·38	$5\frac{1}{2} \times 3 \times \cdot 38$	$5\frac{1}{2} \times 3 \times \cdot 40$	12 10 22.81
35 and 37	$21\frac{1}{2}$		5 × 3 × · 38	$5\frac{1}{2} \times 3 \times \cdot 38$	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times \cdot 38$
37 and 39	$21\frac{1}{2}$		$5\frac{1}{2} \times 3 \times \cdot 38$	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times 38$	6 × 3 × · 38
39 and 42	22	V	$5\frac{1}{2} \times 3 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times 38$	6 × 3 × · 38	6 × 3 × ·40
42 and 45	22	^	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times 38$	6 × 3 × · 38	6 × 3 × ·40	$6\frac{1}{2} \times 3 \times \cdot 40$
45 and 48	$22\frac{1}{2}$		$5\frac{1}{2} \times 3 \times 38$	6 × 3 × · 38	6 × 3 × ·40	$6\frac{1}{2} \times 3 \times \cdot 40$	$6\frac{1}{2} \times 3 \times \cdot 42$
48 and 51	$22\frac{1}{2}$	1 ×	6 × 3 × · 38	6 × 3 × ·40	$6\frac{1}{2} \times 3 \times \cdot 40$	$6\frac{1}{2} \times 3 \times \cdot 42$	7 × 3 × ·42
$51_{ m under}^{ m and}$ 54	23		6 × 3 × ·40	$6\frac{1}{2} \times 3 \times \cdot 40$	$6\frac{1}{2} \times 3 \times \cdot 42$	7 × 3 × · 42	7 × 3 × ·44
$54_{ m under}^{ m and}$ 57	23	ESC	$6\frac{1}{2} \times 3 \times \cdot 40$	$6\frac{1}{2} \times 3 \times \cdot 42$	7 × 3 × ·42	7 × 3 × ·44	$7\frac{1}{2} \times 3 \times \cdot 44$
57 and 60	$23\frac{1}{2}$	BULB ANGLES.	$6\frac{1}{2} \times 3 \times \cdot 42$	7 × 3 × ·42	7 × 3 × ·44	$7\frac{1}{2} \times 3 \times \cdot 44$	$7\frac{1}{2} \times 3 \times \cdot 46$
60 and 63	$23\frac{1}{2}$	B	7 × 3 × ·42	7 ×3 ×·44	$7\frac{1}{2} \times 3 \times \cdot 44$	$7\frac{1}{2} \times 3 \times \cdot 46$	8 × 3 × ·46
33 and 66	24		7 × 3 × ·44	$7\frac{1}{2} \times 3 \times \cdot 44$	$7\frac{1}{2} \times 3 \times \cdot 46$	8 × 3 × ·46	8 × 3 × ·48
36 and 69	24		$7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$8 \times 3\frac{1}{2} \times \cdot 46$	$8 \times 3\frac{1}{2} \times \cdot 48$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot $
39 and 72	$24\frac{1}{2}$		$7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$8 \times 3\frac{1}{2} \times \cdot 46$	$8 \times 3\frac{1}{2} \times \cdot 48$	$ 7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42 \\ 8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 $	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$

^{*} The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships.

FRAMES formed of BULB ANGLES or CHANNELS.

B + D	OF FRAMES.		Feet.	8	Feet.		Fee 19 and under		Feet. 20 and 21	21	Feet.	22
			<			TWO SIDE			>	TI	HREE S	IDE
Feet.	inches.		inches.		inche	s.	inche	es.	inches.	anioni .	inches	
23 and 25	20									08	68	28,55
25 and 27	20											
27 and 29	$20\frac{1}{2}$							18:3		loe .	02	has vo
29 and 31	$20\frac{1}{2}$					36,×	8 × 6).	14.X	8 × §1	for ,		Esta est
31 and 33	21			88- X	ax g	38- X	dx e	98. X	EXE I	18	188	511, 12
33 and 35	21	0- X	ex le	88- X	8 × {8	88· ×	8 × 4	38: X	6× 61	12	100	hon 38
35 and 37	$21\frac{1}{2}$	08-X	a x la	01- ×	s × ło	88- X	8 × 10	. 88 x	8 × 41	line I	78	
37 and 39	$21\frac{1}{2}$	^	6 × 3 ×	•40	a × 4a	nb-x	8 × 41	88: X	ex (c	Įge .	08	Park 18
39 and 42	22		$6\frac{1}{2} \times 3 \times$	•40	$6\frac{1}{2} \times 3$	× ·42	ex la	01- X	exte va		183	101 DB
42 and 45	22	W X	$6\frac{1}{2} \times 3 \times$	•42	7 × 3	× ·42	7 × 3	× ·44	ex (a A	10	163	Jan es
45 and 48	$22\frac{1}{2}$	Ol X	7 × 3 ×	•42	7 × 3	× ·44	$7\frac{1}{2} \times 3$	× ·44	$7\frac{1}{2} \times 3 \times \cdot 46$		184	
48 and 51	$22\frac{1}{2}$	ANGLES.	7 × 3 ×	•44	$7\frac{1}{2} \times 3$	× ·44	$7\frac{1}{2} \times 3$	× ·46	8 × 3 × · 46	8	× 3	× ·48
51 and 54	23	BULB AI	$7\frac{1}{2} \times 3 \times$	•44	$7\frac{1}{2} \times 3$	× ·46	8 × 3	× ·46	8 × 3 × ·48	$8\frac{1}{2}$	× 3	× ·48
54 and 57	23	HX	$7\frac{1}{2} \times 3 \times$	•46	8 × 3	× ·46	8 × 3	× ·48	$8\frac{1}{2} \times 3 \times 48$	$8\frac{1}{2}$	× 3	× ·50
57 and 60	231	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	8 ×3 ×	•46	8 × 3	× ·48	$8\frac{1}{2} \times 3$	× ·48	$8\frac{1}{2} \times 3 \times \cdot 50$	9	× 3	× ·50
60 and 63	$23\frac{1}{2}$	BLX	8 ×3 ×	•48	$8\frac{1}{2} \times 3$	× ·48	$8\frac{1}{2} \times 3$	× ·50	9 × 3 × ·50	9	× 3	× ·52
63 and 66	24	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	$7\frac{1}{2} \times 3\frac{1}{2} \times 3$ $8\frac{1}{2} \times 3\frac{1}{2} \times 3$		$7\frac{1}{2} \times 3\frac{1}{2} \times 8\frac{1}{2} \times 8\frac{1}{2} \times 3\frac{1}{2}$	$\langle 3\frac{1}{2} \times \cdot 42 \rangle$ $\frac{1}{2} \times \cdot 48$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3$ $8\frac{1}{2} \times 3$	$\times 3\frac{1}{2} \times \cdot 44$ $\frac{1}{2} \times \cdot 50$	$\begin{array}{c} 8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44 \\ 9 \times 3\frac{1}{2} \times \cdot 50 \end{array}$			$3\frac{1}{2} \times \cdot \times \cdot 52$
66 and 69	24	CHANNELS OR BULB ANGLES.	$7\frac{1}{2} \times 3\frac{1}{2} \times 3$ $8\frac{1}{2} \times 3\frac{1}{2} \times$		$7\frac{1}{2} \times 3\frac{1}{2} $	$<3\frac{1}{2}\times\cdot44$ $\frac{1}{2}\times\cdot50$		$\times 3\frac{1}{2} \times \cdot 44$ $\frac{1}{2} \times \cdot 50$	$\begin{array}{c} 8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ 9 \times 3\frac{1}{2} \times \cdot 52 \end{array}$			$3\frac{1}{2} \times \cdot \times \cdot 52$
69 and 72	$24\frac{1}{2}$	CH. CH.	$ \begin{array}{ccc} 8 & \times 3\frac{1}{2} \times 3 \\ 9 & \times 3\frac{1}{2} \times \end{array} $		$ \begin{array}{c} 8 \times 3\frac{1}{2} \\ 9 \times 3\frac{1}{2} \end{array} $	$\times 3\frac{1}{2} \times \cdot 44$		$\times 3\frac{1}{2} \times \cdot 46$ $\frac{1}{2} \times \cdot 52$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 52$			$3\frac{1}{2} \times \cdot \times \cdot 54$

^{*} The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships.

TRANSVERSE NUMBER.	OF			Foot	Deat	See SKETCH ON PA		West
B + D	FRAMES.*			and under 23	Feet. 23 and under 24	Feet. 24 and under 25	Feet. 25 and under 26	Feet. 26 and 27
			<			THREE SIDE STRINGERS		
Feet.	inches.			inches.	inches.	inches.	inches.	inches.
23 and 25	20							
25 and 27	20							
27 and 29	$20\frac{1}{2}$		18 × 17	34- X	8 × 10 × 10 × 10 × 1	6 × 7	182 × 1, 8 × 80	
29 and 31	$20\frac{1}{2}$							
31 and 33	21							
33 and 35	21			1 1 1 1 X	18 N. P. B. T. B. B. P. K.	1×6 14 14	M-X BEX TO	1,32, 84, 35,1
35 and 37	$21\frac{1}{2}$		x lays					
37 and 39	$21\frac{1}{2}$							
39 and 42	22						- 194-X 38-X 18	TE OF 22.5
42 and 45	22		x (8 X	2 11 × 18		v lie v lig ou A		
45 and 48	$22\frac{1}{2}$							
48 and 51	$22\frac{1}{2}$			2 (61- × 48)				3 86 98 0000
	X 18	τή				Texter is		
51 and 54	23	ANGLES	9 ×	(3 ×·50		SECRETARIA MANAGEMENTA CANADA ANTA SECRETARIA DE CONTRA		
54 and 57	23	BULB	9 >	3 ×·52	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 52$		34-148-18	in the latest
57 and 60	$23\frac{1}{2}$	^		$\frac{\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}{3\frac{1}{2} \times \cdot 52}$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 54$	$\begin{array}{c} 9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ 10 \times 3\frac{1}{2} \times \cdot 56 \end{array}$		1
60 and 63	$23\frac{1}{2}$			$\begin{array}{c} \frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ \times 3\frac{1}{2} \times \cdot 52 \end{array}$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $10 \times 3\frac{1}{2} \times \cdot 54$	$ \begin{array}{c c} \hline 10 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ 10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56 \end{array} $	$\begin{array}{c c} 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ & 11 & \times 3\frac{1}{2} \times \cdot 58 \end{array}$	100 EN 552
63 and 66	24	CHANNELS OR BULB ANGLES.		$\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $\times 3\frac{1}{2} \times \cdot 54$	$\begin{array}{c} 9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ 10 \times 3\frac{1}{2} \times \cdot 56 \end{array}$		$ \begin{array}{c c} \hline 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 11 & \times 3\frac{1}{2} \times \cdot 60 \end{array} $	$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 62$ $11\frac{1}{2} \times 3\frac{1}{2} \times \cdot 62$
66 and 69	24	CH BU		$\begin{array}{l} \frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ \times 3\frac{1}{2} \times \cdot 54 \end{array}$	$ \begin{array}{c c} \hline 10 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ 10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56 \end{array} $	$\begin{array}{c c} \hline 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ & 11 & \times 3\frac{1}{2} \times \cdot 58 \end{array}$	$ 11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 11\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60 $	$ \begin{array}{c c} 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \\ 12 \times 3\frac{1}{2} \times \cdot 62 \end{array} $
69 and 72	$24\frac{1}{2}$	\ \ V		$\begin{array}{c} \frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ \times 3\frac{1}{2} \times \cdot 56 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c c} 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 11 & \times 3\frac{1}{2} \times \cdot 60 \end{array} $	$ \begin{array}{c} 11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 52 \\ 11\frac{1}{2} \times 3\frac{1}{2} \times \cdot 62 \end{array} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

^{*} The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships.

FRAMES formed of BULB ANGLES, CHANNELS, or CHANNELS WITH REVERSED FRAMES.

TABLE 3.

(See Continuation.)

Depth (d) at middle of length, from top of floors at centre in way of single bottoms, and from top of margin plate in way of double bottoms, to top of lowest tier of beams, at side. See sketch on page 21. TRANSVERSE Spacing FRAMES IN NUMBER. PEAKS Feet. Feet. Frames B + D8 and 9 9 and 10 10 and under 11 11 and 12 ONE SIDE STRINGER. inches. inches. Feet. inches $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $7 \times 3\frac{1}{2} \times \cdot 42$ $7 \times 3\frac{1}{2} \times \cdot 44$ 72 and 75 24½ $6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$ $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $8 \times 3\frac{1}{2} \times \cdot 46$ 75 and 78 $6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$ $7 \times 3^{1}_{2} \times \cdot 44$ ANGLES $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $8 \times 3\frac{1}{2} \times \cdot 46$ $8 \times 3\frac{1}{2} \times \cdot 48$ 78 and 81 25 1 $7 \times 3^{1}_{2} \times \cdot 42$ BULB $7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$ $7\frac{1}{2} \times 3\frac{1}{2} \times .46$ $8 \times 3\frac{1}{2} \times \cdot 46$ $8 \times 3\frac{1}{2} \times \cdot 48$ 81 and 84 26 $7 \times 3\frac{1}{2} \times \cdot 44$ $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$ $7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ 84 and 87 26 1/2 $8 \times 3\frac{1}{2} \times \cdot 46$ $8 \times 3\frac{1}{2} \times \cdot 48$ $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ $7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$ $7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ $8 \times 3\frac{1}{2} \times .48$ $7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ 87 and 90 27 $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ $9 \times 3\frac{1}{2} \times \cdot 50$ $8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44 \mid 8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$ 90 and 93 27 1/2 $8 \times 3^{1}_{2} \times \cdot 46$ $9 \times 3\frac{1}{2} \times \cdot 52$ $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ $9 \times 3\frac{1}{2} \times \cdot 50$ $9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 52$ BULB ANGLES. $9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 93 and 96 28 $8 \times 3\frac{1}{2} \times \cdot 48$ $9\frac{1}{2} \times 3\frac{1}{2} \times .52$ $9\frac{1}{9} \times 3\frac{1}{9} \times .54$ $10 \times 3\frac{1}{2} \times .54$ $9 \times 3\frac{1}{2} \times \cdot 52$ $9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $9\frac{1}{9} \times 3\frac{1}{9} \times 3\frac{1}{9} \times \cdot 48$ OR 96 and 99 281 $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $9\frac{1}{2} \times 3\frac{1}{2} \times .54$ $10 \times 3\frac{1}{2} \times .54$ $10 \times 3\frac{1}{2} \times .56$ $10 \times 3\frac{1}{2} \times .56$ CHANNELS $10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \mid 10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \mid 10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 99 and 102 29 $8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ $10\frac{1}{2} \times 3\frac{1}{2} \times .56$ $10\frac{1}{2} \times 3\frac{1}{2} \times .58$ $10\frac{1}{5} \times 3\frac{1}{5} \times .58$ 11 $\times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 11 $\times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 11 $\times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ 102 and 105 29½ $9 \times 3\frac{1}{2} \times \cdot 50$ $11 \times 3\frac{1}{2} \times .58$ $11 \times 3\frac{1}{2} \times .58$ $11 \times 3\frac{1}{2} \times \cdot 60$ $8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \quad 8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ 105 and 108 30 $9 \times 3\frac{1}{2} \times \cdot 52$ EX- $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \quad 9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ THE LOWER EDGE OF OF THE LOWEST DECK. $108_{\text{under}}^{\text{and}} 111 \quad 30\frac{1}{2}$ $9\frac{1}{9} \times 3\frac{1}{9} \times .52$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$ $9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \mid 10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 111 and 114 31 $9\frac{1}{2} \times 3\frac{1}{2} \times .54$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ $9 \times 4 \times 4 \times \cdot 52$ $9 \times 4 \times 4 \times \cdot 52 \mid 10 \times 4 \times 4 \times \cdot 50$ 114 and 118 31½ $10 \times 3\frac{1}{2} \times .54$ $4 \times 3\frac{1}{2} \times \cdot 52$ $4 \times 3\frac{1}{2} \times \cdot 52$ $4 \times 3\frac{1}{2} \times \cdot 50$ $10 \times 4 \times 4 \times \cdot 52 \mid 10 \times 4 \times 4 \times \cdot 52 \mid 11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ WITH 118 and 122 32 $10 \times 3\frac{1}{2} \times .56$ $4 \times 3\frac{1}{2} \times \cdot 52$ $4 \times 3\frac{1}{2} \times \cdot 52$ $4 \times 3\frac{1}{2} \times \cdot 50$ TO $11 \times 4 \times 4 \times \cdot 52$ $11 \times 4 \times 4 \times \cdot 52$ $11 \times 4 \times 4 \times \cdot 54$ CHANNELS TENDING T BEAMS $122_{\text{under}}^{\text{and}} 126 \quad 32\frac{1}{2}$ $10\frac{1}{2} \times 3\frac{1}{2} \times .56$ $4 \times 3\frac{1}{2} \times \cdot 52$ $4 \times 3\frac{1}{2} \times \cdot 52$ $4 \times 4 \times \cdot 54$ $11 \times 4 \times 4 \times \cdot 54$ $11 \times 4 \times 4 \times \cdot 54$ $12 \times 4 \times 4 \times \cdot 54$ 126 and 130 33 $10\frac{1}{2} \times 3\frac{1}{2} \times .58$ $4 \times 4 \times \cdot 54$ $4 \times 4 \times \cdot 54$ 4 × 4 × · 54

^{*} The spacing of the frames in the peaks is not to exceed 24 inches where wider spacing is allowed amidships; and from the collision bulkhead to one-fifth the vessel's length from the stem the spacing is not to exceed 27 inches unless the frames are doubled to the height of the lowest tier of beams.

	on wit wheel not			
	der seld selle seller in der selle seller in	made de la company		
	on × (a × (a ×) * ()) on × (a × (a ×) * ())			
mar few feet				
	SE NORM TO NOT SELECT			
	Lan x fairfe in a			
	Se s fe s			
	DE SERVER DE SERVER DE LE SERVER DE			

FLOOR PLATES IN VESSELS WITH SINGLE BOTTOMS.

TRANSVERSE	DEPTH AT	THICK	NESS *		TRANSVERSE	DEPTH AT	THICKN	TESS.*
B + D	CENTRE.	For $\frac{3}{5}$ length Amidships.	At Ends of Vessel.		B + D	CENTRE.	For $\frac{3}{5}$ length Amidships.	At Ends
feet 23 and under 24	inches. $8\frac{1}{2}$	inches.	inches.		48 and under 49	inches.	inches.	inches.
24 and under 25	$8\frac{1}{2}$.24	·24		49 and under 50	20	.36	.32
25 and under 26	9	.24	·24		50 and sinder 51	20	.38	·34
26 and under 27	$9\frac{1}{2}$.24	.24	MIN	$51 ^{ m and}_{ m under} 52$	21	.38	.34
27 and under 28	10	.24	·24	8118	52 and 10 under 53	22	.38	.34
28 and under 29	10	.26	·24	016	53 and 54	22	.40	.34
29 and under 30	$10\frac{1}{2}$.26	·24	nen	54 and $_{ m under}$ 55	23	.40	.34
30 and under 31	11	.26	·24	080	55 and 10 under 10 un	24	.40	.34
31 and 32	$11\frac{1}{2}$.26	·24	K	56 and under 58	. 24	·42	.36
32 and under 33	$11\frac{1}{2}$.28	.26	9889	58 and under 60	25	.42	.36
33 and and and under 34	12	.28	.26	222	60 and der 62	26	·42	.36
34 and 35	$12\frac{1}{2}$.28	.26	8834	62 and under 64	26	.44	.36
35 and under 36	13	.28	.26	ISB	$64 {}^{\mathrm{and}}_{\mathrm{under}} 66$	27	·44	.36
36 and under 37	13	.30	.26	hehi	66 and der 68	28	•44	.36
37 and under 38	$13\frac{1}{2}$.30	.26	ren l	68 and under 70	28	.46	.38
38 and under 39	14	.30	.26		70 and 12	29	.46	.38
39 and 40	$14\frac{1}{2}$.30	.26		72 and under 74	30	.46	.38
40 and under 41	$14\frac{1}{2}$.32	.28	18900	74 and under 76	30	.48	.38
41 and 42	15	.32	.28	MARK	76 and under 78	31	.48	.38
42 and under 43	$15\frac{1}{2}$.	.32	.28	Mark To	78 and under 80	32	.48	.38
$43 _{\mathrm{under}}^{\mathrm{and}} 44$	16	.32	.28	THE REAL PROPERTY.	80 and under 82	32	.50	.40
44 and 45	16	.34	.30		82 and under 84	33	.50	•40
45 and 46	17	.34	.30		84 and under 86	34	.50	•40
$46~^{\rm and}_{\rm under}~47$	18	·34	.30		86 and under 88	35	.50	•40
47 and under 48	18	.36	.32		X 25530 X 18	13- x 3886		

^{*} In the engine space of steam vessels the floors are to be '04 of an inch thicker, and in the boiler space '10 of an inch thicker than required by the Table.

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON-17th June, 1909.

		1	d) AT M	IDDLE OF PLATE IN	LENGTH FF WAY OF I	ROM TOP O	F FLOORS	AT CENTRE	E IN WAY	OF SINGLE	BOTTOMS, WEST LAID	AND FROM	Terridaer or	OF ATES.
NUMBER. B + D.	$\overset{ ext{feet.}}{14}_{ ext{and under}}$	15 and under 16	$16 \atop { m and \ under} \atop 17$	17 and under 18	18 and under 19	$\overset{ ext{feet.}}{19}_{ ext{and under}}$	20 and under 21	21 and under 22	22 and under 23	23 and under 24	$24 \atop ext{and under} \atop ext{}25$	25 and under 26	26 and under	THICKNESS STRINGER PL
	ONE SIDE	STRINGER.	<			rwo side	STRINGERS	5		>	< THREE	SIDE STRI	NGERS. >	STR
48 and under 51	14×30	14×32	14×34	14×36	15×36	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	·30
$51_{\mathrm{under}}^{\mathrm{and}}$ 54	14×·32	14×·34	14×·36	15×36	16×·36	16×·38		9	16	0	88.38	2.88		30
$54_{\mathrm{under}}^{\mathrm{and}}$ 57	14×·34	14×·36	15×·36	16×36	16×·38	17×·38	$18 \times .38$	2	16-	10	79.19	26.2		30
$57_{\mathrm{under}}^{\mathrm{and}}$ 60	14×·36	15×36	16×36	16×·38	17×·38	18×38	$18 \times \cdot 40$	19×·40	$20 \times \cdot 42$	10	88 38	27		.30
60 and 63	15×36	16×36	16×·38	17×·38	18×·38	$18 \times \cdot 40$	$19 \times \cdot 40$	$20 \times \cdot 40$	$21 \times \cdot 42$	$22 \times \cdot 44$	$24 \times \cdot 44$	88		.32
63 and delinder 66	16×36	36×·38	17×·38	18×·38	18×·40	$19 \times \cdot 40$	$20 \times \cdot 40$	$21 \times \cdot 40$	$22 \times \cdot 42$	$23 \times \cdot 44$	$24 \times \cdot 46$	26×·46	$27 \times \cdot 48$	32
66 and moder 69	16×:38	37×38	18×·38	$18 \times \cdot 40$	19×·40	$20 \times \cdot 40$	$20 \times \cdot 42$	$21 \times \cdot 42$	$22 \times \cdot 44$	$24 \times \cdot 44$	25×46	$26 \times \cdot 48$	$28 \times \cdot 48$	34
69 and under 72	17×38	318×38	18×·40	19×·40	$20 \times \cdot 40$	20×42	21×42	$22 \times \cdot 42$	$23 \times \cdot 44$	$24 \times \cdot 46$	$26 \times \cdot 46$	$27 \times \cdot 48$	28×·50	34
72 and under 75	18×38	$18 \times \cdot 40$	$19 \times \cdot 40$	$20 \times \cdot 40$	$20 \times \cdot 42$	$21 \times \cdot 42$	22×42	$23 \times \cdot 42$	$24 \times \cdot 44$	25×46	$26 \times \cdot 48$	$28 \times \cdot 48$	$29 \times .50$	34
$75_{\mathrm{under}}^{\mathrm{and}}$ 78	$18 \times \cdot 40$	$19 \times \cdot 40$	$20 \times \cdot 40$	$20 \times \cdot 42$	$21 \times \cdot 42$	$22 \times \cdot 42$	22×·44	$23 \times \cdot 44$	$24 \times \cdot 46$	26×46	$27 \times \cdot 48$	$28 \times .50$	$30 \times .50$	36
78 and under 81	$19 \times \cdot 40$	20×·40	20×·42	$21 \times \cdot 42$	22×·42	$22 \times \cdot 44$	$23 \times \cdot 44$	$24 \times \cdot 44$	$25 \times \cdot 46$	26×48	28 × ·48	29×·50	$30 \times .52$	36
81 and 84	$20 \times \cdot 40$	20×·42	21×·42	$22 \times \cdot 42$	22×·44	$23 \times \cdot 44$	24×·44	$25 \times \cdot 44$	$26 \times \cdot 46$	27×·48	28×·50	$30 \times .50$	$31 \times .52$	38
.84 and 87	20×42	221×·42	$22 \times \cdot 42$	$22 \times \cdot 44$	23×·44	24×·44	24×·46	$325 \times \cdot 46$	26×48	328×·48	39×·50	$30 \times .52$	$32 \times .52$.38
87 and 90	21 × ·42	22× ·42	22×·44	$23 \times \cdot 44$	24×·44	24×·46	325×46	$326 \times \cdot 46$	27×48	328×·50	30×·50	$31 \times .52$	$32 \times .54$	40
90 and 93	22×·44	123×·44	$24 \times \cdot 44$	$24 \times \cdot 46$	25×·46	26×·46	326×48	$327 \times \cdot 48$	328×·50	30×·50	$31 \times .52$	$32 \times .54$	$34 \times .54$	40
93 and 96	$24 \times \cdot 44$	124×·46	325×46	$26 \times \cdot 46$	26×48	$327 \times \cdot 48$	328×·48	329×48	30×·50	31×·52	32×·54	$34 \times .54$	$35 \times .56$	42
96 and 98	$25 \times \cdot 46$	326×·46	326×48	$27 \times \cdot 48$	328×·48	328×·50)29×·50	$30 \times .50$	31×·52	32×·54	$34 \times .54$	$35 \times .56$	$36 \times .58$	42
99 and 102	$26 \times \cdot 48$	327×·48	328×·48	28×:50	29×·50	30×·50	$30 \times .52$	$231 \times .52$	32×·54	34×·54	$35 \times .56$	$36 \times .58$	$38 \times .58$	44
102 and 105	28×48	$328 \times \cdot 50$)29×·50	30×·50	$30 \times .52$	31×·52	$232 \times .52$	23×52	234×·54	35×·56	36×·58	$38 \times .58$	39×·60	44
105 and 108 under 108	$329 \times .50$	$30 \times .50$	$030 \times .52$	$231 \times .52$	$32 \times .52$	232×·54	133×·54	434×·54	35×·56	$36 \times .58$	38×·58	$39 \times .60$	40×·62	46
108 and under 111	$30 \times .52$	$231 \times \cdot 52$	232×·52	$232 \times .54$	33×·54	34×·54	134×·56	$35 \times .56$	$36 \times .58$	38×·58	39×·60	40×·62	42×·62	46
111 and 114	32×52	$232 \times \cdot 54$	133×·54	34×·54	34×·56	35×·56	36×56	37×·56	$38 \times .58$	39×·60	40×·62	42×·62		48
$114_{\mathrm{under}}^{\mathrm{and}}118$	$33 \times .54$	434×54	134×·56	35×·56	$36 \times .56$	$36 \times .58$	$37 \times .58$	$38 \times .58$	39×·60	040×·62	242×·62			48
118 and 122	234×·56	$635 \times .56$	$36 \times .56$	36×58	$37 \times .58$	$38 \times .58$	38×·60	39×·60	040×·62	242×·62	2	47		.50
122 and under 120	$36 \times .56$	636×58	$837 \times .58$	$38 \times .58$	38×.60	$39 \times \cdot 60$	040×·60)41×:60)42×·62	2	pro oft a			.50
126 and under 130	$37 \times .58$	$8 38 \times .58$	$838 \times .60$	$39 \times .60$	$39 \times .62$	$240 \times \cdot 62$	241×·65	242×-62	2	ad to s	parasti s	axoni		52

INTERMEDIATE FRAMES, FACE ANGLES, &c.

(Concluded.)

TRANSVERSE	WING.*	INTERMEI	DIATE FRAMES.	GGTM STATE OF THE STATE OF THE	FACE ANGLES.	-	FA	CE A	OR STR	INGER
NUMBER. B + D.	AME SPAC	Built Framing.	Bulb Angles.	Channels.	Double on Web Frames, Single on	Din Tength.	eadth.		Number in Straps and Stringer Face Angles	uper in the stand stand stand stands
48 and 10 moder 10 moder 11 moder 11 moder 12 mo	ins. 221	Frames. Reversed Frames. $3\frac{1}{2} \times 3 \times 303 \times 2\frac{1}{2} \times 30$	inches.	inches.	single on Stringers. web Frames. inches. 3 × 3 × 30 5 × 3 × 48		ins.	ins. ·46	Num Stra Stra Face	Stra Web
51 and 54	23	$3\frac{1}{2} \times 3 \times 303 \times 3 \times 30$			$3 \times 3 \times 325 \times 3 \times 50$) ,,	22	22	27	22
54 and 57	23	4 ×3 ×·303 ×3 ×·30		GEXE LEGI	$3 \times 3 \times 345 \times 3 \times 52$	2 27	22	.48	22	22
57 and 60	$23\frac{1}{2}$	$4\frac{1}{2} \times 3 \times 303 \times 3 \times 30$	$\overline{5_{\frac{1}{2}} \times 3 \times 36}$	CEEN LE TRAIS	$3 \times 3 \times 365 \times 3\frac{1}{2} \times 55$	2 ,,	22	22	22	27
60 and 63	$23\frac{1}{2}$	$4\frac{1}{2} \times 3 \times 323 \times 3 \times 32$	$\overline{5_{\frac{1}{2}} \times 3} \times 38$		$3\frac{1}{2} \times 3 \times 365 \times 3\frac{1}{2} \times 56$	1 ,,	27	.50	22	27
63 and 66	24	$5 \times 3 \times 323 \times 3 \times 32$	6 ×3 ×·38	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	$3\frac{1}{2} \times 3 \times 386 \times 3\frac{1}{2} \times 54$	1 ,,	22	22	27	22
66 and 69	24	$5 \times 3 \times 343 \times 3 \times 34$	$6 \times 3 \times \cdot 40$	8x 6 80	$3\frac{1}{2} \times 3 \times 40 6 \times 3\frac{1}{2} \times 50$	3 ,,	22	.52	27	27
69 and 72	$24\frac{1}{2}$	$5\frac{1}{2} \times 3\frac{1}{2} \times 343 \times 3 \times 34$	$6\frac{1}{2} \times 3\frac{1}{2} \times 40$		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40 6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 58$	3 48	7	22	12	4
72 and 75	$24\frac{1}{2}$	$5\frac{1}{2} \times 3\frac{1}{2} \times 34 3\frac{1}{2} \times 3 \times 34$	$6\frac{1}{2} \times 3\frac{1}{2} \times 40$		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42 6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$) ,,	27	.54	27	27
75 and under 78	25	$5\frac{1}{2} \times 3\frac{1}{2} \times 36 3\frac{1}{2} \times 3 \times 36$	$6\frac{1}{2} \times 3\frac{1}{2} \times 42$	8×13 101	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 447 \times 3\frac{1}{2} \times \cdot 60$) ,,	27	27	27	22
78 and under 81	$25\frac{1}{2}$	$6 \times 3\frac{1}{2} \times 36 3\frac{1}{2} \times 3 \times 36$	$7 \times 3\frac{1}{2} \times 42$	W = 8 Ob	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 467 \times 3\frac{1}{2} \times \cdot 68$	2 ,,	22	.56	27	27
81 and 84	26	$6 \times 3\frac{1}{2} \times 38 3\frac{1}{2} \times 3 \times 38$	$7 \times 3\frac{1}{2} \times 44$		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 487 \times 3\frac{1}{2} \times \cdot 64$	1 ,,	27	27	27	22
84 and 87	261	$\frac{1}{2}6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 38$ $3\frac{1}{2} \times 3 \times \cdot 38$	$7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$		$3\frac{1}{2} \times 3\frac{1}{2} \times 50 7 \times 3\frac{1}{2} \times 60$	3 ,,	22	.58	27	27
87 and 90	27	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$ $3\frac{1}{2} \times 3 \times \cdot 40$	$7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$		$3\frac{1}{2} \times 3\frac{1}{2} \times 527 \times 3\frac{1}{2} \times 68$	8 "	22	27	27	27
90 and 93	327	$\frac{1}{2}$ 7 ×3 $\frac{1}{2}$ ×·40 3 $\frac{1}{2}$ ×3 ×·40	$8 \times 3\frac{1}{2} \times \cdot 46$		$4 \times 3\frac{1}{2} \times 52$	54	8	.60	22	27
93 and 96	328	$7 \times 3\frac{1}{2} \times \cdot 42 3\frac{1}{2} \times 3 \times \cdot 42$	$8 \times 3\frac{1}{2} \times \cdot 48$	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 42$	$24 \times 3\frac{1}{2} \times 54$	27	22	22	27	27
96 and 98	28	$\frac{1}{2}$ 7 × 3 $\frac{1}{2}$ × '42 $\frac{3}{2}$ × '42	$8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 4\frac{1}{2}$	$24 \times 3\frac{1}{2} \times 56$	27	27	.62	22	22
99 and 102	29	$7 \times 3\frac{1}{2} \times 44 3\frac{1}{2} \times 3\frac{1}{2} \times 44$	$8\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 44$	$14 \times 3\frac{1}{2} \times 58$	27	27	22	22	27
$102_{\mathrm{under}}^{\mathrm{and}}105$	29	$\frac{1}{2}$ 7 × 3 $\frac{1}{2}$ × '44 4 × 3 $\frac{1}{2}$ × '44	$9 \times 3\frac{1}{2} \times \cdot 50$	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 44$	14 ×4 ×·58	27	27	.64	22	27
105 and 108	30	$7 \times 3\frac{1}{2} \times 464 \times 3\frac{1}{2} \times 46$	$39 \times 3\frac{1}{2} \times 52$	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	34 ×4 × ·60	27	27	22	22	22
$108_{ m under}^{ m and} 111$	130	12	$9\frac{1}{2} \times 3\frac{1}{2} \times 52$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	64 ×4 × 62	27	27	.66	27	22
111 and 114	131		$9\frac{1}{2} \times 3\frac{1}{2} \times 54$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	84 ×4 ×·64	60	12	27	14	6
114 and 118	31	$\frac{1}{2}$		$9 \times 4 \times 4 \times \cdot 48$	$84\frac{1}{2} \times 4\frac{1}{2} \times 64$	27	27	.68	27	27
118 and 122	232	* From the collision bulkho		$9 \times 4 \times 4 \times 5$	$24\frac{1}{2} \times 4\frac{1}{2} \times 66$	"	27	22	27	27
122 and 126	632	the vessel's length from ster of the frames is not to exc when wider spacing is allow	eed 27 inches	$10\times4 \times4 \times 5$	$24\frac{1}{2} \times 4\frac{1}{2} \times 68$	"	27	.70	27	27
126 and 130	STATE OF TAXABLE PARTY.	LEGISTER OF BRITISH AND FORE	1 80 83	$10 \times 4 \times 4 \times 56$	THE RESIDENCE OF THE PARTY OF T	,,	,,	22	22))

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON.—17th June, 1909.

MIDDLE LINE KEELSONS. KEELSON ANGLES. Keelsons with Intercostal Plates. Keelsons with Centre Through Plate. *** LONGITUDINAL Ordinary Keelsons standing Thickness of centre through plate and foundation plates. NUMBER. upon floors.* Internostal Plate For 1 length Thick Thick For Double Angles. For $\frac{1}{2}$ length Thick-For $L \times (B + D)$ Thick ness at Ends. For 1 length Amidships. Ends. length 1 length At Ends. Amilships. Ends. ness at Ends. Amidships. Amidshirs. Amidships inches. Double Angles. inches inches. inches inches. inches inches inches. inches. inches inches. Double Bulb Angles $3 \times 3 \times 30$.26 1400 3 ×3 × ·24 .24 .38 .30 .26 $3 \times 3 \times 24$.26 .26 1200 and under $6\frac{1}{2} \times 3 \times 38$.30 .26 .26 $3\frac{1}{2} \times 3 \times 30$ \times 3×·24 .26 1400 and under 1700 3 $\times 3 \times 24$.24 $7 \times 3 \times 40$.40 .26 1700 and under .32 .28 .26 .28 24 .42 $3\frac{1}{2} \times 3 \times 32$ 3 \times 3×·24 .26 2000 13 × ·24 $7\frac{1}{2}\times3\times42$ $\times 3$ 2000 and under 2400 13 $\times 3$ × ·24 .24 $8 \cdot \times 3 \times 44$.44 $3\frac{1}{2} \times 3\frac{1}{2} \times 32$.32 .28 .26 3 X 3×24 .28 .26 .30 .34 .26 3 3×26 .30 2400 and under $8 \times 3\frac{1}{2} \times 46$ $3\frac{1}{2} \times 3\frac{1}{2} \times 34$.26 2800 $3 \times 3 \times 26$.26 .46 X $8 \times 3\frac{1}{2} \times 48$.30 2800 and under × ·26 26 .48 $4 \times 3\frac{1}{2} \times 34$.34 .26 3 $\times 3 \times 26$.30 .26 3200 13 $\times 3$.36 .30 .26 3 $\times 3 \times 28$.30 3200 and under 3700 13 $\times 3$ $\times .28$.28 $8\frac{1}{9} \times 3\frac{1}{9} \times 48$.48 $4 \times 3\frac{1}{2} \times 36$.26 3700 and under .32 × ·28 .28 $4\frac{1}{2} \times 3\frac{1}{2} \times 36$.36 .28 $3 \times 3 \times 28$.32 4200 3×3 $9 \times 3\frac{1}{2} \times 48$.48 .28 4200 and under 4700 .50 $4\frac{1}{9} \times 3\frac{1}{9} \times 38$.38 .32 .28 3 $3 \times .30$.32 3 $\times 3 \times 30$.30 $9 \times 3\frac{1}{2} \times .50$.28 X Double Bulb Angle Plate. .32 4700 and .36 .28 5200 $3 \times 3 \times 30$.30 11×42 $5\frac{1}{2} \times 3 \times 36$ $3 \times 3 \times 30$.32 .28 .34 5200 and under $3\frac{1}{2} \times 3 \times 30$.30 11×44 .38 $5\frac{1}{5} \times 3 \times 38$.38 .34 .30 $3\frac{1}{2} \times 3 \times 30$.34 .30 5800 5800 and under .34 $3\frac{1}{2} \times 3 \times 32$.32 12 × ·44 .38 $5\frac{1}{2} \times 3 \times 40$.40 .30 $3\frac{1}{2} \times 3 \times 32$.34 6400 .30 .34 6400 and under $3\frac{1}{2} \times 3 \times 32$ $6 \times 3 \times 40$.30 $3\frac{1}{2} \times 3 \times 32$ 7000 .32 12 × ·46 .38 .40 .34 .30 7000 and under 7600 $3\frac{1}{2} \times 3 \times 34$.34 13×46 .38 $6\frac{1}{2} \times 3 \times 40$.40 .36 .32 $3\frac{1}{9} \times 3 \times 34$.36 .32 7600 and under $\times 34$.34 13 × ·48 .36 .32 8200 4×3 .40 $7 \times 3 \times 40$.40 $4 \times 3 \times 34$.36 .32 8200 and under 8800 4×3 $\times 34$.34 14×48 .40 $7\frac{1}{2}\times3\times42$.42 .36 .32 $4 \times 3 \times 34$.36 .32 8800 and 9400 .38 $4 \times 3 \times 36$.34 $14 \times .50$.40 $8 \times 3 \times 44$.44 .34 $4 \times 3 \times 36$.38 .34 9400 and 10000 $15 \times .50$.38 $4 \times 3 \times 36$.34 .40 $8 \times 3\frac{1}{2} \times 46$.46 .34 .38 $4 \times 3 \times 36$.34 Double Bulb Angle 10000 and 10600 .38 $4\frac{1}{2} \times 3 \times 36$.34 15×52 .42 $8 \times 3\frac{1}{2} \times 48$.48 .34 .38 .34 $5\frac{1}{2} \times 3 \times 38$ $10600_{\text{under}}^{\text{and}} 11200 | 4\frac{1}{2} \times 3\frac{1}{2} \times 36$.34 $16 \times .52$.40 .42 $8\frac{1}{2} \times 3\frac{1}{2} \times 48$.48 $5\frac{1}{2} \times 3 \times 40$.36 .40 .36 11200 and 11800 $4\frac{1}{2} \times 3\frac{1}{2} \times 36$.34 16×54 .44 $9 \times 3\frac{1}{2} \times 48$.48 .40 .36 $6 \times 3 \times 40$.40 .36 11800 and 12400 .34 17×54 $9 \times 3\frac{1}{2} \times .50$.40 $5 \times 3\frac{1}{2} \times 36$.44 .50 .36 $6\frac{1}{2} \times 3 \times 40$.40 .36 12400 and 13000 $5 \times 3\frac{1}{2} \times 38$.36 $17 \times .56$.46 10×56 .42 .38 .46 $7 \times 3 \times 40$.42 .38 13000 and 13600 .36 $5 \times 3\frac{1}{2} \times 40$ $18 \times .56$.46 $11 \times .56$.46 .42 .38 $7\frac{1}{2}\times3\times42$.42 .38 13600 and 14200 $5 \times 3\frac{1}{2} \times \cdot 40$.36 18×58 $11 \times .58$.48 .42 .48 .38 .42 $8 \times 3 \times 44$.38 14200 and 14800 $5\frac{1}{9} \times 3\frac{1}{9} \times 40$.36 19 × .58 .48 $12 \times .58$.48 .44 .38 $8 \times 3\frac{1}{2} \times 46$.44 .38 14800 and 15400 .36 $12 \times .60$ $15\frac{1}{5} \times 3\frac{1}{5} \times 40$ 19 $\times .60$.50 .50 .44 .38 $8 \times 3\frac{1}{2} \times 48$.44 .38 15400 and 16000 $5\frac{1}{5} \times 3\frac{1}{5} \times 42$.36 $20 \times .60$ $13 \times .60$.50 .44 .50 .38 $8\frac{1}{2} \times 3\frac{1}{2} \times 48$.44 .38 16000 and 16600 $6 \times 3\frac{1}{2} \times 42$.36 20×62 .52 13×62 .52 .46 .40 .46 $9 \times 3\frac{1}{2} \times 48$.40 16600 and 17200 21×62 $6 \times 3\frac{1}{2} \times 42$.36 .52 14×62 .52 .46 .40 9 $\times 3\frac{1}{2} \times .50$.46 .40 Plate, Four Angles and R ider Plate 17200 and 18000 .38 $6 \times 3\frac{1}{2} \times 44$ 21 $\times .64$.54 14×64 .54 .46 .40 .46 .40 11 18000 and 19000 .38 $6 \times 3\frac{1}{9} \times 44$ 22 × .64 .54 $15 \times .64$.54 .46 .40 12 .46 .40 19000 and 20000 $6 \times 3\frac{1}{2} \times 44$.38 22 $\times .66$.56 $15 \times .66$.56 .46 .40 12 .46 .40 20000 and 21000 .38 $6\frac{1}{2} \times 3\frac{1}{2} \times 44$ 23 $\times .66$.56 16×66 .56 .48 .40 13 .48 .40 21000 and 22000 $6\frac{1}{2} \times 3\frac{1}{2} \times 44$.38 23×68 .58 16×68 .58 .48 .42 13 .48 .42 22000 and 24000 $6\frac{1}{9} \times 3\frac{1}{9} \times 46$.38 $24 \times .68$.58 $17 \times .68$.58 .48 .42 14 .48 .42 24000 and 26000 $6\frac{1}{2} \times 3\frac{1}{2} \times 46$.38 $24 \times .70$.60 $17 \times .70$.60 .48 .42 14 .48 .42 Plate, Four Angles, Ric and Foundation I r Plat 26000 and 28000 $6\frac{1}{5} \times 3\frac{1}{5} \times 48$.38 25 $18 \times .70$ $\times .70$ $\cdot 60$.60 .50 .42 15 .50 .42 28000 and 30000 $6\frac{1}{2} \times 3\frac{1}{2} \times 48$.38 × ·70 26 19 $\times .70$.60 .60 .50 .42 16 .50 .42 30000 and 32000 $6\frac{1}{2} \times 3\frac{1}{2} \times .50$.40 × ·72 26 .62 $19 \times .72$.62 .50 .42 16 .50 .42 32000 and 34000 $6\frac{1}{2} \times 3\frac{1}{2} \times .50$.40 × .72 27 .62 $20 \times .72$.62 .50 .42 17 .50 .42 34000 and 36000 $7 \times 3\frac{1}{2} \times .50$.40 $28 \times .72$.62 21 $\times .72$.62 .52 .44 18 .52 .44

KEEL ANGLES and SIDE 173 KEELSONS in VESSELS with SINGLE BOTTOMS.

		1			
LONGVENDANIA	FLAT KEE	L	SIDE KE	EELSONS.	
LONGITUDINAL	PLATE ANG	LES.			
NUMBER.			For 1 length	Thickness	Intercostal
$L \times (B + D)$	For $\frac{1}{2}$ length	Thickness	Amidships.	at Ends.	Plates.
	Amidships.	at Ends.		Ends.	
	inches.	inches.	inches. Double Angles.	inches.	inches.
1200 and 1400	$3 \times 3 \times 24$.24	$3 \times 3 \times 24$.24	.22
1400 and 1700	$3 \times 3 \times 24$.24	$3 \times 3 \times 24$.24	.22
1700 and 2000	$3 \times 3 \times 24$	·24	$3 \times 3 \times 24$.24	.24
2000 and 2400	$3 \times 3 \times 24$	·24	$3 \times 3 \times 24$.24	.24
2400 and 2800	$3 \times 3 \times 26$.26	$3 \times 3 \times 26$.26	.26
2800 and 3200	$3 \times 3 \times 26$.26	$3 \times 3 \times 26$.26	.26
3200 and under 3700	$3 \times 3 \times 28$.28	$3 \times 3 \times 28$.28	.26
3700 and 4200	$3 \times 3 \times 28$.28	$3 \times 3 \times 28$.28	.28
4200 and 4700	$3 \times 3 \times 30$.30	$3 \times 3 \times 30$.30	.28
, undo					-28
4700 under 0200	$3 \times 3 \times 32$	-32	$3 \times 3 \times 30$.30	
J200 under J000	$\frac{3\frac{1}{2} \times 3\frac{1}{2} \times 32}{21 \times 21 \times 24}$	-32	$\frac{3\frac{1}{2} \times 3}{21 \times 2} \times \frac{30}{21}$.30	.30
JOOO under OTO	$\frac{3\frac{1}{2}\times3\frac{1}{2}\times\cdot34}{31\times31\times34}$.34	$\frac{3\frac{1}{2}\times3\times32}{21\times2}$.32	.30
0400 under 7000	$\frac{3\frac{1}{2}\times3\frac{1}{2}\times34}{21\times226}$	34	$\frac{3\frac{1}{2}\times3}{21\times2}\times32$.32	.30
7000 under 7000	$\frac{3\frac{1}{2} \times 3\frac{1}{2} \times 36}{21 \times 21 \times 29}$.36	$3\frac{1}{2} \times 3 \times 34$	*34	.32
7000 under 0200	$3\frac{1}{2} \times 3\frac{1}{2} \times 38$.38	$4 \times 3 \times 34$	•34	-32
8200 and under 8800	$3\frac{1}{2} \times 3\frac{1}{2} \times 40$	•40	$4 \times 3 \times 34$	•34	-32
8800 and 9400	$3\frac{1}{2} \times 3\frac{1}{2} \times 42$	•40	$4 \times 3 \times 36$	•34	•34
9400 and 10000	$3\frac{1}{2} \times 3\frac{1}{2} \times 42$	•40	$4 \times 3 \times 36$.34	•34
$10000_{\rm under}^{\rm and} 10600$	$3\frac{1}{2} \times 3\frac{1}{2} \times 44$.42	$4\frac{1}{2} \times 3 \times 36$.34	.34
10600 and 11200	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	•44	$\frac{1}{4\frac{1}{2} \times 3\frac{1}{2} \times 36}$	•34	•36
11200 and 11800	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	•46	$4\frac{1}{2} \times 3\frac{1}{2} \times 36$	•34	.36
11800 and 12400	$\frac{3}{4} \times 4 \times 48$	•46	$5 \times 3\frac{1}{2} \times 36$	•34	.36
					.00
12400 and 13000	$4 \times 4 \times 48$	•46	$5 \times 3\frac{1}{2} \times 38$.36	.38
13000 and 13600	$4 \times 4 \times \cdot 48$	•46	$5 \times 3\frac{1}{2} \times 40$.36	-38
13600 and 14200	$4 \times 4 \times 48$	•46	$5 \times 3\frac{1}{2} \times 40$.36	-38
14200 and 14800	$4 \times 4 \times 50$	•46	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40}{51}$.36	.38
14800 and 15400	$4 \times 4 \times 50$	•46	$5\frac{1}{2} \times 3\frac{1}{2} \times 40$.36	-38
15400 and 16000	$4 \times 4 \times 50$	•46	$\frac{5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42}{3}$.36	.38
16000 and 16600	$4 \times 4 \times 52$	•48	$\frac{6 \times 3\frac{1}{2} \times 42}{31 \times 42}$.36	•40
16600 and 17200	$4 \times 4 \times 52$	•48	$6 \times 3\frac{1}{2} \times 42$ Double Bulb	·36	. 40
17200 and under 18000	$4 \times 4 \times 52$.48	$7 \times 3\frac{1}{2} \times 42$	·40	.40
18000 and 19000	$4 \times 4 \times 54$		$8 \times 3\frac{1}{2} \times 46$	•44	•40
19000 and 20000	$4 \times 4 \times 54$		$9 \times 3\frac{1}{2} \times .50$.46	•40
20000 and 21000	$4 \times 4 \times 56$.52	$10 \times 3\frac{1}{2} \times 54$	•48	•40
			Plate, Four Angles & Ri	der Plate.	-
21000 and 22000	$4 \times 4 \times 56$	•52	11×50	•40	•42
22000 and 24000	$4 \times 4 \times 58$	•54	$\frac{12 \times 52}{12 \times 54}$	•42	•42
24000 and under 26000	$4 \times 4 \times 58$.54	13×54	•44	•42
26000 and 20000	41 . 41	. = 4	14 4.50	.46	.42
26000 and 20000	$\frac{4\frac{1}{2} \times 4\frac{1}{2} \times .58}{41 \times .41 \times .60}$	•54	14 × ·56	•46	•42
28000 and 30000	$\frac{4\frac{1}{2} \times 4\frac{1}{2} \times .60}{41 \times .41 \times .60}$		15 × ·58	•48	•42
30000 and 32000	$\frac{4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60}{41 \times \cdot 41 \times \cdot \cdot 60}$	•54	16 × ·60	.50	
32000 and 34000	$\frac{4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60}{41 \times 41 \times \cdot 60}$	_	17×62	•52	•42
34000 and 36000	$4\frac{1}{2} \times 4\frac{1}{2} \times 60$.54	18 × ·64	.54	:44

TABLE 6.

* Where flat plate keels are adopted intercostal plates or centre through plates must be fitted.

** Where a centre through plate keelson is adopted foundation plates must be fitted of the thickness of the centre through plate, and extending not less than 12 inches on each side of the middle line.

† The thickness of rider plates is to be as required for the vertical plates, and the width is to be one inch greater than the sum of the wide flanges of the angles.

†† The foundation plate is to be 18×50 inches.

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON, 17th June, 1909.

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SIDE STRINGERS.

NUMBER. L × (B + D)	SIDE STRINGER ANGLES.	SIDE STRINGER INTER- COSTAL PLATES.	LONGITUDINAL NUMBER. $L \times (B + D)$	SIDE STRINGER ANGLES.	SIDE STRINGER INTER- COSTAL PLATES.
	inches.	inches.		inches.	inches.
1200 and under 2000	$3 \times 3 \times 24$.22	15400 and 16000	$5\frac{1}{2} \times 3\frac{1}{2} \times .42$.38
$2000~^{\rm and}_{\rm under}~2400$	$3 \times 3 \times 24$	·24	16000 and 16600	$6 \times 3\frac{1}{2} \times 42$.38
$2400~^{\rm and}_{\rm under}~2800$	3 ×3 × ·26	.24	16600 and 17200	$6 \times 3\frac{1}{2} \times 42$.40
2800 and under 3200	3 ×3 × ·26	·26	17200 and 20000	$6 \times 3\frac{1}{2} \times \cdot 44$	•40
3200 and under 3700	3 ×3 × ·28	·26	20000 and 22000	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	•40
3700 and 4200	3 ×3 × ·28	.28	22000 and 26000	$6\frac{1}{2} \times 3\frac{1}{2} \times .46$	•42
4200 and 4700	3 ×3 × ·30	.28	26000 and 30000	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	·42
4700 and 5200	3 ×3 × ·30	.30	30000 and 32000	$6\frac{1}{2} \times 3\frac{1}{2} \times .50$	·42
5200 and 5800	$3\frac{1}{2} \times 3 \times 30$.30	32000 and under 34000	$6\frac{1}{2} \times 3\frac{1}{2} \times .50$	•44
5800 and 0400	$3\frac{1}{2} \times 3 \times 32$.30	34000 and 38000	$7 \times 3\frac{1}{2} \times .50$	•44
6400 and moder 7000	$3\frac{1}{2} \times 3 \times 32$.32	38000 and 42000	$7 \times 3\frac{1}{2} \times .52$	•44
7000 and under 7600	$3\frac{1}{2} \times 3 \times 34$.32	42000 and 45000	$7 \times 3\frac{1}{2} \times .52$	•46
7600 and winder 8200	4 ×3 × ·34	.32	45000 and 51000	$7 \times 3\frac{1}{2} \times .54$	•46
8200 and under 8800	4 ×3 × ·34	·34	51000 and s4000	7 ×4 × ·54	•46
8800 and 10000	4 ×3 × ·36	•34	54000 and 57000	7 ×4 × ·56	·46
10000 and 10600	$4\frac{1}{2} \times 3 \times 36$	•34	57000 and 60000	7 ×4 × ·56	•48
10600 and 11200	$4\frac{1}{2} \times 3\frac{1}{2} \times 36$	•34	60000 and 63000	7 ×4 × ·58	•48
11200 and 11800	$4\frac{1}{2} \times 3\frac{1}{2} \times 36$	·36	63000 and 66000	7 ×4 × ·60	.48
11800 and 12400	$5 \times 3\frac{1}{2} \times 36$	·36	66000 and 70000	7 ×4 × ·62	•48
12400 and 13000	$5 \times 3\frac{1}{2} \times .38$	•36	70000 and 74000	8 ×4 × ·62	•48
13000 and 13600	$5 \times 3\frac{1}{2} \times \cdot 40$.36	74000 and 78000	8 ×4 × ·64	.50
13600 and 14200	$5 \times 3\frac{1}{2} \times \cdot 40$.38	78000 and under 82000	8 ×4 × ·66	.50
14200 and 15400	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$.38		70	

Intercostal plates attached to the outside plating are to be fitted to the side stringers, where the depth of framing exceeds 3 inches by Table 2, and 4 inches by Table 3.

The number of side stringers to be as required by Tables 2 and 3.

(See Continuation.)

		ENTRE ELLULA			SIDE	GIR	DERS.	MAE	GIN PI	LATE.	CELLU	LAR BO	OTTOM,	Height		11	NNER 1	воттом	PLAT	ING.	
LONGITUDINAL	above Keel.	2	Thicknes	ss.	т	hickne	ess.	2	hicknes	s.	- 201	hicknes	-	of Tank Side Brackets		ile Line t in Boile			Thic	kness.	
NUMBER.	a about	Half		-	In F	Iolds.	7	In E	lolds.		In H	olds.		above Top of	ch.	Thick	rness.	In H	olds.	In	In
$L \times (B + D),$	Depth g Top of	Length Amid- ships.	At Ends.	In Boiler Space.	Halt Length Amids.	At Ends	In Boil'r Space	Half Length Amid- ships.	At Ends.	In Boiler Space.	Half Length Amid- ships.	At Ends.	In Boiler Space.	Margin Plate.	Breadth.	Half Length Amid- ships.	At Ends.	Half Length Amid- ships.	At Ends.	Engine Space.	Middle
Under 7500	ins. 30	ins. ·36	ins. ·30	ins. ·46	ins28	ins. ·28	ins. ·38	ins. ·30	ins. ·30	ins. ·40	ins. ·28	ins. ·28	ins. ·38	ins.	ins. 30	ins. ·34	ins.	ins. ·28	ins. ·28	ins.	ins. •44
7500 and 9000	31	.38	.32	.48	.28	.28	.38	.32	.32	.42	.30	.30	.40	5	31	.36	.32	.30	.28	.34	.46
9000 and 10500	32	.40	.34	.50	.30	.30	.40	.34	.34	.41	.30	.30	.40	8	32	.38	.32	.30	.28	.34	•46
10500 and 12000	33	•40	.34	.50	.30	.30	.40	.34	.34	•44	.30	.30	•40	11	33	.38	.32	.30	.28	.34	.46
12000 and 14000	34	.42	.36	.52	.30	.30	.40	.36	.36	.46	.32	.32	.42	14	34	.40	.34	.32	.30	.36	.48
14000 and 16000	35	.44	.36	.54	.32	.32	.42	.36	.36	.46	.32	.32	.42	17	35	.40	.34	.32	.30	.38	.48
16000 and under 18000	36	.46	.38	.56	.32	.32	.42	.38	.38	.48	.34	.34	.44	18	36	.42	.36	.34	.30	.40	.50
18000 and 20000	37	.46	.38	.56	.34	.34	.44	.40	.40	.50	.34	.34	.44	19	37	.44	.36	.36	.32	.42	.52
20000 and 22000	38	.48	.38	.58	.34	.34	.44	.40	.40	.50	.34	.34	.44	20	38	.44	.36	.36	.32	.44	.52
22000 and 24000	39	.48	.38	.58	.34	.34	.44	.42	.42	.52	.36	.34	.46	21	39	.44	.36	.36	.32	.44	.52
24000 and 26500	40	.48	.38	.58	36	.34	.46	.42	.42	.52	.36	.34	.46	22	40	.46	.38	.38	.34	.46	.54
26500 and 29000	41	.50	.40	.60	.36	.34	.46	.44	.44	:52	.38	.36	.48	23	41	.48	.40	.38	.34	.46	.54
29000 and 31500	42	.50	.40	.60	.38	.36	.48	.46	.46	.56	.40	.36	.50	24	42	.50	•40	•40	.34	.48	.56
31500 and 34000	43	.50	•40	.60	.40	.36	.50	.48	.48	.58	.40	.36	.50	25	43	.50	•40	.40	.36	.48	.56
34000 and 36800	44	.52	.42	.60	.40	.36	.50	.48	.48	.58	.40	.36	.50	26	44	.52	.42	.40	.36	.50	.56
36800 and 39600	45	.54	.44	.62	.40	.36	:50	.50	.50	.58	.42	.38	.52	27	45	.52	.42	•40	.36	.50	.56
$39600_{\mathrm{under}}^{\mathrm{and}}42600$	46	.56	.46	.62	.42	.38	.52	.50	.50	.58	.42	.38	.52	28	46	.54	•44	.42	.38	.52	.58
$42600_{\mathrm{under}}^{\mathrm{and}}45600$	47	.58	.46	.64	.42	.38	.52	.52	.52	.58	.44	.40	.54	29	47	.54	.44	.42	.38	.52	.58
$45600_{\rm under}^{\rm \ and} 48600$	48	.60	.48	.64	•44	.40	.54	.52	.52	.58	.46	.40	.54	30	48	.56	.46	.44	.40	.54	.60
$48600_{\rm under}^{\rm \ and}51800$	49	.62	.48	.66	.46	.40	.54	.54	.54	.60	.46	.40	.54	31	49	.58	.46	.46	•40	.56	.62
$51800_{\rm under}^{\rm and}55000$	50	:64	.50	.68	.46	.40	.54	.56	.56	.60	.48	.42	.54	32	50	.58	.46	.48	.42	.58	.62
$55000_{\mathrm{under}}^{\mathrm{and}} 58400$	51	.66	.50	.70	.48	.42	.54	.58	.58	.62	.48	.42	.54	33	51	.60	.46	.48	.42	.58	.64
$58400_{\rm under}^{\rm and} 61800$	52	.68	.52	.72	.48	.42	.54	.60	.58	.64	.50	.42	.54	34	52	.60	.46	.50	.44	.60	.64
$61800_{\rm under}^{\rm and} 65400$	53	.70	.54	.74	.50	.42	.54	.62	.58	.66	.50	.42	.54	35	52	.62	.48	.52	.44	.62	.66
$65400_{\rm under}^{\rm and} 69000$	54	.72	.56	.76	.50	.42	.54	.64	.60	.68	.52	.42	.56	36	53	.64	.50	.52	.44	.62	.66
69000 and 72800	55	.74	:58	.78	.52	.42	.56	.66	.62	.70	.52	.42	.56	37	53	.66	.52	.54	•44	.64	.66
72800 and 76700	56.	.78	.60	.82	.52	.42	.56	.68	.64	.72	.54	•44	.58	38	54	.68	.54	.54	•44	.64	.68
$76700_{\rm under}^{\rm and} 81000$	57	.82	.62	.86	.54	.44	.58	.72	.66	.76	.54	.44	.58	39	54	.70	.58	.56	.46	.66	.70

Number of SIDE GIRDERS in CELLULAR DOUBLE BOTTOMS.

FLOOR . PL	ATES AT EVERY FRAME.		FLOOR PLATE	ES AT ALTERNATE FRAME	ES.
	be in accordance with the dring the greater number.	Number of Side Girders on each side		be in accordance with the niring the greater number.	Number of Side Girders on each side
Rule Breadth of Vessel.	Breadth of Inner Bottom Amidships.	exclusive of Margin Plate.	Rule Breadth of Vessel.	Breadth of Inner Bottom Amidships.	exclusive of Margin Plate
Under 50	Under 36	1	Under 34	Under 28	1
50 and under 62	36 and 48	2	34 and under 50	28 and under 36	2
62 and under 74	48 and under 60	3			
74 and under 86	60 and 72	4	and and and areas	0.001	

DOUBLE BOTTOMS.

(Concluded.)

			DIM	ENSIONS OF ANGLE	BARS (a).	g and tanks	ramin
LONGITUDINAL NUMBER. L × (B + D),	Angles connecting Centre Girder to Flat Keel Plate.	Angles at top of Centre Girder in Cellular Bottom.	Angles connecting Margin Plate to outside Plating.	Frames and Reversed Frames on Floors in Cellular Bottom, Side Girder Angles and Vertical Angles on Centre Girder and Margin Plate.	Vertical Angles connecting Floors and Side Girders.	Intermediate Frames where Floors are fitted at alternate Frames.	Intermediate Reversed Frames where Floors are fitted at alternate Frames.
Under 7500	ins. ins. ins. $3\frac{1}{2} \times 3\frac{1}{2} \times 36$	ins. ins. ins. $3 \times 3 \times 34$	$3 \times 3 \times 30$	ins. ins. ins. $3 \times 3 \times 28$	ins. ins. ins. $2\frac{1}{2} \times 2\frac{1}{2} \times 28$	ins. ins. ins. $3\frac{1}{2} \times 3 \times 30$	ins. ins. ins. $3 \times 2\frac{1}{2} \times 26$
7500 and 9000	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$3 \times 3 \times 36$	$3 \times 3 \times 32$	$3 \times 3 \times 30$	$\frac{2\frac{1}{2} \times 2\frac{1}{2} \times \cdot 30}{2}$	$3\frac{1}{2} \times 3 \times 32$	$3 \times 2\frac{1}{2} \times 28$
9000 and 10500	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$		$3\frac{1}{2} \times 3\frac{1}{2} \times 34$		$2\frac{1}{2} \times 2\frac{1}{2} \times 30$		$3 \times 2\frac{1}{2} \times 28$
$\frac{10500_{\mathrm{under}}^{\mathrm{and}}12000}{10500_{\mathrm{under}}^{\mathrm{and}}12000}$	$\frac{3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}{3 \cdot \frac{1}{2} \times \frac{1}{2} \times \cdot 46}$	$3 \times 3 \times 38$	$3\frac{1}{2} \times 3\frac{1}{2} \times 34$	$3 \times 3 \times 30$	$2\frac{1}{2} \times 2\frac{1}{2} \times 30$	$4 \times 3 \times 34$	$3 \times 3 \times 30$
$\frac{12000_{\mathrm{under}}^{\mathrm{and}}14000}{12000_{\mathrm{under}}^{\mathrm{and}}14000}$	$4 \times 4 \times 48$	$3 \times 3 \times 40$	$3\frac{1}{2} \times 3\frac{1}{2} \times 36$	$3 \times 3 \times 32$	$2\frac{1}{2} \times 2\frac{1}{2} \times 32$	$4\frac{1}{2} \times 3 \times 34$	3 ×3 × ·30
$\overline{14000_{\mathrm{under}}^{\mathrm{and}}16000}$	$4 \times 4 \times 50$	$3 \times 3 \times 40$	$3\frac{1}{2} \times 3\frac{1}{2} \times 36$	$3 \times 3 \times 32$	$2\frac{1}{2} \times 2\frac{1}{2} \times \cdot 32$	$\frac{1}{4\frac{1}{2}\times3\times36}$	$3\frac{1}{2} \times 3 \times 32$
16000 and 18000	$4 \times 4 \times 52$	$3 \times 3 \times 42$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 38$	$3 \times 3 \times 34$	$3 \times 3 \times 34$	$5 \times 3 \times 36$	$\frac{1}{3\frac{1}{2}\times3}\times3$
18000 and 20000	$4 \times 4 \times 54$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$3\frac{1}{2} \times 3\frac{1}{2} \times 34$	$3 \times 3 \times 34$	$5 \times 3\frac{1}{2} \times 38$	$3\frac{1}{2} \times 3 \times 34$
20000 and 22000	$4 \times 4 \times 56$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$3\frac{1}{2} \times 3\frac{1}{2} \times 36$	$3 \times 3 \times 34$	$5 \times 3\frac{1}{2} \times \cdot 40$	$4 \times 3 \times 36$
22000 and 24000	$4 \times 4 \times 58$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$3\frac{1}{2} \times 3\frac{1}{2} \times 36$	$3 \times 3 \times 36$	$5 \times 3\frac{1}{2} \times \cdot 42$	$4 \times 3 \times 38$
$\overline{24000_{\mathrm{under}}^{\mathrm{and}}26500}$	$4 \times 4 \times 58$	$3\frac{1}{2} \times 3\frac{1}{2} \times 46$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$3\frac{1}{2} \times 3\frac{1}{2} \times 36$	$3 \times 3 \times 36$	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$4 \times 3 \times 40$
26500 and 29000	$4\frac{1}{2} \times 4\frac{1}{2} \times 58$	$3\frac{1}{2} \times 3\frac{1}{2} \times 48$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$3\frac{1}{2} \times 3\frac{1}{2} \times 38$	3 ×3 × ·38	$5\frac{1}{2} \times 3\frac{1}{2} \times 44$	$4\frac{1}{2} \times 3 \times 42$
29000 and 31500	$4\frac{1}{2} \times 4\frac{1}{2} \times 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times .50$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$3\frac{1}{2} \times 3\frac{1}{2} \times 40$	$3 \times 3 \times 40$	$5\frac{1}{2} \times 3\frac{1}{2} \times 46$	$4\frac{1}{2} \times 3\frac{1}{2} \times 44$
31500 _{under} 34000	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times 50$	$4 \times 4 \times 48$	$3\frac{1}{2} \times 3\frac{1}{2} \times 40$	$3 \times 3 \times 40$	$5\frac{1}{2} \times 3\frac{1}{2} \times 48$	
34000 and 36800	$4\frac{1}{2} \times 4\frac{1}{2} \times 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times 52$	$4 \times 4 \times \cdot 48$	$3\frac{1}{2} \times 3\frac{1}{2} \times 42$	$3 \times 3 \times 40$	- 190 100	-
36800 and 39600	$4\frac{1}{2} \times 4\frac{1}{2} \times 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times 52$	$4 \times 4 \times 50$	$3\frac{1}{2} \times 3\frac{1}{2} \times 44$	$3 \times 3 \times 42$		-
$39600_{\rm under}^{\rm and} 42600$	$5 \times 5 \times 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times 54$	$4 \times 4 \times 50$	$3\frac{1}{2} \times 3\frac{1}{2} \times 44$	$3 \times 3 \times 42$		
$\overline{42600_{\mathrm{under}}^{\mathrm{\ and}}45600}$	$5 \times 5 \times 62$	$3\frac{1}{2} \times 3\frac{1}{2} \times 54$	$4 \times 4 \times 52$	$3\frac{1}{2} \times 3\frac{1}{2} \times 46$	$3 \times 3 \times 44$		_
$\overline{45600_{\mathrm{under}}^{\mathrm{and}}48600}$	$5 \times 5 \times 62$	$3\frac{1}{2} \times 3\frac{1}{2} \times .56$	$4 \times 4 \times 52$	$3\frac{1}{2} \times 3\frac{1}{2} \times 48$	$3 \times 3 \times 46$	- 1	
48600 and 51800	$5 \times 5 \times 62$	$3\frac{1}{2} \times 3\frac{1}{2} \times .58$	$4 \times 4 \times 54$	$3\frac{1}{2} \times 3\frac{1}{2} \times 50$	$3 \times 3 \times 46$		av Tenor
51800 and 55000	$5 \times 5 \times 64$	$3\frac{1}{2} \times 3\frac{1}{2} \times .58$	$4 \times 4 \times 56$	$3\frac{1}{2} \times 3\frac{1}{2} \times 52$	$3\frac{1}{2} \times 3\frac{1}{2} \times 48$		-
$\overline{55000_{\mathrm{under}}^{\mathrm{and}}58400}$	$5 \times 5 \times .66$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$	$4 \times 4 \times 58$	$3\frac{1}{2} \times 3\frac{1}{2} \times 54$	$3\frac{1}{2} \times 3\frac{1}{2} \times 48$		_
58400 and 61800	$5 \times 5 \times 68$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$	$4 \times 4 \times \cdot 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times 54$	$3\frac{1}{2} \times 3\frac{1}{2} \times 50$		Marie Charles
61800 and 65400			The street of the same of the		THE RESIDENCE OF THE PARTY OF T	Appropriate and the second	-
65400 and 69000	$5 \times 5 \times 72$	$3\frac{1}{2} \times 3\frac{1}{2} \times 64$	$4 \times 4 \times 64$	$4 \times 4 \times 56$	$3\frac{1}{2} \times 3\frac{1}{2} \times 52$	- 02	18 87
69000 and 72800	$5 \times 5 \times .74$	$4 \times 4 \times 66$	$4 \times 4 \times 66$	$4 \times 4 \times 58$	$3\frac{1}{2} \times 3\frac{1}{2} \times 52$	constanting of the last	
72800 and 16700	$5 \times 5 \times .76$	$4 \times 4 \times \cdot 68$	$4 \times 4 \times \cdot 68$	$4 \times 4 \times 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times 54$	-12	
76700 and s1000	$5 \times 5 \times .80$	$4 \times 4 \times .72$	$4 \times 4 \times .72$	$4 \times 4 \times \cdot 60$	$3\frac{1}{2} \times 3\frac{1}{2} \times 54$	- 198	188 4 18

(41) All angle bars in boiler space (except those attached to outside plating and covered with cement) to be '10 of an inch thicker than given in the above Table.

In all cases where flanged plates are adopted as a substitute for fitting angles on the edges of floors, brackets, intercostal plates, &c., the faying surface should not be less than the breadth of the flange of the angle required by the rule.

Where floors and intercostal plates are flanged on their lower edges as a substitute for fitting attachment angles to the outside plating, such plates are to be '02 of an inch thicker than that given in the Table.

All angles (except margin angles) may be reduced in thickness as follows:-

Thickness for half length amidship ... '40 and under '50 | '50 and under '60 | '60 and under '70 | '70 and under '80 | '04 | '06 | '08

The margin angles where '60 and above in thickness may be reduced at the ends of the vessel to the same extent as the margin plates to which they are attached.

The floors are to be attached to the centre girder by double angles throughout the engine and boiler spaces in all cases, and where the transverse number is 66 or above, they are to be attached by double angles for one-half the vessel's length amidships.

Where double bottoms are constructed with girders on top of ordinary floors, the frames and reversed frames on the floors are to be of the same thickness as the floor plates to which they are attached, and the breadth of flanges to be as required for frames and reversed frames on floors in cellular bottoms.

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON.—15th December, 1910.

Depths of MARGIN PLATE OF DOUBLE BOTTOMS AND ATTACHMENTS of side TABLE 9. framing and tank side brackets to margin plate and inner bottom plating.

		рертн (d)	AT MIDDLE	e of LEN	GTH FROM T	OP OF MARG	IN PLATE	TO TOP OF	LOWEST TI	ER OF BE	AMS AT SIDI	G.
TRANSVERSE	01.6 0 01.6 0 01.6 0	Feet. 7 and under 1	0	Y 120	10 and under	13		Feet. and under 1	16		16 and under	9
	Depth of Margin	Attachmer Margin P		Depth of Margin	Attachmen Margin F	nt outside Plate. (a)	Depth of Margin	Attachmer Margin F	nt outside Plate. (a)	Depth of Margin	Attachme Margin I	nt outside Plate. (a)
B+D.	Plate (exclusive of flange).	Angle Attachment.	Gussets to Floor Brackets.	Plate (exclusive or flange).	Angle Attachment.	Gussets to Floor Brackets.	Plate (exclusive of flange).	Angle Attachment.	Gussets to Floor Brackets.	Plate (exclusive	Angle Attachment.	Gussets to Floor Brackets
Under 45	inches.	Single angle.	08 - 8-	inches.	Single angle.	32	inches. 21	Single angle.	- THE X	inches,	0.	
$45_{\mathrm{under}}^{\mathrm{and}}$ 48	20	27	08 8	21	27	12-	22	27	I A	18-18	Tocasily	ann ac
48 and 51	21	27		22	27		23	27	3 <u>21</u> 3X	24	Single angle.	00201
$51_{\mathrm{under}}^{\mathrm{and}}$ 54	22	27	00:5.10	23	"	10 X 10	24	27	- A	25	22	- N. <u>22</u>
$54_{ m under}^{ m and}$ 57	23	"	18 <u>x</u> 8 x	24	"	- 81 <u>- 3</u> 7 (8	25	27	26 <u>26</u> %	25	Double angles from collision bulkhead to one-fourth vessel's length from stem.	Every fifth frame.
$57_{\mathrm{under}}^{\mathrm{and}}$ 60	24	27	<u> </u>	25	27		25	27	The Array	26	22	27
60 and 63	25	"	08 <u>2</u> 8 x	25	27	81 <u> </u>	26	Double angles from collision bulkhead to one-fourth vessel's length from stem.	6 <u>25</u> X	27	"	27
63 and 66	25	27	01 - 2 ×	26	Double angles from collision bulkhead to one-fourth vessel's length from stem.	81=x 18 81=x 18	27	27	Every fifth frame.	28	"	Every fourth frame.
$66_{\mathrm{under}}^{\mathrm{and}}$ 69	26	Double angles from collision bulkhead to one-fourth vessel's length from stem.	9-X 8X	27	27	Every fifth frame.	28	27	27	29	Double angles from collision bulkhead to after end of engine room.	27
69 and 72	27	27	Every fifth frame.	28	27	27	29	27	Every fourth frame.	30	27	27
72 and 75	28	27	27	29	"	Every fourth frame.	30	Double angles from collision bulkhead to after end of engine room.	"	31	"	Every third frame.
75 and 78	29	"	Every fourth frame	30	Double angles from collision bulkhead to after end of engine room.	27	31	27	27	32	27	27
78 and 81	30	Double angles from collision bukhead to after end of engine room.	27	31	27	27	32	27	Every third frame.	33 •	27	n
81 and 84	31	, ,,	"	32	22	Every third frame.	33	27	27	34	27	"
84 and 87	32		Every third frame.	33	22	22	34	27	27	35	22	Every second frame.
87 and 90	33	27	"	34	22	22	35	27	Every second frame.	36	"	22
90 and 93	34	,,,	22	35	22	Every second frame.	36	. 27	"	37	Double angles fore and aft.	27
93 and 96	35	"	Every second frame.	36	27	22	37	Double angles fore and aft.	27	38	27	22
96 and 99	36	"	27	37	Double angles fore and aft.	"	38	27	27	39	27	Every frame
99 and 102	37	Double angles fore and aft.	"	38	"	22	39	27	27	40	27	27
102 and 105	38	"	"	39	27	27 .	40	27	Every frame.	41	27	27
$105_{\mathrm{under}}^{\mathrm{and}}108$	39	27	27	40	27	Every frame.	41	27	27	42	27	27
108 and 114	40	27	Every frame.	41	27	27	42	27	27	43	27	22
$114_{\mathrm{under}}^{\mathrm{and}}122$	41	27	27	42	27	27	43	"	27	44	"	27
122 and 130	42	"	"	43	27	"	44	27	27	_	_	_

Depths of MARGIN PLATE OF DOUBLE BOTTOMS AND ATTACHMENTS of side framing and tank side brackets to margin plate and inner bottom plating.

TABLE 9.

(Concluded.)

TRANSVERSE		Feet.			Feet.			Feet.	-
NUMBER.		19 and under			22 and under 2		d 400	25 and under 2	
B + D.	Depth of Margin		ent outside Plate. (a)	Depth of Margin	Attachme Margin	nt outside Plate. (a)	Depth of Margin Plate	Attachme Margin 1	nt outside Plate. (a)
	Plate (exclusive of flange).	Angle Attachment.	Gussets to Floor Brackets.	Plate (exclusive of flange).	Angle Attachment.	Gussets to Floor Brackets.	(exclusive of flange).	Angle Attachment.	Gussets to Floor Bracket
Under 45	inches.			inches.			inches.	and and	
							287 18		
45 and 48						1000	16 X 16		
48 and 51									
51 and 54 and 57 and 57		Double angles from collision bulkhead to one-fourth vessel's length from stem.	Every fourth frame.				1		
57 and 60	27	27	27	_	_	-	-		_
60 and 63	28	Double angles from collision bulkhead to after end of engine room.	27	29	Double angles from collision bulkhead to after end of engine room.	Every third frame.	1 s × 4 s	- in	10- 89
63 and 66	29	"	27	30	27	27	11 <u>~</u> [4	10 <u>v</u> .16	[m8s
66 and 69	30	27	Every third frame.	31	"	Every second frame.	32	Double angles fore and aft.	Every fram
69 and 72	31	27	27	32	"	27	33	27	27
72 and 75	32	27	27	33	27	27	34	27	27
$75_{\mathrm{under}}^{\mathrm{and}}$ 78	33	"	27	34	Double angles fore and aft.	27	35	27	"
78 and 81	34	27	Every second frame.	35	27	. 27	36	27	27
81 and 84	35	27	"	36	27	Every frame.	37	"	27
84 and 87	36	Double angles fore and aft.	27	37	"	27	38	"	"
87 and 90	37	27	27	38	27	27	39	27	"
90 and 93	38	27	Every frame.	39	27	27	40	27	"
93 and 96	39	27	27	40	27	22	41	27	27
96 and 99	40	27	27	41	27	27	_	_	
99 and 102	41	27	22	42	27	27	920	35-2-617	1 - p
$102_{\mathrm{under}}^{\mathrm{and}}105$	42	27	27	43	27	27		-	_
$105_{\mathrm{under}}^{\mathrm{and}} 108$	43	27	27	_	all man a hor	_	_	_	-
$108_{\mathrm{under}}^{\mathrm{and}}114$	44	27	27	_	1903	400			
$114_{\mathrm{under}}^{\mathrm{and}}122$	_	× 4	- X 1	_					_
122 and 130	-	_		_	ales I manage	-	-	_	

CONNECTION	OF FLOO	RS AND
OUTSIDE	BRACKET	S TO
MAR	GIN PLATI	ES.
Depth of Margin Plate.	Number of Rivets in each flange of vertical angles.	Diameter of Rivets.
inches. inches.		inch.
$19_{\mathrm{under}}^{\mathrm{and}}24$	5	$\frac{3}{4}$
$24_{\mathrm{under}}^{\mathrm{and}}28$	6	$\frac{3}{4}$
$28_{\mathrm{under}}^{\mathrm{and}}30$	6	$\frac{7}{8}$
$30_{\rm under}^{\rm \ and}35$	7	$\frac{7}{8}$
$35_{\mathrm{under}}^{\mathrm{and}}40$	8	7/8
$40_{\rm under}^{\rm \ and} 44$	9	$\frac{7}{8}$
Where doub	le angles	are fitted

(a) If it is desired to dispense with the double angles, other efficient methods of connection may be submitted for approval.

there may be one rivet less than required above.

In high powered vessels, when the Committee may consider it necessary, the gusset plates are to be fitted on every frame in way of the machinery space, or a continuous plate may be fitted in lieu of gusset plates.

The breadth of the margin plate may be gradually reduced abaft the three-fifths length amidships towards the after end of the tank where it may be 15 per cent. less than the midship depth.

All web frames are to be attached to the margin plate by double angles. Where web frames are 15 inches and above in depth, they are also to be attached to the inner bottom plating by gusset plates or angles. Where the web frames are 17 inches and under 20 inches in depth, an additional gusset is to be fitted to the frame midway between the webs; where 20 inches and under 26 inches in depth, gussets are to be fitted at every alternate frame; and where 26 inches and above in depth, a gusset is to be fitted at every frame.

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON. 17th June, 1909.

Thickness of PLATING and dimensions of VERTICAL STIFFENING for WATERTIGHT BULKHEADS.

TABLE 10. (See Continuation.)

HEAD A	OF BUI AT MIDI ROM UPI TO TOP O	PER OF	THICK OF BUL PLAT	KHEAD	ANGLES ATTACH	E PLATING,		FLOORS OR INNER	RE FROM LOWEST BOTTOM PLATING OR LOWER 'TWEEN	: ALSO HEIGHT OF
LOWER ANY E 'TWEEN LOWE	M; ALSO R PART (EFFICIEN DECKS, R TWEE TIFFENE	OF NT FOR	At Floor or Double Bottom.	At Upper Deck.	Double Angles to Outside Plating and Double Bottom, and Single Angles to Deck.	Single Angles to Outside Plating and Double Bottom.		Under 8	Feet. 8 and under 9	Feet. 9 and 10
	Feet.		Inches.	Inches.	Inches.	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	Angle	$\begin{array}{c} \text{Inches.} \\ 3 \times 2\frac{1}{2} \times \cdot 30 \end{array}$	Inches.	Inches
8 1	and 10)	•26	•26		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	Angle		$3\frac{1}{2} \times 2\frac{1}{2} \times \cdot 30$	$4 \times 2\frac{1}{2} \times \cdot 30$
10 τ	and under 12	2	•26	•26		$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	Angle			10 32,10
12 "	and under 14	1	•28	•26		4 × 4 × · 40	Angle	$3\frac{1}{2} \times 3 \times \cdot 36$	100	
14 ,	and under 16	6	•30	•26	3 × 3 × · 30	$4 \times 4 \times \cdot 42$	Angle	4 × 3 × · 36	$4\frac{1}{2} \times 3 \times \cdot 36$	5 × 3 × ·38
16 1	and under 18	8	•30	•26	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 30$	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 42$	Angle	$4\frac{1}{2} \times 3 \times 36$	5 × 3 × · 36	$5 \times 3 \times \cdot 40$
18 ,	and under 20	0	-32	•28	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 32$	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 44$	Angle or Bulb Angle Flanged Plate	5 × 3 × · 36	5 × 3 × · 38	$5\frac{1}{2} \times 3 \times 36$ 6×3
20	and under 22	2	-32	•28	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 32$	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 46$	Angle or Bulb Angle	5 × 3 × ·38	5 × 3 × ·40	$5\frac{1}{2} \times 3 \times 38$ 6×3
22 ,	and under 24	4	•34	•30	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 34$	5 × 5 × ·46	Angle or Bulb Angle		$5\frac{1}{2} \times 3 \times \cdot 36$ 6×3	$5\frac{1}{2} \times 3 \times 38$ 6×3
24	and under 20	6	•34	•30	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 34$	5 × 5 × ·48	Angle or Bulb Angle		$5\frac{1}{2} \times 3 \times \cdot 38$ 6×3	$5\frac{1}{2} \times 3 \times \cdot 40$ 6×3
26	and under 28	8	•36	•30	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 36$	5 × 5 × ·50	Bulb Angle Flanged Plate		$5\frac{1}{2} \times 3 \times \cdot 40$ 6×3	6 × 3 × · 40 7 × 3
28	and under 3	0	•36	•30	4 × 4 × ·36	$5 \times 5 \times \cdot 52$	Bulb Angle	$5\frac{1}{2} \times 3 \times \cdot 38$	6 × 3 × ·40 6 × 3	$6\frac{1}{2} \times 3 \times \cdot 40$ 7×3
30	and under 3	2	-38	.30	4 × 4 × ·38	5 × 5 × ·54	Bulb Angle		6 × 3 × ·40 6 × 3	$6\frac{1}{2} \times 3 \times \cdot 40$ 7×3
32	and under 3	4	•40	•30	$4 \times 4 \times \cdot 40$	5 × 5 × · 56	Bulb Angle Flanged Plate		6 × 3 × ·40 6 × 3	7 × 3 × ·40 7 × 3
34	and under 3	6	•40	•30	4 × 4 × · 40	6 × 6 × · 56	Bulb Angle		$\begin{array}{ccc} 6 & \times 3 & \times \cdot 40 \\ & 7 \times 3 & \end{array}$	7 × 3 × ·40 8 × 3
36	and under 3	8	•42	•30	$4 \times 4 \times \cdot 42$	6 × 6 × · 58	Bulb Angle Flanged Plate		$6\frac{1}{2} \times 3 \times \cdot 40$ 7×3	7 × 3 × ·40 8 × 3
38	and under 4	-()	•42	•30	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 44$	6 × 6 × · 60	Bulb Angle		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7 × 3 × ·42 8 × 3
. 40	and under 4	2	•44	•30	$4\frac{1}{2}\times4\frac{1}{2}\times\cdot46$	6 × 6 × · 62	Bulb Angle		7 × 3 × ·40 8 × 3	$7\frac{1}{2} \times 3 \times \cdot 44$ 9×3
42	and under 4	4	.44	•30	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 46$	6 × 6 × ·62	Bulb Angle	$6\frac{1}{2} \times 3 \times \cdot 40$	7 × 3 × ·40 8 × 3	$7\frac{1}{2} \times 3 \times \cdot 4$ 9×3
44	and under 4	16	•46	•30	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 48$	6 × 6 × ·64	Bulb Angle		$7\frac{1}{2} \times 3 \times \cdot 42$ 8×3	8 × 3 × · 44 9 × 3
46	and under 4	18	•46	•30	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 48$	6 × 6 × ·64 ·	Bulb Angle		$7\frac{1}{2} \times 3 \times \cdot 44$ 8×3	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
48	and under 5	50	.46	.30	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 50$	6 × 6 × ·64	Bulb Angle	$7\frac{1}{2} \times 3 \times \cdot 42$		$8\frac{1}{2} \times 3 \times \cdot 40$ $7\frac{1}{2} \times 3 \times 3 \times \cdot \cdot$

For Footnotes see page 184.

VERTICAL STIFFENING for WATERTIGHT BULKHEADS.

VERTICAL	STIFFENING	for WATE	RTIGHT BULK	CHEADS.	See Continuation.)
	Feet. 10 and under 11	Feet. 11 and under 12	Feet. 12 and under 13	Feet. 13 and 14	Feet. 14 and under 15
Angle	Inches. $4\frac{1}{2} \times 3 \times 30$	Inches. $4\frac{1}{2} \times 3 \times 34$	Inches.	Inches.	Inches.
Angle			5 × 3 × · 36	$5\frac{1}{5} \times 3 \times \cdot 40$	- no has as
Angle or Bulb Angle	5 × 3 × · 40			2	$5\frac{1}{2} \times 3 \times \cdot 36$
Angle or Bulb Angle		$5\frac{1}{2} \times 3 \times \cdot 38$	THE RESERVE AS THE PERSON OF T		2
	$\frac{5\frac{1}{2} \times 3 \times \cdot 38}{}$	$5\frac{1}{2} \times 3 \times \cdot 40$	6 × 3 × ·40 7 × 3	6 × 3 × ·40 7 × 3	8
Bulb Angle	$5\frac{1}{2} \times 3 \times \cdot 40$	$6 \times 3 \times \cdot 40$	6 × 3 × ·40	$6\frac{1}{2} \times 3 \times \cdot 40$	7 × 3 × ·42
					8 × 3
	7 × 3	7 × 3	7 × 3	8 × 3	$7 \times 3 \times \cdot 44$ 9×3
		$6\frac{1}{2} \times 3 \times \cdot 40$ 7×3	$7 \times 3 \times \cdot 42$ 8×3	$7 \times 3 \times \cdot 44$ 9×3	$7\frac{1}{2} \times 3 \times \cdot 46$ 9×3
Channel		7 × 3 × ·42	7 × 3 × ·44	$7\frac{1}{2} \times 3 \times \cdot 46$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Flanged Plate					10 × 3
Channel					$8\frac{1}{2} \times 3 \times \cdot 46$ $7\frac{1}{2} \times 3 \times 3 \times \cdot 40$
Flanged Plate					$10 \times 3\frac{1}{2}$
Channel				$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
Channel			$7 \times 3 \times 3 \times \cdot 40$	$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	
Bulb Angle					$9 \times 3 \times \cdot 50$
Channel			$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	$8 \times 3 \times 3 \times \cdot 40$	
	$7\frac{1}{2} \times 3 \times \cdot 44$	8 × 3 × ·46	$8\frac{1}{2} \times 3 \times \cdot 46$	9 × 3 × · 50	$9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$
	9×3 $71 \times 9 \times 46$				
Channel		$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	$8 \times 3 \times 3 \times \cdot 40$	$8 \times 3 \times 3 \times \cdot 44$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$
Bulb Angle	$7\frac{1}{2} \times 3 \times \cdot 46$	$8\frac{1}{2} \times 3 \times \cdot 46$	9 × 3 × · 50	$9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 52$	$ \begin{array}{c c} 12 \times 3\frac{1}{2} \\ \hline 10 \times 3\frac{1}{2} \times \cdot 52 \end{array} $
	10 × 3	$10 \times 3\frac{1}{2}$	$11 \times 3\frac{1}{2}$	$12 \times 3\frac{1}{2}$	12 × 4
Channel	$7 \times 3 \times 3 \times \cdot 40$	$8 \times 3 \times 3 \times \cdot 40$	$8 \times 3 \times 3 \times \cdot 46$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$
Flanged Plate	$\frac{10 \times 3}{8\frac{1}{2} \times 3 \times 46}$	$10 \times 3\frac{1}{2}$ $9 \times 3 \times \cdot 46$	$\frac{11 \times 3\frac{1}{2}}{9\frac{1}{2} \times 3\frac{1}{2} \times 50}$	$ \begin{array}{c c} 12 \times 3\frac{1}{2} \\ \hline 10 \times 3\frac{1}{2} \times 52 \end{array} $	12×4 $10 \times 3\frac{1}{2} \times .56$
Channel	$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	$8 \times 3 \times 3 \times \cdot 40$	$8\frac{1}{2} \times 3 \times 3 \times \cdot 46$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 12×4
Bulb Angle Channel	$9 \times 3 \times \cdot 46$	$9 \times 3 \times \cdot 50$	$9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$10 \times 3\frac{1}{2} \times \cdot 54$	$10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56$
Flanged Plate	10 × 3	$10 \times 3\frac{1}{2}$	$11 \times 3\frac{1}{2}$	$12 \times 3\frac{1}{2}$	12 imes 4
	Angle Angle or Bulb Angle Angle or Bulb Angle Bulb Angle Bulb Angle Flanged Plate Bulb Angle Flanged Plate Bulb Angle Flanged Plate Bulb Angle Flanged Plate Bulb Angle Channel Flanged Plate	DEPTH AT CEN Feet. 10 and	DEPTH AT CENTRE FROM LOWEST REIGHT OF TWEEN 10 and 11 under 12 11 and 12 12 11 and 12 12 11 under 12 12 11 under 12 12 12 13 14 15 12 13 14 15 15 15 15 15 15 15	DEFTH AT CENTRE FROM LOWEST DECK TO TOP OF FLOW and in the control of the contr	PRIFE AT GREATER FROM LOWER TO TOP OF FLOORS OR INMER BOTTO' Feet

For Footnotes see page 184.

VERTICAL STIFFENING for WATERTIGHT BULKHEADS.

(See Continuation.)

Foot From the property	DEPTH OF BULK- HEAD AT MIDDLE	1961	DEPTH AT CENTRE	FROM LOWEST DECK TO	TOP OF FLOORS OR INNER	BOTTOM PLATING.
14	LINE FROM UPPER DECK TO TOP OF FLOORS OR DOUBLE	MOSTOR ACTOR AN ARTICLE ACTOR COMPANY	Feet. 15 and under 16	Feet. 16 and under 17		
10 under 10 Hander 10 Hander Plate.			$5\frac{1}{2} \times 3 \times \cdot 40$	Inches.	Inches.	Inches.
Bunder 20	16 and under 18	designat.				nine at the or
Planged Plate.	18 and under 20		88 × 87 - 4	(i)-× 8		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20 and under 22			x 2 8 x 4 8 08 x 2 8	And the second	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	22 and under 24	Channel	01-X 11-X 2 04-	$7 \times 3 \times 3 \times \cdot 40$	$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	Departs Of when \$1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	24 and under 26	Channel	$7 \times 3 \times 3 \times \cdot 40$	$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$8 \times 3 \times 3 \times \cdot 44$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	26 and under 28	Channel	$7\frac{1}{2} \times 3 \times 3 \times \cdot 40$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$8\frac{1}{2} \times 3 \times 3 \times \cdot 46$ $12 \times 3\frac{1}{2}$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	28 and under 30	Channel	$8 \times 3 \times 3 \times \cdot 40$	8 × 3 × 3 × ·44	$8\frac{1}{2} \times 3 \times 3 \times \cdot 46$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	30 and under 32	Channel	$8 \times 3 \times 3 \times \cdot 44$	$8\frac{1}{2} \times 3 \cdot \times 3 \times \cdot 46$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	32 and 34	Channel	$8\frac{1}{2} \times 3 \times 3 \times \cdot 46$	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	34 and 36 under 36	Channel	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	36 and 38	Channel	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	38 and 40	Channel	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$
10 10 10 10 10 11 10 11 10 11 10 11 10 11 10 10 11 10	40 and 42	Channel	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 13×4	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$ 14×4
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	42 and 44		4 4		14 × 4	
Flanged Plate	44 and 46	Channel	$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ 15×4
Flanged Plate	46 and under 48	Channel	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$ 14×4	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	48 and under 50	Channel	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56$

For Footnotes see page 184.

DEPTH OF BULK-		DEPTH AT CENTRE	FROM LOWEST DECK TO	TOP OF FLOORS OR INNER	R BOTTOM PLATING.
LINE FROM UPPER DECK TO TOP OF LOORS OR DOUBLE BOTTOM.		Feet. 19 and under 20	Feet. 20 and under 21	Feet 21 and 22	Feet. 22 and 23
Feet. 18 and under 20	Bulb Angle	Inches. $7\frac{1}{2} \times 3 \times \cdot 46$ 10×3	Inches.	Inches.	Inches.
20 and under 22	Bulb Angle	01- × (0 × (0 ×)	$ \begin{array}{cccc} 8 & \times 3 & \times \cdot 46 \\ 7 & \times 3 & \times 3 & \times \cdot 40 \\ & & 10 \times 3\frac{1}{2} \end{array} $	$\begin{array}{c} 8\frac{1}{2} \times 3 & \times \cdot 46 \\ 7\frac{1}{2} \times 3 & \times 3 & \times \cdot 40 \\ & 11 \times 3\frac{1}{2} \end{array}$	orad
22 and 24 under 24	Bulb Angle			1000	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
24 and under 26	Bulb Angle	$\begin{array}{c} 9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 8\frac{1}{2} \times 3 \times 3 \times \cdot 46 \\ 12 \times 3\frac{1}{2} \end{array}$		dissa	Man OE Ame SE
26 and under 28	Bulb Angle	$\begin{array}{c} 9\frac{1}{2} \times 3\frac{1}{2} \times \cdot 52 \\ 8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ 12 \times 4 \end{array}$	$ \begin{array}{ccc} 10 & \times 3\frac{1}{2} \times \cdot 52 \\ 9 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ & 12 \times 4 \end{array} $	$ \begin{array}{ccc} 10 & \times 3\frac{1}{2} \times \cdot 54 \\ 9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ & 13 \times 4 \end{array} $	28 100 08
28 and under 30	Bulb Angle	$ \begin{array}{c} 10 \times 3\frac{1}{2} \times \cdot 52 \\ 9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ 12 \times 4 \end{array} $	$ \begin{array}{rr} 10 & \times 3\frac{1}{2} \times \cdot 54 \\ 9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ & 13 \times 4 \end{array} $	$ \begin{array}{c} 10\frac{1}{2} \times 3\frac{1}{2} \times .56 \\ 10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times .48 \\ 13 \times 4 \end{array} $	$10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$ $10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 5$ 14×4
30 and under 32	Bulb Angle	$ \begin{array}{c} 10 \times 3\frac{1}{2} \times \cdot 54 \\ 9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ 13 \times 4 \end{array} $	$ \begin{array}{c} 10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56 \\ 10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \\ 13 \times 4 \end{array} $	$ \begin{array}{c} 10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60 \\ 10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 14 \times 4 \end{array} $	$ \begin{array}{ccc} 11 & \times 3\frac{1}{2} \times \cdot 60 \\ 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 5 \\ & 15 \times 4 \end{array} $
32 and under 34	Bulb Angle	$10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56$ $10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 13×4	$ \begin{array}{c} 10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60 \\ 10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 14 \times 4 \end{array} $	$ \begin{array}{c c} 11 & \times 3\frac{1}{2} \times \cdot 60 \\ 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ & 14 \times 4 \end{array} $	$ \begin{array}{c} 11\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60 \\ 11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 5 \\ 15 \times 4 \end{array} $
34 and under 36	Bulb Angle	$10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$ $10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ 14×4	$11 \times 3\frac{1}{2} \times \cdot 60$ $11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ 14×4	$ \begin{array}{c} 11\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60 \\ 11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 15 \times 4 \end{array} $	$ \begin{array}{ccc} 12 & \times 3\frac{1}{2} \times \cdot 60 \\ 12 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 5 \\ & 16 \times 4 \end{array} $
36 and under 38	Bulb Angle	$ \begin{array}{ccc} 11 & \times 3\frac{1}{2} \times \cdot 60 \\ 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ & 14 \times 4 \end{array} $	$11\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$ $11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ 15×4	$12 \times 3\frac{1}{2} \times \cdot 60$ $12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ 15×4	$ \begin{array}{r} 12 \times 3\frac{1}{2} \times \cdot 64 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 5 \\ 16 \times 5 \end{array} $
38 and under 40	Bulb Angle	$11\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$ $11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$ 14×4	$ \begin{array}{rrr} 12 & \times 3\frac{1}{2} \times \cdot 60 \\ 12 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ & 15 \times 4 \end{array} $	$ \begin{array}{ccc} 12 & \times 3\frac{1}{2} \times \cdot 64 \\ 12 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 54 \\ & 16 \times 4 \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
40 and under 42	Bulb Angle	$\begin{array}{c} 12 \times 3\frac{1}{2} \times \cdot 60 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 15 \times 4 \end{array}$	$ \begin{array}{r} 12 \times 3\frac{1}{2} \times \cdot 64 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 54 \\ 15 \times 4 \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12 × 4 × 4 × ·60 16 × 5
42 and under 44	Bulb Angle	$ \begin{array}{r} 12 \times 3\frac{1}{2} \times \cdot 60 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 15 \times 4 \end{array} $	$ \begin{array}{r} 12 \times 3\frac{1}{2} \times \cdot 66 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56 \\ 16 \times 4 \end{array} $	12 × 4 × 4 × ·56 16 × 4	tracept out on total of all tenders of quie out to out office only begans away.
44 and under 46	Bulb Angle	$\begin{array}{c} 12 \times 3\frac{1}{2} \times \cdot 66 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56 \\ 15 \times 4 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	to be distributed as the control of	and our definition to the second of the second of the second of the second of the second out of the se
46 and under 48	Channel	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	demonstration of the second section of the sectio	named out the one of passing	yilanlarih sa yant il sanad

VERTICAL STIFFENING for WATERTIGHT BULKHEADS.

(Concluded.)

DEPTH OF BULK- HEAD AT MIDDLE	TOS RETRY NO RESOLUT NO	DEPTH AT CENTRE	FROM LOWEST DECK TO	TOP OF FLOORS OR INNER	BOTTOM PLATING.
LINE FROM UPPER DECK TO TOP OF FLOORS OR DOUBLE		Feet.	Feet.	Feet.	Feet.
воттом.	THE PERSON NAMED IN	23 and under 24	24 and under 25	25 and under 26	26 and under 27
Feet.		Inches.	Inches.	Inches,	Inches.
22 and under 24	Bulb Angle				
24 and under 26	Bulb Angle	01-5 8× 0×	$ \begin{array}{ccc} 10 & \times 3\frac{1}{2} \times \cdot 54 \\ 9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \\ 13 \times 4 \end{array} $	$10\frac{1}{2} \times 3\frac{1}{2} \times \cdot 56$ $10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 14×4	100 SE 100 DE
26 and under 28	Bulb Angle				$11 \times 3\frac{1}{2} \times \cdot 58$ $11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$ 15×4
28 and under 30	Bulb Angle	$\begin{array}{ccc} 11 & \times 3\frac{1}{2} \times \cdot 60 \\ 11 & \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ & 15 \times 4 \end{array},$	0) X 8 X 8 X 8		
30 and under 32	Bulb Angle		$ \begin{array}{c} 12 \times 3\frac{1}{2} \times \cdot 60 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \\ 16 \times 4 \end{array} $	$12 \times 3\frac{1}{2} \times \cdot 64$ $12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 54$ 16×4	
32 and under 34	Bulb Angle	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$ \begin{array}{c} 12 \times 3\frac{1}{2} \times \cdot 64 \\ 12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 54 \\ 16 \times 4 \end{array} $	$12 \times 4 \times 4 \times \cdot 54$ 16×5	$12 \times 4 \times 4 \times \cdot 60$ 16×5
34 and 36	Bulb Angle	-	$12 \times 4 \times 4 \times 54$ 16×5	$12 \times 4 \times 4 \times \cdot 60$ 16×5	$12 \times 4 \times 4 \times \cdot 70$ 16×6
36 and 38	Channel		$12 \times 4 \times 4 \times \cdot 60$ 16×5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
38 and under 40	Channel		T. Jan X Er y Jan		

Bracket plates or other efficient attachments are to be fitted at the heads and heels of all vertical stiffeners, except in the upper 'tween decks. For stiffeners in upper 'tween decks see small Table *

Where the stiffeners are stopped at a wood deck the beam spaces adjacent to the bulkhead are to be plated over to form an efficient semi-box beam, to which the brackets on the stiffeners are to be attached.

In Small Vessels where it may be desired to fit stiffeners without brackets, the stiffeners are to be increased in size beyond the dimensions given in the Table.

The stiffeners are to be spaced 30 inches apart, centre to centre, except on the collision bulkhead.

On the Collision Bulkhead the vertical stiffeners are to be spaced 24 inches apart, and horizontal stiffeners of bulb angle, one inch deeper than required for bulb angle frames in peaks, are to be fitted on the opposite side of the bulkhead, spaced 4 feet apart, and attached to the sides of the ship by efficient brackets.

Where flanged plate stiffeners are 12 inches or more in depth, horizontal tie bars with intercostal plates spaced not more than 10 feet apart are to be fitted as shown in sketches on pages 127 and 129. The tie bars to be of the dimensions required for side stringer angles and the intercostal plates of the same thickness as the bulkhead plating.

The Bulkhead Plating is to maintain the thickness required by the Table, at floor or tank top from the bottom of the bulkhead to one-half the height to the lowest laid deck, from whence it may be gradually reduced to the thickness required at upper deck, but in vessels having 'tween decks the thickness of the plating in the upper 'tween decks need not exceed '26 of an inch, in the second 'tween decks '30 of an inch, and in the third 'tween decks '34 of an inch.

* VERTICAL STIFFENERS TO WATERTIGHT BULKHEADS IN UPPER 'TWEEN DECKS.

	HEIGHT OF TWEEN DECKS.						
	Feet. Under 8	Feet. 8 and 9	Feet. 9 and under 10	Feet. 10 and under 11			
ANGLE.	Inches. $3\frac{1}{2} \times 3 \times \cdot 30$	Inches. 4 × 3 × ·34	Inches. $4\frac{1}{2} \times 3 \times \cdot 34$	Inches $5 \times 3 \times \cdot 34$			
FLANGED PLATE.	4	5	$5\frac{1}{2}$	$6\frac{1}{2}$			

BEAMS fitted TO EVERY FRAME, with a Steel or Iron Deck.

TABLE 11. (See Continuation.)

LENGTH	FOR S	or printed order .	IS FITTED;	A 100	BEAMS AT UPPER DECKS IN STEAMERS WHERE MORE THAN ONE TIER OF BEAMS ARE FITTED, AT AWNING OR SHELTER DECKS AND AT FORECASTLE DECKS, AND DECKS OF THE ORDER OF THE						
		See also Sec. 4			BRIDGE DECKS	BRIDGE DECKS EXCEEDING ONE-TENTH THE VESSEL'S LENGT AND POOP DECKS COVERING ENGINE AND BOILER OPENINGS ?					
OF BEAM AMIDSHIPS.		EAMS AMIDSHIPS. s at ends see Footnote		Beam Knees fore and aft.		BEAMS AMIDSHIPS. as at ends see Footnote		Beam Knees fore and aft.			
- '	With one row of Pillars.	With two rows of Pillars.	With three rows of Pillars.	See also Sec. 20, Pars. 10 & 11.	With one row of Pillars.	With two rows of Pillars.	With three rows of Pillars,	See Sec. 20, Par. 10.			
16 and under 18	$3\frac{1}{2} \times 2\frac{1}{2} \times 30$	$3\frac{1}{2} \times 2\frac{1}{2} \times 30$	$\overset{\text{ins. ins. ins.}}{3} \times 2\frac{1}{2} \times 30$	11×30	Angles. ins. ins. ins.	Angles. ins. ins. ins.	Angles. ins. ins. ins.	ins. ins.			
18 and under 20			$3 \times 2\frac{1}{2} \times 30$								
			$3\frac{1}{2} \times 2\frac{1}{2} \times 30$								
CILL CO.	<i>H</i>		$\frac{4 \times 2\frac{1}{2} \times 30}{4 \times 20}$		41 9 90	4 9 90	-01 01 00	11 . 00			
					~		$3\frac{1}{2} \times 2\frac{1}{2} \times 30$				
under			-			$\frac{4\times3\times30}{41\times2\times20}$					
	Bulb Angles.		$\frac{5 \times 3 \times 30}{5 \times 3 \times 34}$			$\frac{4\frac{1}{2} \times 3 \times 30}{5 \times 3 \times 30}$	$\begin{array}{c c} 4 \times 2\frac{1}{2} \times 30 \\ \hline 4 \times 2\frac{1}{2} \times 30 \end{array}$				
		Bulb Angles.	$\frac{5 \times 3 \times 34}{5\frac{1}{2} \times 3 \times 34}$				$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				
					Rulb Angles	$5\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 30$				
			$5\frac{1}{2} \times 3 \times 34$				5 ×3 × ·30	15×·40			
38 and 40	$7\frac{1}{2} \times 3 \times 42$	$6\frac{1}{2} \times 3 \times 42$	$5\frac{1}{2} \times 3 \times 40$	22×·42	$6\frac{1}{2} \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 34$	$5\frac{1}{2} \times 3 \times 30$	16×·40			
40 and 42	$8 \times 3 \times 46$	$7 \times 3 \times 42$	$6 \times 3 \times 40$	$23 \times \cdot 46$	$7 \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 34$	$17 \times \cdot 40$			
42 and under 44	$8\frac{1}{2} \times 3 \times 46$	$7\frac{1}{2} \times 3 \times 42$	$6\frac{1}{2} \times 3 \times 40$	24×50	$7\frac{1}{2} \times 3 \times 42$	$6 \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 40$ Bulb Angles.	18×·40			
44 and 46			$7 \times 3 \times 40$			$6\frac{1}{2} \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 34$				
46 and 48		$8\frac{1}{2} \times 3 \times 46$	$7 \times 3 \times 44$	$25 \times .50$		$7 \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 40$	$20 \times \cdot 40$			
48 and under 50		$8\frac{1}{2} \times 3 \times 50$	$7\frac{1}{2} \times 3 \times 44$	$27 \times .50$		$7 \times 3 \times 42$	$6 \times 3 \times 40$	21 × ·42			
50 and under 52			$8 \times 3 \times 44$	$28 \times .50$		$7\frac{1}{2} \times 3 \times 42$	$6\frac{1}{2} \times 3 \times 40$	22× ·42			
52 and 54						$8 \times 3 \times 42$	$7 \times 3 \times 40$	$23 \times \cdot 42$			
54 and 56						$8 \times 3 \times 46$					
56 and under 58							$7\frac{1}{2} \times 3 \times 42$				
58 and do						$8\frac{1}{2} \times 3\frac{1}{2} \times 48$	$8 \times 3 \times 42$				
60 and 62							8 ×3 ×·46				
62 and 64							$8\frac{1}{2} \times 3 \times 46$				
64 and 66							$8\frac{1}{2} \times 3\frac{1}{2} \times 48$				
66 and 68							$9 \times 3\frac{1}{2} \times 48$				
68 and 70							$9 \times 3\frac{1}{2} \times 50$				
70 and 72 72 and 74							$9\frac{1}{2} \times 3\frac{1}{2} \times 50$				
72 and vinder 74 74 and vinder 76							$\begin{array}{c} 9\frac{1}{2} \times 3\frac{1}{2} \times 54 \\ \hline 10 \times 3\frac{1}{2} \times 54 \end{array}$				
76 and 78							$\frac{10 \times 3\frac{1}{2} \times 54}{10 \times 3\frac{1}{2} \times 58}$				
78 and noder 80							$\frac{10 \times 3\frac{1}{2} \times 36}{10\frac{1}{2} \times 3\frac{1}{2} \times 58}$				

⁽a) In sailing vessels where the length of the midship beam is less than 30 feet, the upper and lower deck beams are to be ½ inch deeper than given in the Table for upper deck beams of the same length, and where the length is 30 feet and above, the upper, lower and orlop deck beams are to be 1 inch deeper than given in the Table for upper deck beams of the same length.

⁽b) The beams at the ends of hatchways may be of the same size as the remainder of the beams, provided they be supported at the hatch corners by pillars or girders.

^{* *} Where the height between decks exceeds 8 feet 6 inches the size of beams is to be increased.

BEAMS fitted TO EVERY FRAME, with a Steel or Iron Deck.

TABLE 11.

LENGTH		BEAMS (IN STEAM EXCLUSIVELY FOR PASSENGERS.	THE ACCOMMODATI				SS THAN ONE-TENTE DECKS NOT COVER ER OPENINGS.	
OF BEAM		BEAMS AMIDSHIPS. (Beam Knees	1	2	3	Beam Knees
AMIDSHIPS.	1 With one row of Pillars.	ms at ends see Footnote, 2 With two rows of Pillars.	3 With three rows of Pillars.	fore and aft. See Sec. 20, Par. 10.	With one row of Pillars.	With two rows of Pillars.	With three rows of Pillars.	fore and aft See Sec. 20, Par. 10.
16 and under 18	Angles. ins. ins. ins.	Angles. ins. ins. ins.	Angles, ins. ins.	ins.	Angles. ins. ins. ins.	Angles. ins. ins. ins.	Angles. ins. ins. ins.	ins. ins.
18 and 20						11.00	0 × 6 1 00 1	97
20 and 22								
22 and under 24					$3 \times 2\frac{1}{2} \times \cdot 28$	$3 \times 2\frac{1}{2} \times 28$	$3 \times 2\frac{1}{2} \times 24$	8×·28
24 and 26	$5\frac{1}{2} \times 3 \times 30$	$5 \times 3 \times 30$	$4 \times 2\frac{1}{2} \times 30$	13×·30		$3\frac{1}{2} \times 2\frac{1}{2} \times \cdot 28$	$3 \times 2\frac{1}{2} \times 26$	
26 and under 28	$5\frac{1}{2} \times 3 \times 34$	$5 \times 3 \times 30$				$3\frac{1}{2} \times 2\frac{1}{2} \times 30$	$3 \times 2\frac{1}{2} \times \cdot 28$	
28 and under 30	$5\frac{1}{2} \times 3 \times 40$	$5 \times 3 \times 34$			$4 \times 2\frac{1}{2} \times 30$		$3 \times 2\frac{1}{2} \times 30$	
30 and under 32	$5\frac{1}{2} \times 3 \times 34$	$5\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 30$	14×·34	$4 \times 3 \times 30$	$4 \times 2\frac{1}{2} \times 30$	$3\frac{1}{2} \times 2\frac{1}{2} \times 30$	11×·30
32 and mnder 34	$5\frac{1}{2} \times 3 \times 36$	$5\frac{1}{2} \times 3 \times 40$	5 ×3 ×·30	$15 \times \cdot 40$	$4\frac{1}{2} \times 3 \times 30$	4 ×3 ×·30	$3\frac{1}{2} \times 2\frac{1}{2} \times 30$	11×·30
34 and under 36	$6 \times 3 \times 36$	$5\frac{1}{2} \times 3 \times 34$				$4 \times 3 \times 30$	$4 \times 2\frac{1}{2} \times 30$	12×·30
36 and under 38	$6\frac{1}{2} \times 3 \times 38$	$5\frac{1}{2} \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 34$	$17 \times .40$	$5 \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 30$	$4 \times 2\frac{1}{2} \times 30$	$12 \times \cdot 3$
$38 _{\mathrm{under}}^{\mathrm{and}} 40$	$7 \times 3 \times 40$	6 ×3 ×·40	$5\frac{1}{2} \times 3 \times 40$ Bulb Angles.	$18 \times \cdot 40$	$\frac{5\frac{1}{2}\times3\times34}{\text{Bulb Angles.}}$	$5 \times 3 \times 34$	$4 \times 3 \times 30$	13×·34
40 and under 42	$7\frac{1}{2} \times 3 \times 42$	$6\frac{1}{2} \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 34$		$5\frac{1}{2} \times 3 \times 34$		$4\frac{1}{2} \times 3 \times 30$	
42 and under 44	$8 \times 3 \times 44$	$7 \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 40$	$20 \times \cdot 40$	$5\frac{1}{2} \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 40$ Bulb Angles.	$5 \times 3 \times 30$	$15 \times \cdot 40$
44 and 46		$7 \times 3 \times 42$	$6 \times 3 \times 40$			$5\frac{1}{2} \times 3 \times 34$	$\frac{5\frac{1}{2} \times 3}{51 \times 9} \times \frac{30}{24}$	
46 and 48		$7\frac{1}{2} \times 3 \times 42$	$\frac{6\frac{1}{2} \times 3 \times 40}{7 \times 2 \times 40}$			$\frac{5\frac{1}{2}\times3\times40}{6\times2\times40}$	$\frac{5\frac{1}{2}\times3\times34}{51\times2\times40}$	
48 and under 50		8 ×3 ×·42	$7 \times 3 \times 40$			$6 \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 40$ Bulb Angles.	
50 and 52		$8 \times 3 \times 46$	$7 \times 3 \times 42$			$\frac{6\frac{1}{2}\times3\times40}{7}$	$5\frac{1}{2} \times 3 \times 34$	
52 and 54		$8\frac{1}{2} \times 3 \times 46$	$7\frac{1}{2} \times 3 \times 42$			$7 \times 3 \times 40$	$\frac{5\frac{1}{2}\times3\times40}{6\times2}$	
54 and 56		$8\frac{1}{2} \times 3\frac{1}{2} \times 48$	$8 \times 3 \times 42$			$7 \times 3 \times 42$	$6 \times 3 \times 40$	
56 and 58		$\frac{9 \times 3\frac{1}{2} \times 48}{9 \times 3\frac{1}{2} \times 50}$	8 ×3 × ·46			$7\frac{1}{2} \times 3 \times 42$	$\frac{6\frac{1}{2} \times 3 \times 40}{7 \times 3 \times 40}$	
58 and 60		$9 \times 3\frac{1}{2} \times 50$	$8\frac{1}{2} \times 3 \times 46$			8 × 3 × 42	$7 \times 3 \times 40$	
60 and 62			$8\frac{1}{2} \times 3\frac{1}{2} \times 48$				$7 \times 3 \times 42$	
62 and 64			$9 \times 3\frac{1}{2} \times 48$				$7\frac{1}{2} \times 3 \times 42$	
64 and 66			$9 \times 3\frac{1}{2} \times 50$				$\begin{array}{c} 8 \times 3 \times 42 \\ 8 \times 3 \times 46 \end{array}$	
66 and dunder 68			$\frac{9\frac{1}{2} \times 3\frac{1}{2} \times 50}{9\frac{1}{2} \times 3\frac{1}{2} \times 54}$				$\frac{8 \times 3 \times 40}{8 \times 2 \times 3 \times 46}$	
68 and ro			$\frac{9\frac{1}{2}\times 3\frac{1}{2}\times 34}{10\times 3\frac{1}{2}\times 54}$				$\frac{8\frac{1}{2} \times 3}{8\frac{1}{2} \times 3\frac{1}{2} \times 48}$	
70 and 72			$\frac{10 \times 3\frac{1}{2} \times 54}{10 \times 3\frac{1}{2} \times 58}$				$\frac{6_{\overline{2}} \times 3_{\overline{2}} \times 48}{9 \times 3_{\overline{1}} \times 48}$	
72 and 74			$\frac{10 \times 3\frac{1}{2} \times 36}{10\frac{1}{2} \times 3\frac{1}{2} \times 58}$				$\frac{9 \times 3\frac{5}{2} \times 40}{9 \times 3\frac{5}{2} \times 40}$	
74 and 76			$\frac{10\frac{1}{2} \times 3\frac{1}{2} \times 36}{10\frac{1}{2} \times 3\frac{1}{2} \times 62}$				$\frac{9\frac{1}{2}\times 3\frac{1}{2}\times 50}{9\frac{1}{2}\times 3\frac{1}{2}\times 50}$	
76 and 178			$\frac{10^{\frac{1}{2}} \times 3^{\frac{1}{2}} \times 62}{11 \times 3^{\frac{1}{2}} \times 62}$				$\frac{9\frac{1}{2} \times 3\frac{1}{2} \times 50}{9\frac{1}{2} \times 3\frac{1}{2} \times 54}$	
78 and under 80			11 X 02 X 02	30 X 02			$0\overline{2} \wedge 0\overline{2} \wedge 0\overline{4}$	00 \ 0

⁽b) The beams at the ends of hatchways may be of the same size as the remainder of the beams, provided they be supported at the hatch corners by pillars or girders.

Beams at the ends of decks below the upper deck less than two-fifths the length of the midship beam may be of the size given for upper deck beams at the ends of the vessel.

See footnotes on Table 13.

[†] The beams of decks fitted exclusively for the accommodation of passengers and of all tiers in peaks may be of the size given for upper deck beams where more than one tier of beams are fitted.

^{* *} Where the height between decks exceeds 8 feet 6 inches the size of beams is to be increased.

BEAMS fitted TO ALTERNATE FRAMES where no steel or iron deck is fitted.

TABLE 12.

(See Continuation.)

	1	11011	deck is ii	00001	1		(See Contin			
LENGTH OF		OF BEAMS IN STEA OF BEAMS ONLY SAILING VESSELS, See also Sec. 47	IS FITTED; see Footnote (a)米米	TIER	BEAMS AT UPPER DECKS IN STEAMERS WHERE MORE THAN TIER OF BEAMS ARE FITTED, AT AWNING OR SHELTER DECKS AT FORECASTLE DECKS AND BRIDGE DECKS EXCEEDING ONE-TI THE VESSEL'S LENGTH AND POOP DECKS COVERING ENGINE BOILER OPENINGS. **					
BEAM AMIDSHIPS.	1	EAMS AMIDSHIPS. (at ends, see Footnote,		Beam Knees fore and aft.	(For Beams	EAMS AMIDSHIPS. (at ends, see Footnote,	b) Table 13.)	Beam Knees		
	With one row of Pillars.	With two rows of Pillars.	With three rows of Pillars.	See Sec. 20. Par. 10.	With one row of Pillars.	2 With two rows of Pillars.	With three rows of Pillars.	See Sec. 20. Par. 10.		
16 and under 18	$\begin{array}{ c c c }\hline & \text{ins.} & \text{Angles.} \\\hline 4\frac{1}{2} \times 3 & \times 34 \\\hline \end{array}$	$\begin{array}{c} \text{ins.} & \text{Angles.} \\ 4\frac{1}{2} \times 3 & \times 30 \end{array}$	$\overset{\text{ins.}}{4} \overset{\text{ins.}}{\times} \overset{\text{ins.}}{3} \overset{\text{ins.}}{\times} 30$	12×30	Angles. ins. ins. ins.	Angles. ins. ins. ins.	Angles. ins. ins. ins.	ins. ins.		
18 and under 20	$5 \times 3 \times 34$	$5 \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 34$	13×·30				Table P.I.		
20 and under 22	$5\frac{1}{2} \times 3 \times 40$	$5\frac{1}{2} \times 3 \times 40$	$5 \times 3 \times 40$	$15 \times .30$	$5\frac{1}{2} \times 3 \times 34$	$5 \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 34$	14×·30		
22 and under 24	$5\frac{1}{2} \times 3\frac{1}{2} \times 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times 40$	$5\frac{1}{2} \times 3 \times 40$	16×30	$5\frac{1}{2} \times 3\frac{1}{2} \times 40$	$5\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 34$	14×·30		
24 and 26	Bulb Plate. 6 × 30	$6 \times 3\frac{1}{2} \times 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times 44$	18×·30	Bulb Plate. 6×26	$5\frac{1}{2} \times 3\frac{1}{2} \times 40$	5 ×3 ×·34	15×·30		
26 and under 28	6×·34	Bulb Plate. 6×26	$6\frac{1}{2} \times 3\frac{1}{2} \times 44$	19×·34	6×·30	$5\frac{1}{2} \times 3\frac{1}{2} \times 44$	$5\frac{1}{2} \times 3 \times 34$	15×·30		
28 and under 30	7×·34	6×·30	Bulb Plate. 6×26	21×·34	6 × ·34	Bulb Plate. 6×26	$5\frac{1}{2} \times 3 \times 40$	16×·34		
30 and under 32	7×40	7×·30	6 × ·30	$22 \times \cdot 40$	7×30	6×·30	$5\frac{1}{2} \times 3\frac{1}{2} \times 44$	17×·34		
32 and under 34	8 × ·40	7×34	6 × ·34	$24 \times \cdot 40$	7×34	6×·34	$6\frac{1}{2} \times 3\frac{1}{2} \times 44$	18×·34		
34 and under 36	8×·44	7×·40	7×·30	$25 \times \cdot 44$	7×·40	7×·30	Bulb Plate. 6 × 26	19×·40		
36 and and 38	9×·44	8×·40	7×·34	27×·44	8×·40	7×·34	6×·30	20×·40		
38 and 40	9×·50	8×·44	7 × ·40	$28 \times .50$	8 × ·44	$7 \times \cdot 40$	6 × ·34	21×·44		
40 and 42	10×:50	9×·44	8×·40	30×·50	9×·44	8 × ·40	7×·30	22×·44		
42 and under 44	$10 \times .54$	9×·50	8 × ·44	$31 \times .54$	10×·44	8 × ·44	7×34	23×·50		
44 and 46		10×·44	9×·44	$33 \times .54$	7 7 17 181	9×·40	7×·40	24×·50		
46 and 48	100 0 000	10×·50	9×.50	$34 \times .54$	8 x 8 x x 3	9×·44	8 × ·40	25×·54		
48 and mnder 50	-X-10 X8 X	10×·54	10×·44	$36 \times .54$	EX E	10×·44	8 × ·44	26×·54		
50 and 52			10×·50	$37 \times .54$		10×·50	9×·40	27×·54		
52 and 54			- 100 x	OR BEN	18 x 8	10×·54	9×·44	28×·54		
54 and 56					N.X.,	11×·50	9×·50	29 × ·54		
56 and 58							10×·44	30×·54		
58 and do	63.18			10.40	(8 × 01		10×·50	31×·54		
60 and 62							10×·54	32×·54		
62 and 64							11×·50	33×·54		
64 and de 66	- 10			12 SD X	(8 x 11		11×:54	34×·54		

⁽⁴⁾ In sailing vessels where the length of the midship beam is less than 30 feet, the upper and lower deck beams are to be 1 inch deeper than given in the Table for upper deck beams of the same length; and where the length is 30 feet and above, the upper, lower, and orlop deck beams are to be 1 inch deeper than given in the Tables for upper deck beams of the same length.

⁽b) Single angles fitted to hatch end beams are to be equivalent to the double angles required by the Rules.

^{* *} Where the height between decks exceeds 8 feet 6 inches, the size of beams is to be increased.

BEAMS fitted TO ALTERNATE FRAMES where no steel or

iron deck is fitted.

(Concluded.)

				iror	n deck is	nttea.				(Conci	uaea.)
LENGTH OF	UPPER DE	CKS NOT F	MS (IN STEAMERS	ELY FOR	VESSEL'S LE	DGE DECKS LESS	"STRONG" HOLD BEAMS (c)				
BEAM AMIDSHIPS.	BE. (For Beams	AMS AMIDS at ends see F	HIPS. (b) controte, Table 13.)	Beam Knees	1	2	3	Beam Knees fore and aft.		Double Angles	Beam Knees fore and aft.
	With one row of Pillars.	With two rows of Pillars.	3 With three rows of Pillars.	See Sec. 20. Par. 10.	With one row of Pillars.	Pillars.	With three rows of Pillars.	See Sec. 20. Par. 10.	Plate.	on top and bottom edges.	See Sec. 20. Par. 10.
16 and 18	ins. ins.	ins. ins.	Angles. ins. ins. ins.	ins. ins.	Angles. ins. ins. ins.	Angles. ins. ins. ins.	Angles. ins. ins. ins.	ins. ins.	ins. ins.	ins. ins. ins.	ins. ins.
$18_{ m under}^{ m and}20$											
$20_{ m under}^{ m and} 22$					1						
$22_{\mathrm{under}}^{\mathrm{and}}24$					$4\frac{1}{2} \times 3 \times 30$	$4\frac{1}{2} \times 3 \times 30$	$4 \times 3 \times 30$	$0.11 \times .30$			
$24_{ m under}^{ m and}26$	7×30	Bulb Plate. 6×30	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	17×·34	$4\frac{1}{2} \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 34$	$4 \times 3 \times 34$	11×·30	7 × ·34	$3 \times 3 \times 30$	$21 \times \cdot 40$
26 and 28	7×·34	6×·34	$6\frac{1}{2} \times 3\frac{1}{2} \times 44$	18×·34	$5 \times 3 \times 34$	$4\frac{1}{2} \times 3 \times 34$	$4 \times 3 \times 34$	12×·30	$7\frac{1}{2} \times 34$	$3 \times 3 \times 34$	122×·44
28 and 30	7×·40	7×·30	Bulb Plate. 6×26				$44\frac{1}{2} \times 3 \times 34$				
30 and 32	8×·40	$7 \times .34$	$6 \times .30$				$44\frac{1}{2} \times 3 \times 34$				
32 and 34	8×·44	$7 \times \cdot 40$	6×34	$21 \times \cdot 44$	$5\frac{1}{2} \times 3\frac{1}{2} \times 44$	$5\frac{1}{2} \times 3 \times 40$	$5 \times 3 \times 34$	$414 \times \cdot 30$	9×44	$4 \times 4 \times 34$	$125 \times .50$
$34_{ m under}^{ m and}36$	9×·44	8 × ·40	7×·30	22×·44	Bulb Plate. 6 × 30	$5\frac{1}{2} \times 3\frac{1}{2} \times 4$	$45\frac{1}{2} \times 3 \times 34$	415×·30	$9\frac{1}{2} \times \cdot 44$	$4 \times 4 \times 4$	$26 \times .50$
36 and 38	10×·44	8 × ·44	7×:34	23×·50	6 × ·34	Bulb Plate. 6×26	_			$4 \times 4 \times 4$	
$38_{\mathrm{under}}^{\mathrm{and}}40$	$10 \times .50$	9×·40	$7 \times \cdot 40$	$24 \times .50$	7×34	6×34	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 4$	418×34	110×54	$4 \times 4 \times 4$	$428 \times .54$
$40_{ m under}^{ m and} 42$	10×·54	9 × ·44	8 × ·40	$25 \times .54$	$7 \times \cdot 40$	7×·30	Bulb Plate. 6×26			$4 \times 4 \times 4$	
42 and 44	$11 \times .54$	$10 \times \cdot 44$	8 × ·44	$26 \times .54$	8×40	$7 \times .34$	$6 \times .30$		1	$45 \times 4 \times 4$	
44 and 46		10×·50	9 × ·40	$27 \times .54$	1	$7 \times \cdot 40$	6×34			$45 \times 4 \times 4$	_
$\overline{46_{\mathrm{under}}^{\mathrm{and}}48}$	3	10×·54	9 × ·44	28 × ·54	1	$8 \times \cdot 40$	$7 \times .30$			$05 \times 4 \times 4$	
48 and 50		11×·50	$9 \times .20$	$29 \times .54$	1	8 × ·44	7×34			$06 \times 4 \times 5$	
50 and 52		11×·54	4 10×·44	$30 \times .54$	1	9 × ·40	$7 \times .40$		1	$06 \times 4 \times 5$	
52 and 54	-	12×·50	0 10×·50	31×·5	1	9×·44	8 × ·40			$0 \frac{6\frac{1}{2} \times 4 \times 5}{}$	
$54_{ m under}^{ m and}56$	-	12×:54	4 10×·54	32×·5	4	$9 \times .50$	8 × ·44			$0 6\frac{1}{2} \times 4\frac{1}{2} \times 5$	
56 and 58	-		11×·50	33×·5	4		9×·40			$0 \underline{6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 5}$	
58 and 60			11×·54	34×·5	4		9×·44		1	$06\frac{1}{2} \times 4\frac{1}{2} \times 5$	
60 and 62			12×·50	$35 \times .5$	4		9×·50			$0 6\frac{1}{2} \times 4\frac{1}{2} \times 5$	
62 and 64	_		12×·54	36×5	4		10×·44			$46\frac{1}{2} \times 4\frac{1}{2} \times 6$	
64 and 6			12×·60	37×·6	0		10×·50	31 × ·5	415×6	$46\frac{1}{2} \times 4\frac{1}{2} \times 6$	$30 42\times \cdot 6$

The beams of decks fitted exclusively for the accommodation of passengers and of all tiers in peaks may be of the size given for upper deck beams where more than one tier of beams are fitted.

Beams at the ends of decks below the upper deck, less than two-fifths the length of the midship beam, may be of the size given for upper deck beams at the ends of the vessel.

^{**} Where the height between decks exceeds 8 feet 6 inches the size of beams is to be increased.

⁽b) Single angles fitted to hatch end beams are to be equivalent to the double angles required by the Rules.

⁽c) These beams are to be formed of a plate with double angle bars on the upper and lower edges. The beam plates and angle bars are to be of the sizes given above, and the broad flanges of the angle bars are to be fitted horizontally. Semi-box beams may be adopted in lieu thereof, formed of bulb plate and single angle bars of the sizes given for upper deck beams, kneed to two consecutive frames with a covering plate of the thickness of the angles.

Strong beams in the machinery space are to have double angles on their upper and lower edges, unless cross tie plating is fitted on them, in which case only single angles need be fitted to the upper and lower edges.

WIDELY SPACED PILLARS.

(For 26 feet and above, see continuation.)

		SAMIN SO MAD	LENG	TH AND F	ORM OF	PILLAR.		
NUMBERS.*	the last o	22 feet and under	r 24 fee	et.	mhmi h	24 feet and under	er 26 fe	et.
$S \times B \times H$	TUBULAR.	DOUBLE CHANNELS FACE PLATES.	AND	FOUR ANGLES.	TUBULAR.	DOUBLE CHANNELS FACE PLATES	AND	FOUR ANGLES.
100	0	I			OI			+
	Outside diameter.	, Channels.	Plates.		Outside diameter.	Channels.	Plates.	
11 and 19	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.
11 and 13	$9 \times \cdot 40$			$5 \times 5 \times \cdot 44$		9 ×4 ×4 × ·66		$5 \times 5 \times .50$
13 and 16	9×44					$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$		
16 and under 19	$10 \times \cdot 40$					$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$		
19 and under 22	10×40					$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$		
22 and under 25	10×44	$8\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$						
25 and under 29	$10 \times .50$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	$10 \times \cdot 40$	$5 \times 5 \times 60$	$10 \times .50$	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	10×42	$6 \times 6 \times .50$
29 and under 33	11×·50	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$10 \times \cdot 42$	$6 \times 6 \times 50$	$11 \times .50$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$311 \times \cdot 42$	$6 \times 6 \times .54$
33 and under 37	12×50	$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$11 \times \cdot 42$	$6 \times 6 \times 54$	$12 \times .50$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$311 \times \cdot 46$	$6 \times 6 \times .00$
37 and 42	12×·54	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$11 \times \cdot 46$	$6 \times 6 \times 60$	12×·54	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	3 11×·50	$6 \times 6 \times .60$
42 and 47	13×·54	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	12×·50	$6 \times 6 \times \cdot 64$	$13 \times .54$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	12×·50	$6 \times 6 \times \cdot 64$
47 and under 52	13×·60	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	12× 56	$6 \times 6 \times .70$	13×·60	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	12×·56	$6 \times 6 \times .70$
52 and under 58	14×·60	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	12×·60	$7 \times 7 \times \cdot 60$	14×·60	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	12×·60	$7 \times 7 \times \cdot 60$
58 and dunder 64	$15 \times \cdot 60$	$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	13×·60	$7 \times 7 \times \cdot 64$	15×·60	$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	13×·60	$7 \times 7 \times \cdot 64$
64 and under 71	16×·60	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	13×·70	$7 \times 7 \times .70$	16×·60	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	13×·70	$7 \times 7 \times \cdot 70$
71 and 78	17×·60	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	13×·74	$7 \times 7 \times .74$	17×·60	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	13×·74	7×7×·74
78 and 86	_	$12 \times 4 \times 4 \times \cdot 60$						
86 and under 94	18×·64	$12 \times 4 \times 4 \times \cdot 70$	13×·74	$7 \times 7 \times \cdot 84$	18×·64	$12 \times 4 \times 4 \times \cdot 70$	$13 \times .74$	$7 \times 7 \times \cdot 84$
94 and 102		$12 \times 4 \times 4 \times \cdot 72$						
102 and under 110	18×·74			$8 \times 8 \times \cdot 84$				
110 and 118								
118 and 126								100 0011
126 and under 134					1			
under 101								

- 1. * S is the fore and aft distance in feet from centre of span to centre of span.
 - B is one-third the breadth of vessel in feet at the deck at the head of the pillars, where two rows of pillars are fitted, and one-fourth the breadth where three rows are fitted.
 - H is the sum of the heights of the several 'tween decks in feet from top of beam to top of beam above the pillars with an addition of 5 feet for the upper, awning or shelter deck, bridge, poop or forecastle deck.

In the case of a deck fitted exclusively for the accommodation of passengers, the height of 'tween decks may be taken as being 5 feet.

- 2. For methods of obtaining the numbers regulating the size of the pillars, see Sketches on pages 134 to 137.
- 3. The rivets in the angles or channels forming pillars are to be spaced not more than 7 diameters apart centre to centre, and when the flanges are inches in width or above, zigzag riveting is to be adopted.
 - 4 The rivets in the seams of built tubular pillars are to be spaced not more than 5 diameters apart.
 - 5. Pillars of other form will be admitted provided they are of equivalent strength to those given in the Table.
- 6. Where no seating is fitted, widely spaced hold pillars are to be steppped where practicable at an intersection of floors and intercostals; but in cases where this cannot be done, intercostal brackets are to be fitted on each side of the floors beneath the pillars.
 - For some methods of attaching the pillars at heads and heels see Sketches on pages 132 and 133.

WIDELY SPACED PILLARS.

			LENG'	TH AND FO	ORM OF	PILLAR.		
		26 feet and under	28 fee	et.		28 feet and und	er 30 fe	eet.
NUMBERS. * $S \times B \times H$ 100	TUBULAR.	DOUBLE CHANNELS FACE PLATES.	AND	FOUR ANGLES.	TUBULAR.	DOUBLE CHANNELS		FOUR ANGLES
100	0	I		+	0	I		+
	Outside diameter.	Channels.	Plates.		Outside diameter.	Channels	Plates.	
11 and 13	inches. $10 \times .44$	9 $\times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$10 \times \cdot 40$	$5 \times 5 \times 54$	$10 \times .50$	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	inches. $10 \times \cdot 42$	inches. $6 \times 6 \times 5$
13 and 16	10×·44	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	$10 \times \cdot 40$	$5 \times 5 \times 54$	10×·50	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 48$	3 11×·40	$6 \times 6 \times 5$
16 and 19	10×·50	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	10×·40	$5 \times 5 \times .60$	11×·44	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	3 11×·42	$6 \times 6 \times 5$
19 and 22	10×·50	$9\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	11×·40	$6 \times 6 \times .50$	$11 \times \cdot 44$	$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	3 11×·42	$6 \times 6 \times 5$
22 and 25	11×·44	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	11×·42	$6 \times 6 \times 54$	$11 \times .50$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	3 11×·46	$6 \times 6 \times .6$
25 and under 29	11×·50	$10\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	11×·46	$6 \times 6 \times 54$	$11 \times .50$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$11 \times \cdot 46$	$6 \times 6 \times .6$
29 and under 33	12×·50	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$11 \times \cdot 46$	$6 \times 6 \times .60$	$12 \times .50$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$12 \times .50$	$6 \times 6 \times .6$
33 and 37	12×·50	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$11 \times \cdot 46$	$6 \times 6 \times .60$	12×54	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$12 \times .50$	$6 \times 6 \times .6$
37 and under 42	12×·54	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$12 \times .50$	$6 \times 6 \times \cdot 64$	13×54	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$12 \times .56$	$6 \times 6 \times .7$
42 and 47	13×54	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	$12 \times .56$	$6 \times 6 \times .70$	$13 \times .60$	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$	$12 \times .60$	$7 \times 7 \times .6$
47 and under 52		$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$			1			
52 and under 58		$11\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$						
58 and ander 64		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$						
64 and under 71		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 50$						
71 and under 78	$17 \times .60$	$12 \times 4 \times 4 \times \cdot 60$	$13 \times .74$	$7 \times 7 \times .80$	$18 \times .60$	$12 \times 4 \times 4 \times \cdot 70$	$13 \times .74$	$8 \times 8 \times .7$
78 and 86	18×·60					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	OSSET-	
86 and 94							0641	
94 and 102						1.34		
102 and under 110							Oh L	
110 and under 118							18331	
118 and 126							0.00	
126 and under 134								

- 1. * S is the fore and aft distance in feet from centre of span to centre of span.
 - B is one-third the breadth of vessel in feet at the deck at the head of the pillars, where two rows of pillars are fitted, and one-fourth the breadth where three rows are fitted.
 - H is the sum of the heights of the several 'tween decks in feet from top of beam to top of beam above the pillars with an addition of 5 feet for the upper, awning or shelter deck, bridge, poop or forecastle deck.
 - In the case of a deck fitted exclusively for the accommodation of passengers, the height of 'tween decks may be taken as being 5 feet.
- 2. For methods of obtaining the numbers regulating the size of the pillars, see Sketches on pages 134 to 137.
- 3. The rivets in the angles or channels forming pillars are to be spaced not more than 7 diameters apart centre to centre, and when the flanges are 5 inches in width or above, zigzag riveting is to be adopted.
 - 4. The rivets in the seams of built tubular pillars are to be spaced not more than 5 diameters apart.
 - 5. Pillars of other form will be admitted provided they are of equivalent strength to those given in the Table.
- 6. Where no seating is fitted, widely spaced hold pillars are to be stepped where practicable at an intersection of floors and intercostals; but in cases where this cannot be done, intercostal brackets are to be fitted on each side of the floors beneath the pillars.
 - 7. For some methods of attaching the pillars at heads and heels, see Sketches on pages 132 and 133.

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON, E.C.—17th June, 1909.

GIRDERS AT HEADS OF WIDELY SPACED PILLARS.

(See Continuation.

	ostal	RAMES NO RECOVER	DEPTH O	F BEAMS.							
NUMBERS.*	Thickness of Interostal Plate and Angle.	5 inche	5 inches. 6 inches.								
$\frac{S^2 \times B \times H}{100}$	ate and	THE STATE OF THE S	SIZE OF	GIRDERS.	4 - 4 - 4						
	Thickr	Double Channels.	Double Angles.	Double Channels.	Double Angles.						
150 and 180	.34	inches.	6 ×4 × ·44	inches.	$6 \times 4 \times 40$						
180 and under 210	·34		6 ×4 ×·50		6 ×4 ×·44						
210 and under 250	·34	7 ×3 ×3 ×·38	6 ×4 × ·54		6 ×4 ×·50						
250 and under 290	•40	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 40$	6 ×4 × ·64	7 ×3 ×3 ×·38	6 ×4 ×·54						
290 and under 330	`40	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 42$	$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60$	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 40$	6 ×4 ×·64						
330 and under 380	40	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 64$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 42$	$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60$						
380 and 430	•40	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	6 × 6 × · 64	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 64$						
430 and under 480	•44	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60.$	$6 \times 6 \times 74$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	6 × 6 × · 64						
480 and under 540	•44	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	7 ×7 ×·70	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	$6 \times 6 \times .74$						
540 and 600.	•44	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	7 ×7 ×·80	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	7 ×7 ×·70						
600 and under 670	•44			$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	7 ×7 ×·80						
670 and 140	•44			$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$							
740 and under 820	.50										
820 and under 900	.50	Ax. STORY SILEE XT									
900 and under 990	.50				- Barrier - Barr						
990 and 1090	:50										
1090 and under 1200	.50	Example of the same									
1200 and under 1320	.50										
1320 and under 1450	.50										
1450 and 1590	.54										
1590 and 1740	.54				011 301						
1740 and under 1900	.54										
1900 and 2070	.54				101 33 811						

1.* S is the fore and aft spacing of the pillars in feet from centre to centre.

B is one-third the breadth of vessel in feet at the deck when two rows of pillars are fitted, and one-fourth the breadth when three rows are fitted.

H is the height of the 'tween decks next above the girder, measured in feet from top of beam to top of beam, where the pillars in the 'tween decks are spaced the same as those below. In the case of decks fitted exclusively for the accommodation of passengers, and for upper, awning or shelter, bridge, poop or forecastle deck, H is to be taken as 5. feet.

Where the pillars above a deck are not placed over those below, H is to be the sum of the heights of the several 'tween decks in feet above the girder, with the addition of 5 feet for upper, awning or shelter deck, bridge, poop or forecastle deck.

2. For methods of obtaining the numbers regulating the scantlings for girders, see Sketches on pages 138 to 141.

3. The girders are to consist of double channels or double angles, intercostal plate and rider plate, of the scantlings given in the Table. (See Sketches on pages 132 and 133.)

4. The intercostal plates and channels or angles are to be fitted in long lengths and efficiently strapped or lapped at the butts to the Surveyor's satisfaction. 5. The channels are to be attached by two rivets to the lower flanges of the beams, or, in the case of angle or bulb angle beams to short angle lugs fitted to the beams, and where double angles are fitted in lieu of channels the intercostal plates are to be attached to the beams by angle lugs extending to the bottom of the girder and beams alternately where beams are fitted at every frame and to the bottom of the girder at every beam where beams are fitted at alternate frames. (See Sketch on page 133.)

6. The girders are to be efficiently bracketed to the bulkheads with plates three times the depth of the channels forming girders, measured from the upper edges of the channels and of the same thickness as the channels. The angle attaching the intercostal plate to the deck plating and intercostal plates to beams is to be of the same thickness as the plate, this angle is to be 3 ins. × 3 ins. where the rivets in the intercostal plates are required to be \(\frac{3}{4} \) in. in diameter, and \(3\frac{1}{2} \) ins. where they are \(\frac{1}{3} \) ins. where \(\frac{1}{3} \) ins. those in the flanges of the intercostal angle not more than 5 diameters apart, centre to centre.

7. Girders of other form will be admitted provided they are of equivalent strength to those given in the Table.

(See Continuation.)

	ostal	THE ASSET OF		DEPTH	OF BEAMS.		
NUMBERS. *	Interco	7	inches.		8	inches.	
$\frac{S^2 \times B \times H}{100}$	Thickness of Intercostal Plate and Angle.		10 (9118	SIZE C	OF GIRDERS.		HXBX8
	Thicki	Double Channels.	Rider Plate.	Double Angles.	Double Channels.	Rider Plate.	Double Angles.
150 and 180	·34	inches.	inches.	inches.	inches.	inches.	inches.
180 and 210	·34			$6 \times 4 \times \cdot 40$			110 - 50 1029
210 and 250	•34			$6 \times 4 \times 44$		-18	$6 \times 4 \times 4$
250 and 290	•40		Tones	6 ×4 ×·50		01-	6 ×4 ×·4
290 and 330	•40	7 ×3 ×3 ×·38	THE	$6 \times 4 \times 54$		01/2	6 ×4 × ·5
330 and under 380	•40	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 40$	Turk	$6 \times 4 \times 64$	$7 \times 3 \times 3 \times 38$		6 ×4 ×·5
380 and 430	•40	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 42$	11800	$6\frac{1}{2} \times 4\frac{1}{2} \times 60$	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	101	6 ×4 × ·6
430 and 480	•44	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	110	$6\frac{1}{2} \times 4\frac{1}{2} \times 64$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 42$		$6\frac{1}{2} \times 4\frac{1}{2} \times 6$
480 and 100 moder 100 mode	•44	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	Tony	$6 \times 6 \times 64$	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6\frac{1}{2} \times 4\frac{1}{2} \times 6$
540 and 600	•44	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	Taboxi	$6 \times 6 \times 74$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$	144-1	6 × 6 × · 6
600 and under 670	•44	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	Table 14	$7 \times 7 \times .70$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	100	6 × 6 × · 7
670 and mider 740	•44	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	I I Y X	7 × 7 × ·80	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		7 ×7 × ·7
740 and under 820	.50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	107-x		$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	100	7 ×7 × ·8
820 and under 900	.50	$12 \times 4 \times 4 \times \cdot 64$	1 08°×		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		
900 and under 990	.50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	8×·60		$12 \times 4 \times 4 \times 64$	06-1-	
990 and 1090	.50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 70$	8×·70		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	8×.60	1001 1000
1090 and 1200	.50			00 × 8	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 70$	8×·70	
1200 and under 1320	.50				$12 \times 4 \times 4 \times \cdot 70$	9×·70	KEL EE OOK
1320 and 1450	.50			05.20	$12 \times 4 \times 4 \times \cdot 72$	10×·74	PH 45 001
1450 and 1590	•54			- 17 × 0			TOTAL DESIGNATION OF THE PARTY
1590 and 1740	•54						EXELECTION ORG
1740 and under 1900	•54						1001 120 010
1900 and 2070	•54						KOR Je ono

Where the pillars above a deck are not placed over those below, H is to be the sum of the heights of the several 'tween decks in feet above the girder, with the addition of 5 feet for upper, awning or shelter deck, bridge, poop or forecastle deck.

2. For methods of obtaining the numbers regulating the scantlings for girders, see Sketches on pages 138 to 141.

4. The intercostal plates and channels or angles are to be fitted in long lengths and efficiently strapped or lapped at the butts to the Surveyor's satisfaction.

5. The channels are to be attached by two rivets to the lower flanges of the beams, or in the case of angle or bulb angle beams to short angle lugs fitted to the beams, and where double angles are fitted in lieu of channels the intercostal plates are to be attached to the beams by angle lugs extending to the bottom of the girder and beams alternately where beams are fitted at every frame and to the bottom of the girder at every beam where beams are fitted at alternate frames. (See Sketch on page 133.)

6. The girders are to be efficiently bracketed to the bulkheads with plates three times the depth of the channels forming girders, measured from the upper edges of the channels and of the same thickness as the channels. The angle attaching the intercostal plate to the deck plating and intercostal plates to beams is to be of the same thickness as the plate, this angle is to be 3 ins. \times 3 ins. where the rivets in the intercostal plates are required to be $\frac{3}{4}$ in. in diameter, and $3\frac{1}{2}$ ins. \times $3\frac{1}{2}$ ins. where they are $\frac{7}{8}$ in diameter. The channels and double angles to be zigzag riveted and the rivets spaced not more than 7 diameters apart, and those in the flanges of the intercostal angle not more than 5 diameters apart, centre to centre.

7. Girders of other form will be admitted provided they are of equivalent strength to those given in the Table.

^{1.*} S is the fore and aft spacing of the pillars in feet from centre to centre.

B is one-third the breadth of vessel in feet at the deck when two rows of pillars are fitted, and one-fourth the breadth when three rows are fitted.

H is the height of the 'tween decks next above the girder, measured in feet from top of beam to top of beam, where the pillars in the 'tween decks are spaced the same as those below. In the case of decks fitted exclusively for the accommodation of passengers, and for upper, awning or shelter, bridge, poop or forecastle deck, H is to be taken as 5 feet.

^{3.} The girders are to consist of double channels or double angles, intercostal plate and rider plate, of the scantlings given in the Table. (See Sketches on pages 132 and 133.)

GIRDERS AT HEADS OF WIDELY SPACED PILLARS.

(See Continuation.)

	stal	SEASE S	0 113431	DEPTH	OF BEAMS.		
NUMBERS. *	Thickness of Intercostal Plate and Angle.	9	inches.	relies	1	0 inches.	* 2221207
$\frac{S^2 \times B \times H}{100}$	ate and	олионо	to axis	SIZE O	F GIRDERS.		73 - 2 - 2 - 6
	Thicky	Double Channels.	Rider Plate.	Double Angles.	Double Channels.	Rider Plate.	Double Angles.
150 and 180	·34	inches.	inches.	inches.	inches.	inches.	inches.
180 and 210	•34	· ·	THE	Tex del se del			1124.122.001
210 and under 250	•34		THE X	Text (the part of the part of			
250 and under 290	•40		THE X	6 ×4 ×·40			
290 and under 330	•40			6 ×4 ×·44			6 ×4 ×·40
330 and under 380	•40			6 ×4 ×·50	Mark Mark Mark Mark Mark Mark Mark Mark		6 ×4 ×·44
380 and under 430	•40	$7 \times 3 \times 3 \times 38$		6 ×4 ×·54			6 ×4 × ·50
430 and under 480	•44	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 40$,	6 ×4 × ·64	7 ×3 ×3 ×·38		6 ×4 × ·5
480 and under 540	•44	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 42$		$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60$	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 40$		6 ×4 × ·6
540 and under 600	•44	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 64$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60$
600 and under 670	•44	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	1 OV X	6 ×6 ×·64	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 6$
670 and under 740	•44	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$	08: X	$6 \times 6 \times 74$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		6 × 6 × · 6
740 and under 820	.50	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$		$7 \times 7 \times 70$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	000	6 × 6 × · 7
820 and under 900	.50	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 60$		7 ×7 × ·80	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	08	$7 \times 7 \times 7$
900 and 990	.50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		- 0000	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	-06-	$7 \times 7 \times \cdot 86$
990 and 1090	.50	$12 \times 4 \times 4 \times 64$		- 10Y-X8	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	98	
1090 and under 1200	.50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	8×.60		$12 \times 4 \times 4 \times 64$		1001 424 (100)
1200 and 1320	:50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 70$	8 × ·70		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	8×.60	
1320 and 1450	.50	$12 \times 4 \times 4 \times \cdot 70$	9×·70		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 70$	8×·70	KILL III IKU
1450 and under 1590	.54	$12 \times 4 \times 4 \times \cdot 72$	10×·74		$12 \times 4 \times 4 \times 70$	9×·70	1001 112 (101)
1590 and 1740	.54				$12 \times 4 \times 4 \times \cdot 72$	$10 \times .74$	
1740 and 1900	.54					10	100 E 1200
1900 and 2070	.54					PG [1909 9070

spaced the same as those below. In the case of decks fitted exclusively for the accommodation of passengers, and for depth, awaing of checks, proop of forecastle deck, H is to be taken as 5 feet.

Where the pillars above a deck are not placed over those below, H is to be the sum of the heights of the several tween decks in feet above the girder, with the addition of 5 feet for upper, awaing or shelter deck, bridge, poop or forecastle deck.

2. For methods of obtaining the numbers regulating the scantlings for girders, see Sketches on pages 138 to 141.

3. The girders are to consist of double channels or double angles, intercostal plate and rider plate, of the scantlings given in the Table. (See Sketches on pages 132 and 132) 132 and 133.)

4. The intercostal plates and channels or angles are to be fitted in long lengths and efficiently strapped or lapped at the butts to the Surveyor's satisfaction.

5. The channels are to be attached by two rivets to the lower flanges of the beams, or, in the case of angle or bulb angle beams to short angle lugs fitted to the beams, and where double angles are fitted in lieu of channels the intercostal plates are to be attached to the beams by angle lugs extending to the bottom of the girder and beams alternately where beams are fitted at every frame and to the bottom of the girder at every beam where beams are fitted at alternate frames. (See Sketch on page 133.)

6. The girders are to be efficiently bracketed to the bulkheads with plates three times the depth of the channels forming girders, measured from the upper edges of the channels and of the same thickness as the channels. The angle attaching the intercostal plate to the deck plating and intercostal plates to beams is to be of the same thickness as the plate, this angle is to be 3 ins. × 3 ins. where the rivets in the intercosaal plates are required to be \(\frac{3}{4}\) in. in diameter, and $3\frac{1}{2}$ ins × $3\frac{1}{4}$ ins. where they are $\frac{7}{3}$ in. in diameter. The channels and double angles to be zigzag riveted and the rivets spaced not more than 7 diameters apart, and those in the flanges of the intercostal angle not more than 5 diameters apart, centre to centre.

7. Girders of other form will be admitted provided they are of equivalent strength to those given in the Table.

^{1.*} S is the fore and aft spacing of the pillars in feet from centre to centre.

B is one-third the breadth of vessel in feet at the deck when two rows of pillars are fitted, and one-fourth the breadth when three rows are fitted.

H is the height of the 'tween decks next above the girder, measured in feet from top of beam to top of beam, where the pillars in the 'tween decks are spaced the same as those below. In the case of decks fitted exclusively for the accommodation of passengers, and for upper, awning or shelter, bridge, poop or

(Concluded.)

Contentation es	stal			DEPTH	OF BEAMS.		
NUMBERS *	Thickness of Intercostal Plate and Angle.	11	l inches.		1	2 inches.	
$\frac{S^2\timesB\timesH}{100}$	less of ate an			SIZE OF	F GIRDERS.		4.0000010002
	Thickr	Double Channels.	Rider Plate.	Double Angles.	Double Channels.	Rider Plate.	Double Angles.
150 and 180	•34	inches.	inches.	inches.	inches.	inches.	inches.
180 and under 210	•34						
210 and under 250	•34				082	00	ST. GREVEST
250 and under 290	•40					- 00	1 000
290 and 330	•40						
330 and 380	•40		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6 ×4 ×·40			
380 and 430	•40			6 ×4 × ·44			$6 \times 4 \times \cdot 40$
430 and 480	•44			6 ×4 ×·50			$6 \times 4 \times \cdot 44$
480 and 540	•44	$7 \times 3 \times 3 \times 38$		6 ×4 × ·54			$6 \times 4 \times 50$
540 and 600	•44	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 40$		6 ×4 × ·64	$7 \times 3 \times 3 \times 38$		$6 \times 4 \times 54$
600 and 670	•44	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6\frac{1}{2} \times 4\frac{1}{2} \times 60$	$7 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$		$6 \times 4 \times 64$
670 and 140	•44	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 64$	$7\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{2} \times 42$		$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 60$
740 and under 820	•50	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6 \times 6 \times 64$	$8 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 46$		$6\frac{1}{2} \times 4\frac{1}{2} \times \cdot 64$
820 and under 900	.50	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		$6 \times 6 \times .74$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$		$6 \times 6 \times 64$
900 and 990	•50	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		$7 \times 7 \times .70$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		$6 \times 6 \times .74$
990 and under 1090	.50	$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		7 ×7 × ·80	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		7 ×7 ×·70
1090 and 1200	.50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$			$11 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		$7 \times 7 \times .80$
1200 and 1320	.50	$12 \times 4 \times 4 \times 64$		814	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$		86 (108)
1320 and 1450	.50	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	8×·60		$12 \times 4 \times 4 \times \cdot 64$		601 - 10008
1450 and 1590	•54	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 70$	8×·70		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times 60$	8×.60	
1590 and 1740	•54	$12 \times 4 \times 4 \times \cdot 70$	9×·70		$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 70$	8×·70	as) nastr
1740 and under 1900	•54	$12 \times 4 \times 4 \times \cdot 72$	11×·74		$12 \times 4 \times 4 \times \cdot 72$	10×·70	12000 136
1900 and 2070	•54				$12 \times 4 \times 4 \times \cdot 72$	11×·82	Vicinia di

1.* S is the fore and aft spacing of the pillars in feet from centre to centre.

B is one-third the breadth of vessel in feet at the deck when two rows of pillars are fitted, and one-fourth the breadth when three rows are fitted. H is the height of the 'tween decks next above the girder, measured in feet from top of beam to top of beam, where the pillars in the 'tween decks are spaced the same as those below. In the case of decks fitted exclusively for the accommodation of passengers, and for upper, awning or shelter, bridge, poop or

forecastle deck, H is to be taken as 5 feet.

Where the pillars above a deck are not placed over those below, H is to be the sum of the heights of the several 'tween decks in feet above the girder, with the addition of 5 feet for upper, awning or shelter deck, bridge, poop or forecastle deck.

2. For methods of obtaining the numbers regulating the scantlings for girders, see Sketches on pages 138 to 141.

3. The girders are to consist of double channels or double angles, intercostal plate and rider plate, of the scantlings given in the Table. (See Sketches on pages 132 and 133.)

4. The intercostal plates and channels or angles are to be fitted in long lengths and efficiently strapped or lapped at the butts to the Surveyor's satisfaction. 5. The channels are to be attached by two rivets to the lower flanges of the beams, or, in the case of angle or bulb angle beams to short angle lugs fitted to the beams, and where double angles are fitted in lieu of channels the intercostal plates are to be attached to the beams by angle lugs extending to the bottom of the

girder and beams alternately where beams are fitted at every frame and to the bottom of the girder at every beam where beams are fitted at alternate frames. (See Sketch on page 133.)

6. The girders are to be efficiently bracketed to the bulkheads with plates three times the depth of the channels forming girders, measured from the upper edges of the channels and of the same thickness as the channels. The angle attaching the intercostal plate to the deck plating and intercostal plates to beams is to be of the same thickness as the plate, this angle is to be 3 ins. × 3 ins. where the rivets in the intercostal plates are required to be \(\frac{3}{4}\) in. in diameter, and $3\frac{1}{2}$ ins. × $3\frac{1}{2}$ ins. where they are $\frac{7}{8}$ in. in diameter. The channels and double angles to be zigzag riveted and the rivets spaced not more than 7 diameters apart, and those in the flanges of the intercostal angle not more than 5 diameters apart, centre to centre.

7. Girders of other form will be admitted provided they are of equivalent strength to those given in the Table.

(See Continuation.)

	William W.	Hadi Mi	FLAT KE	EL PLATE.	THICKN	ESS OF	THICKNESS OF OUTSIDE PLATING.					
	LONGITUDINAL NUMBER.	BREADTH OF FLAT KEEL PLATE	Thickness	Thickness throughout if Doubled for 3 length	GARBOARI WITH BA	D STRAKE AR KEEL.	From Flat K Garboard Str	ake to Upper	From Upper T		Propeller	
	$L \times (B+D)$.	AND GAR- BOARD STRAKES,	3 length 5 hamidships without Doubling.	Amidships, also thick- ness at Ends if Keel Plate is fitted without Doubling.	For $\frac{1}{2}$ length Amidships.	At Ends.	For $\frac{1}{2}$ length Amidships	At Ends.	For $\frac{1}{2}$ length Amidships.	At Ends.	Boss Plates.	
-	1950 and 1500	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	
1	$\frac{1250_{\text{under}}^{\text{and}}}{1500}, \frac{1500}{1750}$	_ 30	.36	.30	20	24						
	1750 , 1750 1750 , 2000	31	*38	.32	-30	.26	26	- "		"	.26	
	0000 0000		•40	32					26	"	,,	
	9950 9500	32			-32	.28	28	-26			.28	
	2500 , 2500 2500 , 2750		.42	.36			27	"	.28	26	27	
	2750 , 3000	33	•44		34	.30	30	"	"	"	.30	
	3000 , 3350			- 27	, ,,	"	- 27	"	30	"	22	
	3350 , 3700	34	·46	.38	.36	.32	·32	.28	"	"	.32	
	3700 , 4050	, ,,	•48	•40	22	"))	27	·32	.28	22	
	4050 , 4400	35	22	"	•38	·34	·34	.30	27	"	.34	
	4400 , 4800	"	.50	•42	"	"	"	"	·34	.30	22	
1	4800 , 5200	36	.52	,,,	•40	.36	.36	.32	27	22	.36	
	5200 , 5650	,,	22	"	"	"	27	27	.36	.32	22	
	5650 , 6100	37	.54	•44	•42	.38	.38	.34	22	22	.38	
	6100 , 6600	27	.56	•46	27	"	27	"	.38	.34	22	
	6600 , 7100	38	22	27	•44	.40	•40	.36	27	22	.40	
*	7100 , 7650	,,	.58	. ,,	22	27	22	"	•40	.36	22	
	7650 , 8200	39	.60	•48	•46	.42	•42	"	,,	27	.42	
	8200 , 8900	"	.62	"	27	"	22	"	•42	22	22	
	8900 , . 9600	40	.64	.50	.48	27	•44	:38	"	27	•44	
	9600 , 10300	,,	.66	27	27	27	22	"	•44	.38	27	
	10300 , 11000	41	.68	.52	.50	•44	•46	27	27	27	.46	
	11000 , 11800	.))	.70	27	27	27	,,	,,,	•46	27	.48	
	11800 , 12600		.72	.54	.52	.46	·48	.40	27	22	.50	
ī	12600 , 13600	25	.74	27	27	22 .	27	27	•48	•40	.52	
	13600 , 14600		.76	.56	.54	.48	.50	"	22	22	.54	
	14600 , 15800		.78	27	. ,,	"	27	"	.50	22	.56	
	15800 , 17000		.80	.58	.56		-52	•42	"	27	.58	
	17000 , 18200	, ,,	.82	22	22	27		"	.52	27	.60	
	18200. " 19500	44	- 27	"	.58	.50	.54	"	27	27	.62	
	19500 ,, 20800	. ,,	.84	.60	27	22	"	"	.54	•42	.64	
	20800 " 22200	27	.86	.62	.60	.52	.56	•44	27	22	.66	
	22200 " 23600	45	.88	27	. 22	22	"	27	.56	27	27	
	23600 , 25000	"	.90	.64	.62	.54	.58	27	27	27	.68	
	25000 , 26400)) -	27	27	22	. 22	"	22	.58	•44	22	
	26400 , 27800	46	.92	.66	.64	. ,,	.60	•46		"	.70	
	27800 , 29200	27	.94	27	"	2"	22	"	.60	27	"	

TABLE 17.

OUTSIDE PLATING.

See	Continuation.)	

	BREADTH	FLAT KE	EL PLATE,	THICKN	ESS OF		THICKNES	S OF OUTSIDE	PLATING.	
LONGITUDINAL.	OF FLAT KEEL PLATE AND	Thickness for $\frac{3}{5}$ length	Thickness throughout if Doubled for $\frac{3}{5}$ length Amidships,	GARBOARI WITH BA		From Flat K Garboard Stra Turn of	ake to Upper	From Upper 7		Propelle
$L \times (B + D)$.	GAR- BOARD STRAKES.	Amidships without Doubling.	also thick- ness at Ends if Keel Plate is fitted without Doubling.	For $\frac{1}{2}$ length Amidships.	At Ends.	For $\frac{1}{2}$ length Amidships.	At Ends.	For $\frac{1}{2}$ length Amidships.	At Ends.	Boss Plates.
20200 and 20600	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.
29200 and 30600	46	.96	.68	.66	.56	.62	•46	.60	•44	.72
30600 , 32000	47	.98	.70	"		22	22	.62	27	22
32000 , 33400	27	1.00	.72	.68	.58	.64	·48	22	27	.74
33400 , 34800		1.02	.72	22	22	27	22	.64	.46	22
34800 , 36200	48	1.04		.70	.60	.66	"	27	"	.76
36200 , 37600	27	1.06	.74	27	22	27	22	22	>>	27
37600 , 39000		1.08	.76	.72	.62	.68	.50	.66	22	.78
39000 , 40400	49	1.10	27	22	22	27	22	22	27	22
40400 ,, 41800	27	1.12	.78			.70	22	.68	.48	.80
41800 ,, 43200	27	1.14	.80			27	22	22	27	27
43200 , 44600	50	1.16	27			.72	.52			.82
44600 , 46000	27	1.18	.82				27	•70	27	
46000 , 47400	27	1.20	,,			.74			27	·84
47400 , 48800	51		·84	,			"	-72	.50	
48800 , 50200						76	.54			.86
50200 , 51600	- 27		·86			-			27	00
51600 , 53000	52					.78	27	.74	2)	.88
53000 , 54400			·88			-	27	7 7	27	00
54400 , 55800	- 27		- 00			.80	.56	.76	.52	.90
55800 , 57200	53		·90			- 00		70	32	90
57200 , 58600			- 30			27	27		22	,00
58600 , 60000	27		.92			.82	27	"	22	.92
60000 , 61400	54		-92			27	27	·78	27	22
	34		27			.84	.28	22	27	.94
61400 , 62800	22		·94			22	27	.80	.54	22
62800 , 64200	27		22			.86	27	27	22	.96
64200 , 65600	55		.96			22	22	27	22	22
65600 , 67000	27		22			.88	.60	.82	.56	.98
67000 , 68400	27		.98			22	22	27	22	22
68400 , 69800	56		27			.90	22	.84	27	1.00
69800 , 71200	22		1.00			22	22	27	22	"
71200 " 72600	22		27			.92	.62	22	22	1.02
72600 ,, 74000	57		1.02			22	22	.86	.58	27
74000 ,, 75400	27		22			.94	22	22	22	1.04
75400 ,, 76800	27		1.04			22	27	-88		
76800 , 78200	58					.96	•64		27	1.06
78200 , 79600	22		1.06					27	27	
79600 , 81000						98	27	·90	.60	1.08
//	27		22				27	00	00	1 00

LOWER DECKS.

TABLE 17.

									(See Continuati	ion.)
LONGITUDINAL	OR SHE	DECK CK IN AWNING LTER DECK SSELS).	(2ND DECK I	DECK IN AWNING OR CCK VESSELS).		W 3RD DECK N AWNING OR CCK VESSELS).	BEAM STRINGERS AT ENDS OF 2ND DECK (UPPER DECK	THICK- NESS OF 2ND AND 3RDDECKS (UPPER		CKS IN
NUMBER.			Stringer for	Tie Plates	Stringer for	Tie Plates	IN AWNING OR SHELTER DECK VESSELS) AND ALL	AND 2ND DECKS IN AWNING OR	WAY OF ERECT	IONS.
$L \times (B+D)$.	Stringer for $\frac{1}{2}$ length Amidships,	Tie Plates for $\frac{1}{2}$ length Amidships.	$\frac{1}{2}$ length Amidships.	for $\frac{1}{2}$ length Amidships.	$\frac{1}{2}$ length Amidships.	for $\frac{1}{2}$ length Amidships.	DECKS BELOW, ALSO THICK- NESS OF TIE PLATES AT ENDS.	SHELTER DECK VESSELS) AT ENDS.	For $\frac{1}{2}$ length Amidships.	At Ends.
1250 and 1500	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.
$\frac{1250_{\text{under}}^{\text{and}}}{1500}$, $\frac{1500}{1750}$			- 00 24	0.850		95.2	BE BE	1 00	$2\frac{1}{2} \times 2\frac{1}{2} \times 22$.22
1750 , 2000				-					" " " 24	·24
2000 , 2250										
2250 , 2500									27 27 27 27 27 27	
2500 , 2750									" " <u>"</u> 26	.26
2750 , 3000						-			27 27 27	22
3000 , 3350				,				7 00	" " ·28	.28
3350 , 3700									22 22 22	27
3700 " 4050 4050 " 4400						2		00	" " " 3 ×3 × "	- 27
4400 , 4800		- 128				200			$3 \times 3 \times ,$	
4800 , 5200									" " " " 30	30
5200 , 5650										
5650 , 6100									" " ·32	*32
6100 ,, 6600									27 27 27	22
6600 , 7100			3,400						27 27 27	22
· 7100 , 7650									" " 34	22
7650 " 8200 8200 " 8900									27 27 27	
	40×·34	9×34				0//	18 4.21		27 27 27	.91
9600 , 10300			0.99				$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		27 27 27	•34
10300 , 11000	"" 41×·36	$\frac{"}{10 \times 36}$					20		" " " " 36	
11000 " 11800		27 27					21 ,		" " "	27
11800 " 12600	42 ,,	" "					22×36		27 27 27	.36
12600 , 13600	" ·38	11×38					23 "		$3\frac{1}{2} \times 3\frac{1}{2} \times 38$	22
13600 , 14600	-22 22						24 "		22 22 22	27
14600 , 15800 15800 , 17000	43 , 40	" " 19 × ·10	1990	1020			25 ,,		" " "	27
17000 , 18200		12×40	43×38	12×38			$\begin{array}{c c} 26 \times 38 \\ \hline 27 & , \end{array}$		" " .40	.38
18200 , 19500	." " 44		" " " 44 "	27 27			28		27 22 27	
19500 , 20800	, 42	$\frac{"}{13 \times \cdot 42}$	//	13 "			20		" " " 42	
20800 , 22200	27 27	" "	" ·40	,, ·40			30×40))))))))))))))	·40
22200 , 23600	45 "	22 22	45 ,,	. 27 27			31 ,,		27 27 27	27
23600 , 25000	" ·44	$14 \times \cdot 44$	22 22	14 "			32 "		" " •44	27
25000 , 26400	22 22	.))))	22 22	27 27			" "		22 22 22	27
26400 , 27800 27800 , 29200	46 ,,	" "	46×42	"·42			33×42		22 22 22	.42
2000 , 20200	" 46	15×46	27 27	15 "			27 27		" " .46	27
-	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	1		1		1	-			

LOWER DECKS.

(See Continuation.)

LONGITUDINAL	1	ER DEC	DECK K IN AWNING TER DECK		3RD DECK II LTER DE	N AWNI		(2ND	S BELO DECK I LTER DE	N AWI	NING OR	STRI AT E 2ND	EAM INGERS NDS OF DECK ER DECK	THICK- NESS OF 2ND AND 3RDDECKS (UPPER	AT AND	ALL AT U	INGER A LOWER I	ECKS,
NUMBER. $L \times (B+D).$	$\frac{1}{2}$ 1	ger for length dships.	Tie Plates and Deck Plating for $\frac{1}{2}$ length Amidships.	$\frac{1}{2}$ 1	ger for length dships.	Deck I for $\frac{1}{2}$	Plates nd Plating length ships.	$\frac{1}{2}$ 1	nger for ength	for $\frac{1}{2}$	Plates length	IN A OR SI DECK ANI DECKS ALSO NESS PLAT	WNING HELTER VESSELS) D ALL	AND 2ND DECKS IN AWNING OR SHELTER DECK VESSELS) AT ENDS.		or $\frac{1}{2}$ le		At Ends
29200 and and 30600		ches. × ·46	inches. 15×46		ches.		hes.	ine	ches.	in	ches	9	ches.	inches.	0.1	inch		inche
30600 , 32000	47			47	× ·42	15 >	X 42		-			34	× ·42	1 X 185	$\frac{3\frac{1}{2}}{2}$	$\times 3\frac{1}{2}$	× ·46	-42
32000 , 33400	22	·48	27 27 Dk. ·36 Pltg.		•44	16	·44					35	×·44	30	27	22	·48	.44
33400 , 34800				27											- 27	22		-
34800 , 36200	77	27	-38	48	27		27					36	"	- 27		27))	
36200 , 37600	22	27	"		27	17	27						27	27	27	22	27	
37600 , 39000	22	22	•40	27	27	22	27					37		-32	27	27	27	22
39000 , 40400	49	27	,,	49	27	22	22					27	27	27	22	27	27	27
40400 , 41800	27	.50	27	27	22	18	22					27.	22	27	4		×.50	2"
41800 , 43200	22	22	>>	22	22	22	22					38	22	22	"	. 22	27	22
43200 , 44600	50	22	22	50	22	22	22					22	22	22	27	22	27	27
44600 , 46000	27	27	.42	22	22	19	27	50	× ·44	19	$\times .44$	22	22	22	27	22	"	27
46000 , 47400	27	22	22	22	22	Dk. 3	6 Pltg.	27	22	22	27	39	22	27	27	22	"	27
47400 , 48800	51	"		51	22	,	,	51	27	22	22	27	22	22	27	22	27	27
48800 , 50200	27	.52		27	•46	,	,	27	.46	20	× ·46	27	.46	22	27	22	:52	46
50200 , 51600 51600 , 53000	77	22	27	27	22	,	,	"	27	22	"	40	27	22	27	22	"	
51600 , 53000 53000 , 54400	52	27	•44	52	22	,	,	52	27	27	"	22	"		27	22	"	
54400 , 55800	27	22		22	22	.3	2	22	27	21	"	27	27	.34	27	22	"	
55800 , 57200	53	27		53	22	9	0	53	22	22	"	41	27	54	27	27	27	
57200 , 58600		.54	; ·46	00	27)		27	22	"	27	"	27	27	27	.54	22
58600 , 60000	27			27	27	,			27	-	22	42	27	27	27	22		
60000 , 61400	54	27		54	27		"	54	27		22		27	27	27	27	27	27
61400 , 62800	22))))	27		. 22	•4			27	23	22	27	27	27	27	22	. 22	
62800 , 64200	22	27	•48	27	·48)	27	•48	22	·48	43	×·48	27	22	27	27	48
64200 , 65600	55	22	22	55	,,		"	55	22	27	22	27	22	27	"	27	27),
65600 , 67000	27	.56	"	22	"		"	27	22	24	22	27	22	22	22	22	.56);
67000 , 68400	22	27	.50	27	22		"	27	"	27	22	44	"	22	"	22	22),
68400 , 69800	56	22	22		× ·50	•4	2	56	$\times .20$	27	.20	22	22	.36	22	22	22	22
69800 , 71200	27	.28	27	22	22	,	"	27	27	25	22	27	22	27	27	. 22	.58	27
71200 , 72600	27	27	.52	27	22	,)	22	22	22	22	45	"	27	27	22	"	, ,,
72600 , 74000	57	22	22	57	22	,)	57	27	22	27	27	.50		22	22	"	.20
74000 , 75400 75400 76800	27	.60	27 ~ 4	22	.52		"	22	.52	26	× ·52	27	27	22	27	27	.60	
75400 " 76800 76800 " 78200	77		.54	77	27	•4	4	77	27		22)) 10	22	27	27	22	27	
78200 , 79600	58	.69		58	27		"	58	22	27	22	46	22	22	27	22	.62	
79600 , 81000	27	.62	.56	27	.51		"	22	.5.4	27	27	27	22	- 27	27	22	02	- 27
, 01000	22	27	90	27	.54	,	"	27	.54	27	22	27	27	22	27	27	27	27
																		1

In a vessel requiring two steel decks the thickness of the stringers and deck plating of the 2nd deck may in way of a "long" bridge be as required for a 3rd deck, but in no case is the deck plating to be less than '36 of an inch in thickness.

(See Continuation.)

YOU TO BE ADDRESS OF THE PARTY											"SF	HOR	T" E	REC	CTIC	ONS	· Given		030	anyse:			-		
LONGITUD					POOP	s						** {	SHORT"	BRII	GES.					FOR	ECAS	TLES.			
L×(B+	-D)	Side Plating	Strin	ger Aı	ngle.	Strii Pla		Tie Pl	ates.	Maxi- mum Length of "Short" Bridge.	Side Plating	Str	ringer An	ngle.		inger ate.	Tie Plates and Deck Plating.	Side Plating	St	ringer Ang	le.	Strli Pla	nger te.	Tie Pi	lates.
1950 and	1500	inches.		inches.		incl		inch		feet.	inches.	01.	inches.			hes.	inches.	inches.	01	inches.	.00	inel		inch	nes.
$\frac{1250_{ m under}^{ m and}}{1500}$,	$\frac{1500}{1750}$		$2\frac{1}{2} \times$	21/2)	× .77	10 ×	. 22	$5\times$.77	20	.22	427	$\times 2\frac{1}{2} >$		7 2	(22	$5 \times .22$.22	21/2	$\times 2\frac{1}{2} \times$	22	IUX	. 22	OX	- 66
1750 ,,	2000	- 27	22	22	27	77	22	27	22	22		22	"		$\frac{15}{16}$	22	27 27		27	27	27	77	27		27
2000 ,,	2250	- 22	27	22	22	11	22	27	27	25		27	22	22	-4 1999	22	22 22	27	22	27	27	11	22		27
2250 ,,	2500	- 22	22 .	22	27	22	22	22	27	20		27	22	27	17	22	22 22	27	27	27	22	27	27		27
2500 ,,	2750	- 27	27	22	22	77	22	22	22	27	22	27	27	27	$\frac{18}{19}$	22	0	27	22	22	22	12	27	27	27
2750 ,,	3000	1/ .	22	"		12	27	6	27	30	_ 27	27	"	27	$\frac{19}{20}$	27	6 ,,	22	22	27	27		- 22	6	"
3000 ,,	3350	1)	22	27	.24	27	•24		.24		·24	27	27	.24		·24		24	22	22	·24	22	.24		.24
3350 "	3700	24	22	27		13	24	22	24		24	27	"		22	24	27 24	24	22	- //		" 13		27	
3700 "	4050	22	27	27	. 27	19	22	27	27	25	_ 27	22	27	27		22	27 27	22	27	22	27	10	27	22	27
4050 ,,	4400	8 //	27	27	"	22	27	22	22	35	- 22	22.	"	22	23	22	27 27	27	22	27	27	27	27	22	22
4400 ,,	4800	1 //.	22	22 .	, 22	77	27	22	27	27		27	27	22	24	22	22 22	27	27	22	27	77	27	27	22
4800 ,,	5200	1)	22	27	22	14	22	22	22	27		22	22	22	$\frac{25}{26}$	27	2) 2)	22	22	22	22	14	- 22		22
5200	5650	4 //	27	. 27		27	27	27	"	40		27	22		26	. 22	22 22	27	22	22	22	27	27	22	27
5200 "		1)	3 ×	0	,96	77	27	27	,00	27	277	3	× 3 ·		27	"		27	3	$\times 3$.96	77	·26	27	.26
5650 "	6100		27	,))	20	19 >	< .26	22	.26	77	.26	27	. 27	.26		× ·26	<u></u> ·26	.26	22	22	20	$15 \times$	20	_ 22	20
6100 ,	7100	8 77	22	27	27	77	22	22	. 22	45	22	27	27		29	22	1 27	27	27	27	27	77	22	7	22
6600 ,,	$\frac{7100}{7650}$	8 //	22	22	22	16	22	7	" "	22	27	27	22		30	22	27 27	22	22	27	"	16	.00	1	.28
7100 ,,	7650		22	27	"	22	27	27	"	27	.28	22	27	.28		22	<u></u> ·28	.58	27	22	.28	77	.28	_ ;;	20
7650 "	8200	3	27	22	.28	17>	<.28	27	.28	50	27	27	22	//	32	22	22 22	27	22	27	22	17	22	22	22
8200 "	8900	9 //	22	27	27	22	22	22	22	27	22	27	"	,,	33	"		22	22	22	22	77	"	_ 22	22
8900 ,,	9600	. //	22	27	27	18	22	22	22	27	.30	27	"			× ·30	30	.30	27	. 22	22	18	22		22
9600 ,,			22	27	27	19	22	22	"	55	22	22	22	22	35	"	22 22	22	27	22	22	19	"	22	"
10300 "			22	"			< .30	27	.30	27	22	22	22		36	"	22 22	27	27	27		20 >	< .30	22	.30
11000 ,,			27	22	"	21	. 22	22	"	27	.32	27	22	.32	37 >	× ·32	,, 32	.32	27	27	27	21	"	22	22
11800 ,,	12600	22	27	"	22	22	22	27	22	60	22	22.	22		38	"	8 ,,	27	27	"	22	22	22	22	22
12600 ,,	13600	27	27	"	. 22	23	27	8	27	22	,-	27	"	//	39	22	22 22		22	27		23	22	8	- 22
13600 "	14600	:32	22	27	"	24	. 27	22	22		.34	22	"			× ·34	,, 34	34	27	27	22	24	22	22	22
14600 "	15800	22	22	22	"	25	. 22	27	"		22	22	22	22	41	"	22 22	22	22	27	27	25	22	"	22
15800 "	17000	22	27	22	.32	26>	⟨.32	22	.32	27	22	22	22	22	42	22		22	22	27	.32	26>	(.32	22	.32
17000 ,,	18200	27	22	22	22	27	22	22	27	27	.36	22	22	.36	22	.36	,, 36	.36	22	22	22	27	"	"	"
18200 "	19500	.34	22	22	. 22	28		22	22	70	22	22	22		43	. 22	22 22	22	22	22	22	28	22	"	"
19500 "	20800	27	22	"	22	29	22	22	22))	22	22	22	22	22	22	27 27))	22	22		29	22	"	"
30800 "	22200	22	22	"	22	30	22		"		.38	"	22	. ,,		× ·38			27	22	22	30	"	"	"
22200 "	23600))	22	"	22	31	22	22	27	75	22	22	22	22	22	"	9 "	22	27	27	**	31	"	22	27
23600 "	25000	36	22	22	22	32	22	9	22	22	27	22	"		45	"			22	22	"	32	22	9	"
25000 "	26400	- 22	$3\frac{1}{2} \times$	$3\frac{1}{2}$	× ·34	27	•34	27	.34	22	22		$\times 3\frac{1}{2}$		27		22 22		$3\frac{1}{2}$	$\times 3\frac{1}{2} \times$	•34	22	.34	22	.34
26400 "			22	22	22	33		22	"	80	.40	22	22	.40	38	× ·40	Dk. Pltg. 26	.40	22	,,	22	33	22	22	22
27800 "			17	22		22		27	27	-	22	22			22	22		22	22	27		"	"	22	27
AMERICAN STREET, AND THE STREET, STREE	OF THE PERSON NAMED IN			CHICA STRANGE CO.	- Designation	1	//		,,	1 "	//	"	//		-				1						

(Concluded.)

											"SI	НОІ	RT" E	REC	CTIONS				- 35		ARREIT	
LONGITU					POOP	s.						44 8	SHORT"	BRID	GES.				FORECA	STLES	3.	COX .
L×(B		Side Plating	Strin	ager An	ngle.		nger ate.	Tie	Plates.	Maxi- mum Length of "Short" Bridge.	Plating	St	ringer An	gle.	Stringer Plate.	Deck Plating.	Side Plating	Strin	iger Angle.		inger ate.	Tie Plater and Deck Plating.
20000 and	20000	inches.		inches.	0.4		hes.		ches.	feet	inches.	0.1	inches.	4.0	inches.	inches.	inches.		nches.		ches.	inches.
29200 and unde			$3\frac{1}{2} \times$	$3\frac{1}{2} \times$	('34	$34 \times$	('34	9	× ·34	80	40	$3\frac{1}{2}$	$\times 3\frac{1}{2} \times$	('40	$39 \times \cdot 4$		40	$3\frac{1}{2} \times$	$3\frac{1}{2} \times 34$	134)	× '34	$9 \times .3$
30600 ,,		_ 27	22	22	22	"	27	27	22	27	22	22	22	27	27 2	.28	27	"	27 27	27	22	
32000 ,,	24800	- 27	22	22	- /	35	"	27	.90	85	22	22	27	27	22 2		27	27	27 27		.26	"
33400 " 34800 "	26200	27	22	27	.36	//	.36	22	.36		•42	22	22	.42	$40 \times \cdot 4$	//	42	22	,, .30	96	.36	"
			27	22	27	36	"	22	22	_ 22		27	22	22	27 2	.30	27	22	22 22	36	27	
36200 " 37600 "			22	22	22	27	22	27	22	27		27		22	22 2	27	27	22	22 22	07	22	
39000 ,,			22	22	22	37	22	22	22	27		22	22	22	41 ,	32	27	22	2)))	01	27	
0400 ,,			22	22	22	27	22	77	22	90	- 22	27	22	27	22 2	02	27	22	22 22		22	" 10
1800 "	43200	27	22	22	27	38	22	10	27		277	27	22	27	$\frac{?}{42 \times \cdot 4}$.44		22 22	38		10
3200 ,,	44600	_ 27	27	22	.38	90	.38		.38		•44	27	22	44	42 X 4	*34	11	27	,, 38	2	.38	"
4600 ,,	46000	22	22	27	90	22	90		- 50	27		27	27	22	22 2	94	27	22	27 00			"
6000 ,,	47400	.42	27	22	"	39	22	22	22				27	27	" · · · · · · · · · · · · · · · · · · ·			22	27 27	39	27	- 27
7400 ,,			22	22		00	22	22	22	27		27	27		70 ,		27	22	27 27	-		
8800 ,,	50200	27	27	22	27	27	27_	27	22	95	- 27	27	27		27 2	-36	27	27	27 27		27	
0200 ,,	51600		22	22	27	" 40	27	27	22	30	·46	27	22	·46	$\frac{\cancel{\cancel{0}}}{44 \times 4}$	2	.46	27	27 27	40	27	"
51600 ,,	53000	27	27	22	·40	10	·40		·40	_ 22	40	22);	40	11 / 1			22	;; ·4(7	·40	22 .7
53000 ,,		//	"	22		22	40	27	40	- 27		27	27	27	22 2		27	27	-//			
			27	27	27	27		27	27			27	27	27	27 2		27	27	2) 2)		2)	Dk. Plt
54400 ,,	55800	22	22	22	22	41	22	22	22	27	22	22	"	22	45 ,	.38))	27	22 22	35	22	.38
5800 ,	57200	•44	22	22	22	22	22	11	22	22	_ 22	22	22	22	22 22	22))	27	22 22	22	22	
7200 ,		27	"	22	22	22	22	22	22	22	_ 27	22	22	22	22 22))	22	22 22		22	
8600 ,	60000	22	22	22	22	42	22	22	22	2.	.48	22	"	.48	$46 \times \cdot 48$		48	22	22 22	36	22	
30000 ,		22	"	22	22	22	22	22	"	100	22	4	$\times 4$	22	22 22	•40	22	27	22 22		22	22
1400 ,,	62800	22	22	22	.42	22	.42	22	.42	27		22	22	27	22 22	27))	22	,, .42		.42	22
2800 ,,			"	22	22	43	22	27	22	27	27	22	"	22	47 ,	"	22	22	27 27	37	22	
4200 ,,	65600	22	22	22	22	"	22	22	22	27	27	22	"	22	22 22	22	27	"	22 22	27	22	
5600 ,,	67000	.46	"	27	22	27	22	"	22	27	22	22	"	22	22 22	•42	22	27	22 22	22	22	22
7000 "	68400	22	"	22	22	44	22	22	22	27	.50	22	"	.20	$48 \times .50$) "	.20	"	22 22	38	22	22
8400 ,,	69800	22	"	22	22	"	22	22	22	27	27	22	22	27	22 22	27	27	22	22 22	27	22	22
9800 "			22	22	22	"	22	22	22	22	22	22	"	22	27 27		27	27	" "	22	22	"
1200 "			"	27		45	22	27	22	105	22	22	22	22	49 ,	•44	27	"	22 22	39	22	•40
2600 ,,			22	22	•44	22	•44	22	•44	22		22	22	22	22 22	- 22	22	"	"·44))	•44	
4000 ,,			$4 \times$	4	22	27	"	12	22	22	22	22	22	22	22 22		27	$4 \times$			22	22
5400 ,,			"	"	22		22	"	22	"	.52	22	22	.52	$50 \times .52$.52	"	22 22		22	22
76800 ,,			"	22	22	46	22	"	22	22	22	22	22	22	22 22	.46	22	"	22 22	40	22	27
8200 ,			"	22	22	22		22	22	22	22	22	22	.58	22 22		27	27	27 27	27	22	"
9600 "	81000	22	22	"	22	"	22		22	22	22	22	22	22	51 "	22	22	22	27 27	22	27	22

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON.—17th June, 1909.

TABLE 18. (See Continuation.)

	T	ND V.			avoit	-	PROPORT	IONS OF	L	ENGTH T	O DEPTH.						
LONGITUDI	NAL	KE A			Under	10.			-			10	and under	. 11.			
L×(B+		BREADTH OF SHEERSTRAKE AND STRAKE BELOW.	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	Stringer An for $\frac{1}{2}$ leng amidship	ngle	Stringer Plate for $\frac{1}{2}$ length amidships.	Tie Plates a Deck Plate for $\frac{1}{2}$ leng amidship	ing th	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	Strin	$\frac{1}{2}$ length idships	ngle th	Stringer Plate for $\frac{1}{2}$ length amidships.	Tie Plate Deck P for 1/2 le amidsl	lating ength hips.
- Second		inches.	inches	inches.	inches.		inches.	inches,		inches.	inches.		inches.	.01	inches.	inch	
$1400_{\mathrm{under}}^{\mathrm{and}}$	1650	30	·24	.24	$2\frac{1}{2} \times 2\frac{1}{2} \times$	(24	$14 \times \cdot 22$	5 × .	22	.26	·24	$2\frac{1}{2} \times$	$2\frac{1}{2} \times$		$16 \times \cdot 22$	$5\times$	22
1650 "	1900	22	·26	"	jn 27	27	15 "		"	.28	"	27	22	22	10 ,,	6	.94
1900 ,,	2150	31	"	·26	27 27	.26		"	24	22	.26	"	"	.26	18 × ·24		.24
2150 "	2400	22	.28	22	$3 \times 3 \times$	27	17 ,,	22	"	.30	"	3 ×	3	"	19 ,,		,96
2400 ,,	2650	32	27	.28	22 22	.28		27	26	"	.28	22	"	.28	$20 \times .26$	° 22	.26
2650 "	2900	22	.30	22	27 27	22	19 ,,		"	.32	"	22	22	22	21 ,,		.00
2900 "	3150		27	.30	22 22	.30		77	28	27	.30	22	22	.30	22×·28	27	.28
3150 "	3500	22	.32	, ,,	27 27	"	21 "		"	•34	"	22	"	27	23 ,,	1	,20
3500 "	3850		"	:32	22 22	.32		27	30	"	•32 .	27	22	.32	24×30	27	.30
3850 "	4200	22	·34	"	22 22	22	. 23 "	22	"	.36	27	22	22	22	25 ,,	22	,99
4200 "	4600		22	.34	22 22	.34		//	32	27	•34	27	27	•34	26×32	27	.32
4600 "	5000	,,	.36	22	22 22	22	25 "		"	.38	27	22	22	"	27 ,,	- 8	22
5000 "	5400	.36	27	.36	27 27	.36		"	34	27	.36	27	22	.36	28×34	27	.34
5400 "	5800	,,	.38	"	27 27	"	28 "	22	22	•40	27	27	27	22	30 ,,	27	22
5800 "	6300		"	.38	22 22	.38	30×36	,,	36		.38	22	27	.38	32×36	27	.36
6300 "	6800) ,,	•40	22	27 27	22	32 "	9 .	22	•42	"	27	27	22	34 "	9	22
6800 ,,	7300		"	•40	22 22	.4(34×38	22	38	•44	•40	22	27	.40			.38
7300 ,,	7900) ,,	•42	"	27 27	"	36 ,,	10	"	27	2)	22	"	"	38 "	10	22
7900 "	8500	_ 1 //	"	•42	22 22	.45		22	40	•46	•42	22	"	.42			.40
8500 ;,	9200)	•44	"	$\overline{3\frac{1}{2} \times 3\frac{1}{2}}$	"	40 ,,	11	"	22	22	$3\frac{1}{2}$	$\times 3\frac{1}{2}$	22	42 "	11	22
9200 "	9900	$\frac{1}{40}$	27	•44	22 22	.4		22	42	.48	•44	22	22	•44			.42
	10600		•46	22	22 22	27	44 "	12	"	27	27	22	22	22	46 "	12	27
	11400		22.	•46	22 22	.4		22	•44		•46	22	22	.46			.44
11400 "			•48	. ,,	4×4	22	48 "	13	"	"	"	4 >	× 4	22	50 "	13	27
12200	13100	0 42		•48	22 22	•4		,,	•46		•48	22	22	.48			.46
13100 ,	14100	0	.50	22	22 22	22	59	14	22	"	27	22	22	22	54 ,,	14	22
14100 ,,	1520	0 "	,,,	•50	27 27	22.	51 V ·18	3 ,,	.48		.50	22	22	22	$56 \times \cdot 48$.48
15200 ,,	1640	0 43			$-\frac{7}{4\frac{1}{2} \times 4\frac{1}{2}}$	22	56	15	"	"	27	412	$\times 4\frac{1}{2}$	22	42 ,,	Dk.3(for $\frac{1}{2}$
16400 ,,		0		.52	7)))	.5		_			.52	22	22	.20			"
17600 "	1880	0 -"	54	"	27 27	27	19 V · 15			.58	22	27	22	22	44×·50)	"
18800 "	2010	0 44		•54		.5		22		"	•54	22	22	.52		Cmpl.	30^{de}
20100 ,,	2150	0	.56			27	11	Cmpl. 3) dec	·60	22	22	22	22	46 "		27
$\frac{20100}{21500}$,		0		-56	27 27	.5				27	.56	22	27	.54			32
$\frac{21900}{22900}$,					27 27	22	16 V .51) "		·62	"	22	22	22	48×·5		22
$\frac{24300}{24300}$,	2570	0	-	.58	27 27	.5		3			•58	27	27	.50	3 49 ,,		34
$\frac{24300}{25700}$,	2710	0 ,,	-60				18			.64	"	27	"	22	50 ,,		22
27100 ,,			3	-60	27 27	27	10	-3			-60	27	27	27	51 "	- 1	36
28500 ,,			.62		27 27	27	50 v			.66		-	27	27	52×·5	1	22
,,	2000	"	02	"	27 27	27	,,,	. "			27	27	77	//	-		

The topside scantlings and decks before and abaft a bridge are to be determined by the vessel's proportions taken to the upper deck. These scantlings are to be maintained throughout the length of a "short" bridge, and are to be extended within the ends of a "long" bridge for a distance equal to one-third the breadth of the vessel.

The upper deck stringer angles in the above Table may be gradually reduced at the ends of the vessel to the size given in Table 17 for upper deck stringer angles at ends in way of erections,

TABLE 18.

LONGITUDINAL	AND W.		111111111111111111111111111111111111111	0 0	T, HT		PRO	PORT	TIONS OF L	ENGTH T	O DEPTH						uation.)
NUMBER.	RAKE BELO	1 32 8		U	nder	10.				SI des	11	10) and	d 11.			DE UNI
$L \times (B+D)$.	BREADTH OF SHEERSTRAKE AND STRAKE BELOW.	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	for	nger An $\frac{1}{2}$ leng	gth	Stringer for $\frac{1}{2}$ leading amids	ength	Deck Plating for $\frac{1}{2}$ length amidships.	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	for	nger 1 1 1e midsh	ngth	Stringer for $\frac{1}{2}$ leading amids	ength	Deck Plating for $\frac{1}{2}$ length amidships.
00000 and 01000	inches.	inches.	inches.		nches.	-0	inch		inches.	inches.	inches.		inche		inch		inches.
29900 and 31300		.62	.62	$4\frac{1}{2}$ ×	$(4\frac{1}{2})$.58	51×	:52	.36	.66	.62			× ·58	53×	:54	.38
31300 , 32700		.64	22	22	22	22	52	22		.68	//	$5 \times$	(5	22	54	22	"
32700 , 34100		"	.64	27	27	.60	53	22	.38	"	.64	22	"	.60	55	27	•40
34100 , 35500		.66	- 27	5 ×	5	22	54	22		.70	"	22	22	"	56×	.56))
35500 , 36900		.00	"	22	22	.62	55	22	•40		.66	27	"	.62	57	27	27
36900 , 38300	27	.68	.66	22	22	27	56×	54		.72	"	22	22	"	58	27	•42
38300 , 39700	22	"	27	22	22	.64	57	22		27	.68	22	"	.64	59	27	
89700 , 41100		•70	.68	22	"	27	58	22	.42	·74	"	22	"	22	60 ×	.58	
41100 , 42500	22	"		22	22	27	59	"	27	"	.70	22	"	22	61	27	•44
$\frac{42500}{12000}$, $\frac{43900}{45200}$	27	.72		"	27	22	60	22		.76	"	22	"	"	62	22	
43900 , 45300	50	22	.70	27	22	.66	61 ×	.56	•44		.72	22	"	.66		27	"
45300 , 46700	22	·74	27	27	22	22	62	27		.78	22	27	22	22	64×	.60	.46
16700 , 48100	22	- 22	.72	27	22	.68	63	27	22		.74	22	22	.68		27	"
8100 , 49500		.76		22	22	·70	64	27	•46	.80		22	"	22	66	22	"
$\frac{19500}{19900}$, $\frac{50900}{19900}$	_ 27	"	27	27	22	.70	65 ×	.58	27	.82	.76	22	"	.70	2at48)	×.62	·48
50900 , 52300	27	.78	.74	22	22	27	66	22	27		- 27	22	"	22	22 22	. 22	27
52300 , 53700				22	22	.72	2at48	27	•48	·84	.78	20	"	.72	,, 49	22	27
53700 , 55100	_ 22	.80	.76	22	22	22	22 22	.60	27	.86		22	22	"	22 22	.64	.50
55100 , 56500	22	27	27	27	27	22	,, 49	22		27	.80	6 ×	6	22	,, 50	22	27
56500 , 57900	53	.82	- 27	22	27	27	22 22	.62	.50	.88		27	22	27	22 22	.66	27
57900 , 59300	22	27	.78	22	"	.74	" 50	22	22	.90	·82	27	22	.74	,, 51	22	.52
59300 , 60700	22	·84	27	6 ×	6	22	22 22	.64	22	22	2)	27	"	22	22 22	.68	27
60700 , 62100		27	.80	22	22	.76	,, 51	22	.52	.92	·84	27	"	.76	,, 52	22	.54
32100 , 63500	22	.86	27	22	22	27	22 22	.66	22	.94	22	27	27	22	22 22	.70	.56
3500 , 64900	_ 22	27	27	27	22	.78	" 52	22	.54		.86	22	"	.78	,, 53	22	27
34900 , 66300		.88	.82	27	22	22	22 22	.68	.56	.96	22	22	"			·72	.58
66300 , 67700		27	27	22	22 .	.80	,, 53	22	22	.98	.88	27	"	.80	,, 54	22	.60
7700 , 69100		.80	·84	"	"	22	22 22	.70	.58	22		7 ×	7	22	22 22	.74	27
$\frac{9100}{2500}$, $\frac{70500}{21000}$	56	27	22	"	22	22	,, 54	22	.60	1.00	.80	"	22	27	,, 55	22	.62
70500 , 71900		.92	22	22	22	22	22 22	.72	"	1.02	27	22	27	"	22 22	.76	.64
71900 , 73300	27	.94	.86	27	22	.82	,, 55	27	.62	"	.92	22	22	.82	,, 56	22	22
3300 , 74700		22	27	27	27	22	22 22	.74	.64	1.04	22	22	22	22	22 22	.78	.66
4700 , 76100		.96	.88	22	22	.84	,, 56	22	27	1.06	.94	27	22	.84	,, 57	22	.68
6100 , 77500	- 22	.98	27	7 ×	7		27 27	.76	.66	22		8 ×	8	22	22 22	.80	27
7500 , 78900	58	27	,,	22	22		,, 57	22	.68	1.08	.96	22	22	.86	,, 58	27	.70
8900 , 80300	27	1.00	.90	22	22		22 22	.78	27	1.10	27	27	22	27	22 22	.82	.72
0300 " 81700	27	1.02	22	27	22	22	,, 58	27	.70	27	.98	22	22	22	,, 59	27	22

The topside scantlings and decks before and abaft a bridge are to be determined by the vessel's proportions taken to the upper deck. These scantlings are to be maintained throughout the length of a "short" bridge, and are to be extended within the ends of a "long" bridge for a distance equal to one-third the breadth of the vessel.

The upper deck stringer angles in the above Table may be gradually reduced at the ends of the vessel to the size given in Table 17 for upper deck stringer angles at ends in way of erections.

TABLE 18. (See Continuation.)

LONGITUDI	NAL			130 01 67	эмз.	PROPO	ORTIC	ONS (OF L	ENGTH TO	DEPTH.					
NUMBER		Situ de	OF .	11 and under	12.							1	2 and unde	r 13.		
L×(B+		Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	Stringer An for $\frac{1}{2}$ lengt amidships	h	Stringer P for $\frac{1}{2}$ length amidship	gth	The Plate Deck Plate for $\frac{1}{2}$ less amids h	ating ngth	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	fo	ringer A or $\frac{1}{2}$ leng amidship	th	Stringer Plate for $\frac{1}{2}$ length amidships.	Tie Plates a Deck Plate for $\frac{1}{2}$ lens amidship
	daches	inches.	inches.	inches.		inches.		inche		inches.	inches.		inches.		inches.	inches.
$1400_{\mathrm{under}}^{\mathrm{and}}$	1650	.28	.24	$2\frac{1}{2} \times 2\frac{1}{2} \times$:24	18×	24	5 ×	.24	.30	.24		$\times 2\frac{1}{2}$	× ·28	$20 \times .26$	5 × 2
1650 "	1900	.30	22	" "	22	19	22	6	22	.32	27	3	$\times 3$	22	21 "	6,
1900 "	2150	"	·26	22 22	.26	20×		22	.26	"	.26	22	22	.30	22×·28	27 .6
2150 "	2400	•32	22	3×3	22	21	22	22	22	•34	,,	"	22	22	23 "	22 2
2400 "	2650	27	-28	22 22	.28	22×	28	22	.28	.36	.28	22	27	.32	24×·30	"
2650 ,,	2900	•34				92				.38	,,	"	22	"	25 "	"
2900 ,	3150		*30	27 27	.30	24×	30	27	.30		-30	27	22	•34	26×·32	22
3150 ,,	3500	.36		27 27		25		7	95	·40					27 "	7 ,
3500 ,,	3850	. 00	-32	22 22	.32	26×.	29	•	.32		32		27	.36	28×34	22
3850 "	4200	.38	02	22 22	02		- 50	27	02	•42		27	"		20	- //
	4600	•40	34	22 22	·34	$\frac{27}{28\times}$	21	27	·34	12	*34		"	.38	30×36	8 x :
4200 ,,		40	- 34	22 22	54		04	27	94	·44		27	" "	90	21	7000
4600 ,,	5000	27	22	22 22	22		27	8	27		.26		"	·40	$\frac{32 \times 38}{32 \times 38}$	27
5000 ,,	5400	•42	-36	27 27	.36	30×.	30	27	.36	•46	:36	22	27	40		9
5400 "	5800	•44	"	22 22	22	32	22	22	"	22	"	27	22	22	34 ,,	
5800 "	6300	22	.38	27 27	.38	34×	38	"	.38	•48	.38	$3\frac{1}{2}$	$\times 3\frac{1}{2}$	× ·42		"
6300 "	6800	•46	27	27 27	27		"	9	"	.50	22	22	22	27	38 "	10
6800 "	7300	22	•40	22 22	.40	38×.	40	22 .	•40	22	•40	27	22	•44	$40 \times \cdot 42$	27
7300 "	7900	.48	"	$3\frac{1}{2} \times 3\frac{1}{2}$	"	40	22	10	22	.52	.42	22	"	22	42 "	11
7900 "	8500	27	.42	27 27	.42	42×	42	11×	.42	22	22	22	22	22	44×·44	"
8500 ,,	9200	.50	22	22 22	22	44	22	22	22	.54	•44	22	22	.46	46 "	12
9200 "	9900	•52	•44	27 27	•44	46×		12×		.56	22	27	22	22	$48 \times \cdot 46$	27
	10600					48	22		"	22	•46	22	22	·48	50 ,,	13
. //	11400	.54	•46	27 27	·46			$\frac{7}{13}$ ×		.58			× 4	22	52×·48	22
1400 "				$\frac{\cancel{\cancel{0}}}{4\times4}$	Ti.	52				.60	·48			.50		14×:
2200 ,,	13100	.56	•48	39.	·48		.48	" 14×	.48	.62			27		43 ,,	Dk·30 for
3100 ,,	14100	.58	10	27 27		56	10	117	, 10	•64	.50		27	.52	//	1000
4100 ,,	15200	. 00	.50	. 27 27	27	43×	.50	27	99 for 1 T		.52	27	27		15	- //
			- 30	11 > 11	27	- 4 4				.66		77	$\times 4\frac{1}{2}$	27	16	00 Cmpl·30
.5200 ,,	17600	.60	27	$4\frac{1}{2} \times 4\frac{1}{2}$	22	4 ~	27	27	27	.68	.5.1			.54		
6400 ,,			.52	'22 22	.50	45	77	99 mpl 63)) O deek		.54	27	22	04	48 ,	02
7600 ,,	18800	22	27	27 27	22	46×	-				27)) -F.G		.34
.8800 ,	20100	64	.54	. 22 22	.52		22	.3	2	•72	.56	27	. 22	.56		_
20100 "	21500	.66	22	27 27	22	48	27	22		•74	"	22	22	22	$50 \times .56$	
21500 "	22900	27	.56	22 22	.54	_	22	.3	4	.76	.58	22	22	.58		.36
22900 "	24300	.68	.58	22 22	22	50×	.54	22		22	.60	27	"	.60		22
24300 "	25700	22	"	27 27	.56	51	22	.3	6	.78	27	22	22	22	$53 \times .58$.38
25700 "			.60	22 22	22	50	"	2	,	.80	.62	22	22	.62		22
27100 "			.62	27 27	22	F0	22	.3		.82	.64	22		22	55 ,,	•40
28500 "			27	27 27	22	54×		2		.84	.66		× 5		$56 \times .60$	22

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The upper deck stringer angles in the above Table may be gradually reduced at the ends of the vessel to the size given in Table 17 for upper deck stringer angles at ends in way of erections

TABLE 18.

HORSE			er sketchiste	PROPORT	TONS OF L	ENGTH T	O DEPTH.	and and	(See Contin	dation.)
LONGITUDINAL			11 and 10			1	0 021 1111			
NUMBER.			11 and 12.				1	12 and under 13.		
$L \times (B+D)$.	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	Stringer Angle for $\frac{1}{2}$ length Amidships.	Stringer Plate for $\frac{1}{2}$ length amidships.	Deck Plating for $\frac{1}{2}$ length amidships.	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	Stringer Angle for $\frac{1}{2}$ length amidships.	Stringer Plate for $\frac{1}{2}$ length amidships.	Deck Plating for $\frac{1}{2}$ length amidships.
00000 and 01000	inches.	inches.	inches.	inches,	inches.	inches.	inches.	inches.	inches.	inches.
29900 and 31300	.74	.64	$5 \times 5 \times .58$	$55 \times .56$	•40	.86	.68	$5 \times 5 \times 64$	$57 \times .60$.42
31300 , 32700	.76	.66	22 22 22	56 "	27	.88	.70	" " .66	58 "	22
32700 , 34100	22	27	,, ,, .60	$57 \times .58$	22	27	.72	22 22 22	$59 \times .62$	"
34100 , 35500	.78	.68	27 27 27	58 "	.42	.90	.74	" "	60 ,,	.44
35500 ,, 36900	22	.70	" " .62	59 ,,	27	.92	22	" " ·70	61. "	22
36900 , 38300	.80		22 22 22	$60 \times .60$	27		.76	22 22 22	$62 \times \cdot 64$	"
38300 " 39700	.82	.72	" " ·64	61 ,,	•44	.94	.78	" " .72	63 "	.46
39700 ,, 41100	22	·74	22 22 22	62 ,,	22	.96	.80	22 22 22	64 "	22
41100 ,, 42500	.84	22	27 27 27	$63 \times .62$	27	27	22	" " .74	$65 \times .66$	22
42500 ,, 43900	.86	.76	27 27 27	64 ,,	.46	.98	.82	27 27 27	66 ,,	.48
43900 , 45300	22	.78	" " "66	65 "	22	1.00	·84	" " .76	2at48 ·68	27
45300 ,, 46700	.88	22	27 27 27	$66 \times \cdot 64$	22	1.02	.86	22 22 22	" " .70	22
46700 ,, 48100	.90	.80	" " .68	2at48 ,,	.48	1.04	.88	6 × 6 "	,, 49 ,,	.50
48100 , 49500	22	.82	22 22 22	" " .66	22	22	.90	,, ,, .78	" " .72	27
49500 , 50900	.92	27	.70	" 49 "	22	1.06	.92	27 27 27	"50 "	22
50900 , 52300	.94	·84	6 × 6 ,,	" " .68	.50	1.08	•94	27 27 27	" " ·74	.52
52300 , 53700	22	.86	" " .72	2 50 ,	22	27	-96	,, ,, .80	,, 51 ,,	27
53700 , 55100	.96	22	27 27 27	" " ·70	.52	1.10	.98	27 27 27	;; ;; ·76	
55100 , 56500	.98	.88	27 27 27	" 51 "	22	1.12	1.00	27 27 27	<u>,, 52</u> ,,	.54
56500 ,, 57900	27	.90	27 27 27	" " ·72	.54	27	1.02	" " ·82	;; ;; ·78	100000
57900 , 59300	1.00	22	" " .74	, 52 ,,	22	1.14	1.04	// //	53	.56
59300 , 60700	1.02	-92		,, .74	.56	1.16	1.06	$\frac{\cancel{\cancel{7}}}{\cancel{7}} \times \cancel{\cancel{7}} \qquad \cancel{\cancel{\cancel{7}}}$.90	THE RESERVE TO SERVE
60700 , 62100	1.04	.94		,, 53 ,,		1.18	1.08	" " ·84	54	.58
62100 , 63500	1.06		7 × 7 ,,	,, ,, .76	.58	1.20	1.10	// //	.29	
63500 , 64900		-96	.78	$,54 \times .78$		·90pbld.	.86		$\frac{,,}{,}$ $\frac{,}{,}$ $,$.60
64900 , 66300	1.08	.98		22 22 22	-60	.92 "	.88	27 27 27	22 22 22	.62
66300 , 67700	1.10		.80	$\frac{55 \times 80}{100}$			-90		$\frac{,56 \times .86}{,}$	
67700 , 69100	27	1.00		,, ,, .82	.62	94 ,,		" " " " ·86	" " ·88	·64
69100 , 70500	1.12	1.02	27 27 27 27 27 27	, 56 ,	.64	.96 "	.92	8 × 8	57	.66
70500 , 71900	1.14						•94	.99	00	
71900 , 73300	22	1.04	" " "	", " ·84 "57×·86	.66	98 ,,		// //	" " ·90 "58×·92	.68
73300 , 74700	1.16	1.06	0 0		.68	1.00 "	.96	., ., .90		·70
74700 ,, 76100	1.18			,58×·88			•98	// //	"""" "59×·94	.72
76100 , 77500		1.08		.00	.70	1.02 ,,		, , , 92	0.0	
77500 , 78900	" 1·20	1.10			.72	1.04 "	1.00		// //	.74
78900 , 80300	·90 Dbld	.90		, 59 ,,			1.02	" " " " " · 94	,, 60 ,,	74
80300 , 81700	·92 ,,		27 27 27	" " .92 60 × .94	.74	1.06			" " ·98 "61×1·00	76
,, 01/00	97	27	27 27 27 :	$,60 \times .94$	7 ±	1.06 ,,	27	27 27 27	"01 × 1 0 C	10

The topside scantlings and decks before and abaft a bridge are to be determined by the vessel's proportions taken to the upper deck. These scantlings are to be maintained throughout the length of a "short" bridge, and are to be extended within the ends of a "long" bridge for a distance equal to one-third the breadth of the vessel.

The upper deck stringer angles in the above Table may be gradually reduced at the ends of the vessel to the size given in Table 17 for upper deck stringer angles at ends in way of erections.

TABLE 18.

(See Continuation.)

TONG	ITUDIN	TAT		PROPORTI	ONS OF LENGTH	H TO DEPTI	н.		NESS OF	THICK- NESS OF	BEAM STRINGERS	THICK- NESS OF DECK
	MBER.		SI de i		13 and 14.			UNDER	"LONG"	SHEER- STRAKE AND	AT ENDS OF UPPER, AWNING OR	PLATING AT ENDS
	(B+[Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	Stringer Angle for $\frac{1}{2}$ length amidships.	Stringer Plate for $\frac{1}{2}$ length amidships.	Tie Plates and Deck Plating for $\frac{1}{2}$ length amidships.	Stringer Plate.	Tie Plates and Deck Plating.	STRAKE BELOW AT ENDS.	SHELTER DECKS, ALSO THICKNESS OF TIE PLATES AT ENDS.	UPPER, AWNING OR SHELTER DECKS.
Total L			inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.
1400	and under	1650	.32	.24	$3 \times 3 \times 32$	22×·28	6×28	.22	.22	.24	10×22	
1650	22	1900	•34	22	27 27 27	23 "	27 27	"	"	,,	11 "	
1900	22	2150	.36	.26	" " 34	24×30	,, 30	·24	·24	,,	" ·24	
2150	22	2400	.38	22	27 27 27	25 "	27 27	27	27	,,,	27 27	
2400	22	2650	•40	.28	" " 36	26×32	" ·32	"	22	.26	12 "	18101
2650	27	2900	" "	,,	27 27 27	27 ,,	27 27	.26	.26	"	,, .26	000
2900	22	3150	•42	.30	" " 38	28×34	7×34	27	27	"	27 27	
3150	27	3500	•44	"	22 22 22	29 "	22 22	27		"	13 "	
3500	22	3850	"	·32	" " .40	$30 \times .36$	" 36	.28	.28	.28	" ·28	-0101
3850	"	4200	•46	22	22 22 22 32 4	31 "	22 22	"	"	,,	27 27	000
4200	22	4600	•48	•34	$3\frac{1}{2} \times 3\frac{1}{2} \times 42$	32×·38	8 × ·38	22	27	.30	14 "	
4600	22	5000	22	.36	22 22 22	33 "	" "	.30	.30	,,	,, 30	
5000	27	5400	.50	"	" " ·44	34×40	$9 \times \cdot 40$	27	"	.32	22 22	1000
5400		5800	.52	-38	27 27 27	36 "	22 22	27	27	,,	15 "	11911
5800	"	6300		•40	" " 46	38 × ·42	10×42	.32	.32	•34	" ·32	100
6300	"	6800	.54			40 ,,	27 27	27	"	,,	16 "	
6800	"	7300	.56	•42	.48	42×44	11×·44	"	27	.36	27 27	
7300	27	7900		•44		44 ,,		•34	•34	,,	17 ,,	
7900	22	8500	.58			46×46	$\frac{"}{12\times \cdot 46}$	27	"	1,	27 27	
8500	"	9200	.60	·46		48 ,,		"	22	,,	18×34	
9200	" .	9900	62	•48	$\frac{"}{4\times4\times52}$	$50 \times .48$	$\frac{"}{13\times \cdot 48}$	•36	-36	.38	19 ,,	
9900	27	10600	64		and a series	$42 \times \cdot 48$	Dk.30 for 1/2L.	.36	Dk. 30 pltg	,,	20 ,,	
10600	- 22	11400	.66	.50	" " " " ·54	43×50	-	.38			21 ",	1000
11400	22	12200	68	•52	. //	11	27 27	•40	- 27	"	22×36	
$\frac{11400}{12200}$	22	13100	•70	•54	" " <u>"</u>	$45 \times .52$	Cmpl·30deck	•42	- 27	40	23 "	.30
	22			04	$\frac{,}{4\frac{1}{2} \times 4\frac{1}{2}} \frac{,}{,}$	46 ,	Ompi Odeck	•44	- 27		24 ,,	22
13100	27	$\frac{14100}{15200}$.56	.58		32		. 22	,,	25 ,,	22
$\frac{14100}{15200}$	"	$\frac{13200}{16400}$	-	•58		10	•34		- 27	"	26×38))
	"	$\frac{10400}{17600}$		-60	" " " · · · · · · · · · · · · · · · · ·))	- 27	,,	97	
16400	27		1	-	11 11		38	27	- 27	,,	28	27
17600	22	18800		.69	22 22 22	//		·46	27	.42	90))
18800	22	20100	1	·62.	" " "	$51 \times .58$	//	40	- 27		30×40	27
20100	22	21500	1	.64	,, ,, .62		•40	27	"	"	21	- 27
21500	,,,	22900	-1	.66	27 27 27 27	$53 \times .60$	27	- 27	- "	"	29	- 27
22900		24300	- 6	"	" " ·64		,40	27	.29	•44	//	-32
24300		25700		.68	77 77 77	$55 \times .62$	•42	27	.32	11	33×42	-
25700		27100		•70	<u>"</u> " .66	//	"))		7,7))
27100		28500	-1	.72	5×5 ,	$57 \times .64$		"	.34	22	34 ,,	27
28500	22	29900	.96	.74	27 27 27	58 "	•44))	22	"	34 "	27

The topside scantlings and decks before and abaft a bridge are to be determined by the vessel's proportions taken to the upper deck. These scantlings are to be maintained throughout the length of a "short" bridge, and are to be extended within the ends of a "long" bridge for a distance equal to one-third the breadth of the vessel.

The upper deck stringer angles in the above Table may be gradually reduced at the ends of the vessel to the size given in Table 17 for upper deck stringer angles at ends in way of erections.

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TOPSIDE PLATING, DECK and STRINGER PLATES at UPPER, AWNING or SHELTER DECKS, and "LONG" BRIDGES.

TABLE 18.

(Concluded.)

LONGITUDINAL		PROPORTIO	ONS OF LEN	GTH	TO DEPTH	Н.		NESS OF R DECK	THICK- NESS OF	STRIN	AM	THICK-
NUMBER.			13 and under	14.			UNDER	"LONG"	SHEER- STRAKE	OF U AWNI	ENDS PPER, NG OR	DECK PLATIN AT END OF
$L \times (B+D)$.	Sheerstrake for $\frac{1}{2}$ length amidships.	Strake below Sheerstrake for $\frac{1}{2}$ length amidships.	Stringer Angl for $\frac{1}{2}$ length amidships.		Stringer Plate for 1 length amidships.	Deck Plating for $\frac{1}{2}$ length amidships.	Stringer Plates.	Deck Plating.	AND STRAKE BELOW AT ENDS.	DECKS THICK! TIE P	LTER S, ALSO NESS OF LATES ENDS.	UPPER AWNING OR SHELTE DECKS.
	inches,	inches.	inches.	0.0	inches.	inches.	inches.	inches.	inches.	30466534655	hes.	inches.
29900 and 31300	.98	.76	5×5	.68	$59 \times .64$	·44	•48	•36	•44		× ·42	•34
31300 , 32700	1.00	.78	27 27	"	$60 \times .66$	22	27	27	"	35	× ·44	27
32700 , 34100	1.02	.80	22 22	.70	61 "	•46	22	"	.46	22	"	27
34100 " 35500	1.04	.82	22 22	"	62 "			.38	,,	36	22	27
35500 , 36900	1.06	·84	27 27	"	$63 \times .68$		27		,,,		. ,,	.36
36900 " 38300	1.08	.86	22 22	.72	64 ,,	22	27	27	,,	37	27	27
38300 , 39700	1.10	.88	22 22	"	65 "	.48	27	•40	,,	22	"	22
39700 , 41100	1.12	.90	22 22	22	$66 \times .70$	22	.50	27	.48	22	22	22
41100 , 42500	1.14	.92	27 27	.74	$2at48 \times .72$	27	27	"	,,	38	22	22
42500 ,, 43900	1.16	.94	6×6	27	" " ·74	.50	27	22	7,7	22	22	22
43900 , 45300	1.18	.96	22 22	"	,, 49 ,,	27	27	.42	22	22	27	27
45300 , 46700	1.20	.98		.76	,, ,, .76	27	27	22	,,	39	22	27
46700 , 48100	•90Dbld.	·82	27 27	22	, 50 ,	.52	22	27	.50	27	27	"
48100 , 49500	22 22	27	27 27	22	" " ·78	22	.52	22	,,	22	·46	22
49500 , 50900	•92	·84		.78	" 51 "	22	27	27	,,	40	27	22
50900 , 52300	22 22	-86			.80	•54	27	27	,,	"	22	27
52300 , 53700	.94 ,,	22	27 27	·80	52	22	27	•44	,.	27	22))
53700 " 55100	.96 ,,	.88			.89	.56	"	"	•52	41	27	38
55100 , 56500	/	.90	$\frac{n}{7} \times 7$	27	53		27	27	22	27	22	22
56500 57900	.98 ,,			.82	.81	.58	.54		"			22
57900 , 59300	1.00 "	.92			54			·46	27	42	22	
59300 60700		•94		27	.86	.60	27					27
60700 , 62100	1.02 "		27 27	·84	55	-62	- 27	27	•54))	27
62100 62500	1.04 "	.96			.88			"		$\frac{7}{43}$ ×	.48	27
63500 , 64900		.98	27 27	.86	$\frac{3}{56} \times 90$.64		·48	- ;;			27
64900 , 66300	1.06 "					-66	.56		.56		27	27
66200 67700	1.08 "	1.00	8 V 8		$\frac{"}{,57 \times .92}$					44	"	
67700 60100	27 27	1.02		00	0.1	·68		.50	- ''	7	27	- 27
00100 70500	1.10 "				" " ·94 " 58 "	-70	27		"	22	"	27
70500 71000	1.12 "	7.04			.00		.58			45	27	•40
71000 70000		1.06		<u>"</u>	11 11	.72		.52	.58		.50	
79900 74700	"" 1·14 "				59×98	.74	27			"		27
74700 70100	1.16 "	1.08		"	" " " 60×1:00		.60	22	22	27	"	27
76100 77500					$\frac{,,60\times1.00}{1.02}$.76		.54				27
77500 70000	" " " 1.10	1.10	27 27		,, 1.02		22	94		10	27	27
79000 90900	1.18 ,,	77		22	<u>" 61 "</u>	.78	.69	27	<u>"</u>	22	"	27
78900 , 80300	1.20 "	1.12		22	,, 1.04	.20	.62	.56	- 00	22	27	
80300 ,, 81700	27 22	1.14	27 22	94	$,62\times1.06$.80	27	.56	27	27	22	27

The topside scantlings and decks before and abaft a bridge are to be determined by the vessel's proportions taken to the upper deck. These scantlings are to be maintained throughout the length of a "short" bridge, and are to be extended within the ends of a "long" bridge for a distance equal to one-third the breadth of the vessel.

The upper deck stringer angles in the above Table may be gradually reduced at the ends of the vessel to the size given in Table 17 for upper deck stringer angles at ends in way of erections.

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	-					
	inches.	inches.		inches.	inches.	inches.
Thickness of Plates	·22	·34	·48	·66	·88	1·14 to
THICKNESS OF FLATES	under ·34	under ·48	under '66	under ·88	1.14	1.20
Diameter of Rivers	. 5	$\frac{3}{4}$	7/8	1	$1\frac{1}{8}$	$1\frac{1}{4}$
Breadth of QUADRUPLE riveted BUTT STRAPS in inches			22	25	$28\frac{1}{4}$	$31\frac{1}{2}$
Breadth of TREBLE riveted BUTT STRAPS in inches		$14\frac{1}{4}$	$16\frac{3}{4}$	19	$21\frac{1}{2}$	24
Breadth of Double riveted Butt Straps in inches	8	$9\frac{3}{4}$	$11\frac{1}{4}$			
Breadth of Single riveted Butt Straps in inches	$4\frac{1}{2}$	$5\frac{1}{4}$				
Breadth of QUADRUPLE riveted BUTT LAPS in inches			12	14	16	18
Breadth of TREBLE riveted BUTT LAPS in inches		$7\frac{1}{2}$	9	$10\frac{1}{2}$	12	$13\frac{1}{2}$
Breadth of Double riveted Butt Laps in inches	$4\frac{1}{4}$	5	6			
Breadth of Single riveted Butt Laps in inches	$2\frac{1}{2}$	3				
Breadth of TREBLE riveted Edge Laps in inches				81/2	$9\frac{1}{2}$	$10\frac{1}{2}$
Breadth of Double riveted Edge Laps in inches	33	$4\frac{1}{2}$	$5\frac{1}{4}$	6	$6\frac{3}{4}$	$7\frac{1}{2}$
Breadth of Single riveted Edge Laps in inches	$2\frac{1}{4}$	$2\frac{1}{2}$	3			
3½ diam. Eeam Stringer Plates (except quadruple riveted butt laps)	$2\frac{1}{4}$	$2\frac{5}{8}$	31/8	$3\frac{1}{2}$	4	438
In Edges of Outside Plating (forward and aft) Quadruple Riveted Butt Laps and Double Butt Straps: Butts of Deck Plating, Butts of Margin Plates, Girders, Tie Plates, and Floor Plates; also Butts and Edges of Inner Bottom Plating	$2\frac{1}{2}$	3	$3\frac{1}{2}$	4	$4\frac{1}{2}$	5
In Gunwale Angle Bars, Margin Plate Angles, Edges and Butts of Bulkhead Plating, Angles connecting Side Stringers to Web Frames and Edges of Deck Plating.	$2\frac{3}{4}$	$3\frac{3}{8}$	4	$4\frac{1}{2}$		
In Flat Keel Angles, Vertical Angles connecting Floors and Centre Girder. Bulkhead Frames where caulked, Butts and Edges of Mast Plates, Floors and cross ties in after peak	318	$3\frac{3}{4}$	$4\frac{3}{8}$	5	$5\frac{5}{8}$	$6\frac{1}{4}$
of diam. In Deck Plating to Beams where single to to c. Iflange beams are fitted at alternate frames	$3\frac{3}{4}$	$4\frac{1}{2}$	514			
In °Frames, Reversed Frames, Floors, Keelsons, Beam Angles, Deck and Hold Stringer Angles, Face Angles on Web Frames and Side Stringers, Bulkhead Stiffeners, Longitudinal Angles on continuous Girders, Vertical Angles connecting Floors and Side Girders, and Deck Plating to beams except where single flames	$4\frac{1}{2}$	$5\frac{1}{4}$	614	7		

Mistale	THICK	NESS OF BUT	T STRAPS.	Thick-	THICK	NESS OF BUT	TSTRAPS
Thick- ness	3000	Doul	ole.	ness	-	Dou	ble.
of Plates.	Single.	Strapwhich is Counter- sunk for Rivets.	Strap on opposite side of Plate.	ot Plates.	Single.	Strapwhich is Counter- sunk for Rivets.	Strap on opposite side of Plate.
·22	inches.	inches.	inches.	inches.	inches.	inches.	inches.
.24	.24			.74	.94	.54	27
.26	.26			.76	.96	.56	.46
.28	.28			.78	.98	.58	.48
.30	.30	- 19		.80	1.00	,,	.50
.32	•34			.82	1.04	.60	"
.34	.38			.84	1.06	22	.52
.36	•40	189		.86	1.08	.62	22
.38	•44			.88	1.10	22	.54
.40	•48			.90	1.12	.64	.56
.42	.52			.92	1.16	22	.58
.44	.54	.34	.28	.94	1.18	.66	.60
.46	.58	.36	27	.96	1.20	22	.62
.48	.60	.38	.30	.98	1.22	.68	22
.50	-62	•40	22	1.00	1.24	22	.64
.52	.64	22	.32	1.02	1.28	.70	22
.54	-68		22	1.04	1.30	22	.66
.56	-70	22	•34	1.06	1.32		22
.58	.74		22	1.08	1.34	"	.68
.60	.76	27	.36	1.10	1.38	-	"
.62	.78	-	27	1.12	1.40	22	.70
.64	.80	27	.38	1.14	1.44		"
.66	.82		•40	1.16	1.46	27	.72
.68	86	27	.42	1.18	1.48	.78	22
.70	-88		11	1.20	1.50	27	.74

 \dagger In butts connected by single butt straps alternate rivets may be omitted in the back row of treble riveting when the longitudinal number is 16,000 and under; when above this number, the rivets in the back row are not to be more than 5 to 5½ diameters apart from centre to centre. All overlapped butts are to have complete rows of rivets.

 $^{\circ}$ The rivets attaching the outside plating to the frames are to be spaced not more than 6 diameters apart from centre to centre where the depth of framing is 11 inches and above, and throughout the vessel where the rule frame spacing is 26 inches and above. Where the framing consists of channel bars with reversed frames the rivets attaching the outside plating to the frames are to be spaced not more than $5\frac{1}{2}$ diameters apart from centre to centre.

Where the framing is in accordance with the requirements of Table 2, the rivets attaching the reversed frames to the frames are to be spaced the same as the rivets through the frames and outside plating.

In deep water ballast tanks and in fore and after peak tanks, the rivets through the frames and outside plating are to be spaced not more than $5\frac{1}{2}$ diameters apart from centre to centre.

Before the three-fifths lengths of a steamer having a tonnage co-efficient of 76 or having a full form at the fore part, the rivets in the frames and plating forming the flat of the bottom are to be spaced not more than 5½ diameters apart from centre to centre.

Rivets to be \$\frac{1}{2}\$ of an inch larger in diameter in the Stem, Stern Frame, and Keel, but in no case need these exceed \$1\frac{1}{2}\$ inches in diameter, and to be spaced 5 diameters apart from centre to centre. In single screw steamers above \$50 feet in length, the after lengths of shell plating are to be connected to the portion of the stern frame below the boss with three rows of rivets.

For diameter and spacing of rivets in Rudders, see Table 24.

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NUMBER of RIVETS IN EDGES of Plating between Frames Amidships, excluding Rivets in Frames.

		NU	IMB	ER	OF		SIZE OF COUNTERSINK FOR RIVETS IN OUTSIDE PLATING.
			IVE				Ins.
		EA	CH	R	ow.		$\frac{5}{8}$ Rivet
	ins. ·22	ins. ·34	ins48	ins.		ins. 1·14	$ \begin{array}{cccc} & & & & & & & \\ & & & & & & \\ & & & & &$
Thickness of PLATES	under	and under ·48	and under .66	and under ·88	and under 1.14	to 1.20	
Diameter of RIVETS	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	1	$1\frac{1}{8}$	$1\frac{1}{4}$	Rivet
Spacing of FRAMES 20 ins.	7	5					< 18 ^j >
", ", $20\frac{1}{2}$ ",	7	6					$\leftarrow1\frac{16}{16}$
" " " 21 "	7	6	5				
$, , , , 21\frac{1}{2},$	1	6	5				Rivet
" " " 22 "	-	6	5				
" " " 22½ "	_	6	5				150
" " " 23 "		6	5	5			< 1 ₁₆ >
$"$ $"$ $"$ $23\frac{1}{2}$ $"$	1-	7	6	5			
,, ,, ,, 24 ,,	-	7	6	5			Rivet
$"$ $"$ $"$ $24\frac{1}{2}$ $"$	-		6	5			Three districts of the second
" " " 25 "	-		6	5			111111111111111111111111111111111111111
251	-		7	6			$1\frac{19!}{16} - \cdots \rightarrow$
26	-		7	6	5		
261	-1		7	6	5		118
27	-		7	6	5		Rivet
971	-	-	7	6	6		
28	-	-	7			5	13"
281			8	7	6	5	415 "
29	1	•••	8	7	6	5	116
291	-	••••	8	7	6	5	VIIII
30		• • • •	8	7	6	5	
	-	••••		7	6	6	$\frac{1_{\frac{1}{4}}}{\text{Rivet}}$
${}$, , , ${}$, ${}$ 30 $\frac{1}{2}$, , , ${}$ 31 ,		•••	•••	7	6	6	
	-	-	••••	8	7	6	
$\frac{1}{1}$, $\frac{1}{1}$, $\frac{1}{1}$		•••	•••	8	7	6	15"
	-	•••	•••	-	_		The countersink is to extend through the whole thickness of the plate when less than '60 of an inch in thickness; when '60 of
$\frac{n}{2}$ $\frac{n}{2}$ $\frac{n}{2}$ $\frac{32\frac{1}{2}}{2}$	1	• • • •	•••	8	7	6	an inch or above, the countersink is to extend through nine-tenths the thickness of the plate.
,, ,, ,, 33 ,,	1	,		8	7	6	Similar and the second

FORM OF RIVET TO BE USED IN OUTSIDE PLATING.

In single riveted seams one frame rivet is to be fitted through the landing edges at each frame. In double riveted seams one frame rivet is to be fitted through the landing edges at each frame, except where the frames or the edges of the outside plating are joggled when two rivets are to be fitted. In treble riveted seams two frame rivets (the upper and lower)

the thickness of plate in which it is intended to be used.

Where the fore and aft flange of the frame does not exceed 3 inches, the rivets attaching the outside plating thereto should not exceed $\frac{1}{8}$ inch in diameter, and where it is $3\frac{1}{2}$ inches wide, they should not exceed 1 inch in diameter.

are to be fitted through the landing

edges at each frame.

There are to be at least four rivets in each flange of the angle bars between the frames, which connect the stringer plates and intercostal plates to the outside plating, where the frames are spaced less than 26 inches apart; where the spacing is 26 inches and less than 30 inches there are to be five rivets in each flange; and where the spacing is 30 inches and not more than 33 inches there are to be six rivets in each flange.

The rivets in the beam knees are to be in number and size as required by Section 20, paragraph 14.

The rivets in the vertical angles connecting floors and outside brackets to margin plates are to be in number and size as required by Table 9.

The rivets in the connecting straps for web frames and side stringers are to be in number and size as required by Table 5.

	39				1	THICKNESS O	F PLATES.					
	·22 and under ·30	·30 and under ·36	·36 and under ·42	·42 and under ·48	·48 and under ·54	·54 and under ·60	·60 and under ·68	·68 and under ·76	.76 and under .84	·84 and under ·94	·94 and under 1·04	1.04 and under 1.20
a	Double.	Double.	Treble.	Treble.	Treble.	Treble.	Quadruple.	Quadruple.	Quadruple.	Double straps treble riveted.	Double straps treble riveted.	Double strap treble riveted
ь	"	22	- "	27	"	27	27	27	22	Quadruple.	Quadruple.	27
c	22	"	Double.	22	22	27	Treble.	Treble.	"	27	. 22	Quadruple.
d	"	27	27	"	"	"	22	Quadruple.	27	27	22	
e	- 27	"	"	Double.	2)	27	27	- 27	27	"	22	-
f	Single.	Single.	Single.	27	Double.	22	27	27	27			
g	27	22 .	Double.	27	27	Double.	Double.	Double.	Double.	Double.	Double.	10 100,000,00
h	27	22	Single.	Single.	27	22	27	27	27	Treble.	Treble.	37
i	27	27	22	27	Single.	27	27	27	27			
k	22	22	22	Double.	Double.	27	"	"	27			
ı	22	22	22	Single.	27	27	22	"				

The requirements as to attachments are to be regulated by the thicker of the plates connected.

The edge attachments all fore and aft of outside plating and middle line strake of inner bottom plating are to be regulated by the thickness of the plating amidships.

Where the breadth of any strake of outside plating exceeds the limits given in the following Table, additional riveting is to be provided at the butts in excess of that required by the thickness of the plates.

Butts of side plating of "short" deck erections should

be not less than double riveted.

a. Butts of sheerstrake, strake below and stringer plates, of the uppermost deck, whether upper, awning or shelter deck or "long" bridge, for half the vessel's length amidships.

Where the sheerstrake is doubled, single butt straps treble riveted are to be fitted to the butts of the sheerstrake and doubling plate, of the same thickness as the plates connected.

Butts of outside plating from keel to upper turn of bilge for half the vessel's length amidships.

Butts of boss plates.

Butts of centre girder plates in double bottoms.

Butts of floor plates and web frame plates.

b. Butts of flat keel plates for half the vessel's length amidships.

Where the flat keel plates are doubled, single butt straps treble riveted are to be fitted to the butts of the keel plate and doubling plate, of the same thickness as the plates connected.

- c. Butts of flat keel plates at ends of vessel.
- d. Butts of outside plating from upper turn of bilge to strake below sheerstrake.

Butts of outside plating from keel to upper turn of bilge at ends of vessel.

Butts of sheerstrake, strake below and stringer plates of upper and awning or shelter decks at ends of vessel.

Butts of beam stringer plates of 2nd decks and decks or tiers of beams below.

Butts of tie plates.

Butts of margin plates and middle line strake of double bottoms for half the vessel's length amidships.

Butts of vertical keelson plates, rider plates, and foundation plates.

DEPTH (D) OF VESSEL.	MAXIMUM BREADTH OF STRAKE FOR RULE RIVETING.
Feet.	Inches.
Not exceeding 20	54
Above 20 and ,, ,, 24	60
,, 24 ,, ,, ,, 28	66
,, 28	72

e. Butts of deck plates for half the vessel's length amidships. Butts of inner bottom plating for half the vessel's length amidships. Butts of side girders in double bottoms.

Butts of margin plates and middle line strake of double bottoms at ends of vessel.

f. Butts of deck plates at ends of vessel.

Butts of inner bottom plating at ends of double bottoms.

g. Edges of outside plating from keel to upper turn of bilge.

Joining seams of stringer plates where the stringer is fitted in two breadths.

h. Edges of outside plating from upper turn of bilge to strake below sheerstrake.

The edges of sheerstrakes are to be double riveted except where the thickness of the side plating is '84 of an inch or above,

when they are to be treble riveted.

In vessels of 480 feet in length and where the thickness of the side plating is less than '84 inch, the landing edges are to be treble riveted for one-fourth of the vessel's length in the fore and after bodies for a depth of one-third the depth of the vessel, the actual position of this treble riveting to depend upon the arrangement of shell plating and the special design of the vessel, or other equivalent strengthening to be afforded. Vessels of from 450 feet to 480 feet in length are to be additionally riveted at the before mentioned parts proportionately to their length, or to have other equivalent strengthening. Each case requiring this additional riveting of the seams is to be submitted for the approval of the Committee. Where the thickness of the side plating is 84 inch or above, the edges are to be treble riveted for four-fifths of the vessel's length amidships.

i. Edges of deck plates.

k. Edges of middle line strake of inner bottom plating.

1. Edges of inner bottom plating except middle line strake.

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	SPEED OF VESSEL IN KNOTS PER HOUR. 米米										
A × D*	Under 10	$10_{ m under}^{ m and} 12$	$12_{\mathrm{under}}^{\mathrm{and}}14$	14 and 16	16 and 18	$18_{ m under}^{ m and}20$	20 and under 22				
	DIAMETER OF RUDDER HEAD IN INCHES.										
22 and 28	$2\frac{3}{4}$	3	$3\frac{1}{4}$	$3\frac{1}{2}$	4	$4\frac{1}{2}$	5				
28 and under 34	3	$3\frac{1}{4}$	$3\frac{1}{2}$	$3\frac{3}{4}$	$\frac{41}{4}$	$\frac{4^{3}}{4}$	$5\frac{1}{4}$				
34 and under 40	$3\frac{1}{4}$	$3\frac{1}{2}$	$3\frac{3}{4}$	4	$\frac{41}{2}$	5	$5\frac{1}{2}$				
40 and 47	$3\frac{1}{2}$	$3\frac{3}{4}$	4	$4\frac{1}{2}$	5	$5\frac{1}{2}$	6				
47 and under 55	$3\frac{3}{4}$	4	$4\frac{1}{4}$	$4\frac{3}{4}$	$5\frac{1}{4}$	$5\frac{3}{4}$	$6\frac{1}{4}$				
55 and under 64	4	$4\frac{1}{4}$	$\frac{41}{2}$	5	$5\frac{1}{2}$	6	$6\frac{1}{2}$				
64 and 73	$\frac{41}{4}$	$4\frac{1}{2}$	$4\frac{3}{4}$	$5\frac{1}{4}$	$5\frac{3}{4}$	$6\frac{1}{4}$	$6\frac{3}{4}$				
73 and 83	$4\frac{1}{2}$	$4\frac{3}{4}$	5	$5\frac{1}{2}$	6	$6\frac{1}{2}$	7				
83 and under 94	$4\frac{3}{4}$	5	$5\frac{1}{2}$	6	$6\frac{1}{2}$	7	$7\frac{1}{2}$				
94 and under 105	5	$5\frac{1}{4}$	$5\frac{3}{4}$	$6\frac{1}{4}$	$6\frac{3}{4}$	$7\frac{1}{4}$	$7\frac{3}{4}$				
105 and 117	$5\frac{1}{4}$	$5\frac{1}{2}$	6	$6\frac{1}{2}$	7	$7\frac{1}{2}$	8				
117 and 130	$5\frac{1}{2}$	$5\frac{3}{4}$	$6\frac{1}{4}$	$6\frac{3}{4}$	$7\frac{1}{4}$	$7\frac{3}{4}$	81/4				
130 and under 144	$5\frac{3}{4}$	6	$6\frac{1}{2}$	7	$7\frac{1}{2}$	8	$8\frac{1}{2}$				
144 and 160	6	$6\frac{1}{4}$	$6\frac{3}{4}$	$7\frac{1}{4}$	$7\frac{3}{4}$	$8\frac{1}{4}$	9				
160 and 176	$6\frac{1}{4}$	$6\frac{1}{2}$	7	$7\frac{1}{2}$	8	$8\frac{1}{2}$	$9\frac{1}{4}$				
176 and 192	$6\frac{1}{2}$	$6\frac{3}{4}$	$7\frac{1}{4}$	$7\frac{3}{4}$	$8\frac{1}{4}$	$8\frac{3}{4}$	$9\frac{1}{2}$				
192 and under 209	$6\frac{3}{4}$	7	$7\frac{1}{2}$	8	$8\frac{1}{2}$	$9\frac{1}{4}$	10				
209 and under 227	7	$7\frac{1}{4}$	$7\frac{3}{4}$	81/4	$8\frac{3}{4}$	91	$10\frac{1}{4}$				
227 and under 246	$7\frac{1}{4}$	$7\frac{1}{2}$	8	$8\frac{1}{2}$	9	$9\frac{3}{4}$	$10\frac{1}{2}$				
246 and 268	$7\frac{1}{2}$	$7\frac{3}{4}$	$8\frac{1}{4}$	83/4	$9\frac{1}{4}$	10	$10\frac{3}{4}$				
268 and under 290	$7\frac{3}{4}$	8	$8\frac{1}{2}$	9	$9\frac{1}{2}$	$10\frac{1}{4}$	11				
290 and 335	8	81/2	9	$9\frac{1}{2}$	10	$10\frac{1}{2}$	$11\frac{1}{2}$				
335 and under 390	$8\frac{1}{2}$	9	$9\frac{1}{2}$	10	$10\frac{1}{2}$	$11\frac{1}{2}$	$12\frac{1}{2}$				
390 and 445	9	$9\frac{1}{2}$	10	$10\frac{1}{2}$	11	12	13				
445 and under 505	$9\frac{1}{2}$	10	$10\frac{1}{2}$	11	12	13	14				
505 and under 570	10	$10\frac{1}{2}$	11	$11\frac{1}{2}$	$12\frac{1}{2}$	$13\frac{1}{2}$	$14\frac{1}{2}$				
570 and under 640	$10\frac{1}{2}$	11	$11\frac{1}{2}$	$12\frac{1}{2}$	$13\frac{1}{2}$	$14\frac{1}{2}$	$15\frac{1}{2}$				
640 and mider 720	11	$11\frac{1}{2}$	12	13	14	15	16				
720 and under 800	$11\frac{1}{2}$	12	$12\frac{1}{2}$	$13\frac{1}{2}$	$14\frac{1}{2}$	$15\frac{1}{2}$	$16\frac{1}{2}$				
800 and under 890	12	$12\frac{1}{2}$	13	14	15	16	17				
890 and under 980	$12\frac{1}{2}$	13	$13\frac{1}{2}$	$14\frac{1}{2}$	$15\frac{1}{2}$	$16\frac{1}{2}$	$17\frac{1}{2}$				
980 and 1080	13	$13\frac{1}{2}$	$14\frac{1}{2}$	$15\frac{1}{2}$	$16\frac{1}{2}$	$17\frac{1}{2}$	$18\frac{1}{2}$				
1080 and under 1180	$13\frac{1}{2}$	14	15	16	17	18	19				
1180 and 1290	14	$14\frac{1}{2}$	$15\frac{1}{2}$	$16\frac{1}{2}$	$17\frac{1}{2}$	$18\frac{1}{2}$	$19\frac{1}{2}$				
1290 and 1400	$14\frac{1}{2}$	15	16	17	18	19	20				

^{*} A is the total rudder area abaft the centre line of the pintles in square feet, and D is the distance in feet of its centre of gravity abaft the centre line of the pintles.

^{**} The diameters of rudder heads of sailing vessels are to be as required for vessels with a speed of less than 10 knots per hour.

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DONG Sine Proce	Chains an	Equipment for	r	SAIL	ING	AND	STE	EAM	TRA	WLE	ERS	Al	ND	TUG	àS.	†				
REGISTE		LONGITUDINAL NUMBER FOR		Cont	ANO		tockless.	Cwts.			CHA	IN (e) (h).			HAWS	ERS.	WAR	PS.
Sailing	Steam Trawlers	IRON AND STEEL STEAM TRAWLERS	No.	Sto	ock.	on	eamers	ex. Stock.	Length.	Dia-		Min	nimum	Weigh	ht.		Length.	Size	Length	Siza
Trawlers.	and Tugs.†	AND TUGS.†		1st Bower.	2nd Bower.	1st Bower.	2nd Bower.	Kedge.	Deng on.	meter	Stud Link.			Short Link.			Long on.	Diac.	Long th.	SIZO.
50 and 65	65 and 80	1980 and 2250	3	3	3	$3\frac{3}{4}$	$3\frac{3}{4}$	134	Fathms.	Ins. 12	Cwts. 17		lbs.	Cwts.	*~	lbs.	Fathms.	Ins. 5	Fathms.	Ins. 21
65 ,, 80	80 ,, 100	2250 ,. 2620	3	$3\frac{1}{2}$	$3\frac{1}{2}$	41/2	41/2	2	60	13		1	11	22	0	11	60	$5\frac{1}{2}$	60	3
80 ,, 100		2620 ,, 2950			4	5	5	$2\frac{1}{4}$	60	14		1	17	25	1	17	60	$5\frac{1}{2}$	60	3
$\frac{100}{120}$, $\frac{120}{140}$	11	2950 ,, 3230 3230 ,, 3510			4	$\frac{5\frac{1}{4}}{5\frac{1}{2}}$	5	$\frac{2\frac{1}{2}}{2\frac{1}{2}}$	60		$\frac{23}{33}$	3	$\frac{17}{11}$	$\frac{25}{36}$	$\frac{1}{1}$	11	60	$\frac{5\frac{1}{2}}{5\frac{1}{2}}$	60	$\frac{3\frac{1}{2}}{3\frac{1}{2}}$
		3510 , 3790			41/4	6	$5\frac{1}{4}$	$\frac{2^{2}}{2^{\frac{1}{2}}}$	90	$\frac{16}{15}$			13	43	2	13	60	$5\frac{1}{2}$	60	4
-		3790 ,, 4040			41/2	$6\frac{1}{4}$	$5\frac{1}{2}$	$2\frac{1}{2}$	90		45		17	49		0	60	$5\frac{1}{2}$	60	4
-	9 1 36	4040 ,, 4290	,		$\frac{4^{\frac{3}{4}}}{7}$	$6\frac{1}{2}$	6	$\frac{2\frac{1}{2}}{2}$	90		45		17	49	_	0	60	6	60	41
		4290 ,, 4530 4530 ,, 4770			$\frac{5}{5\frac{1}{4}}$	7 71	$\frac{6\frac{1}{4}}{6\frac{1}{9}}$	$\frac{2^{3}}{3}$		$1\frac{1}{16}$ $1\frac{1}{16}$	60		18	64 64	3	12 12	60	6	60	$\frac{4\frac{1}{2}}{5}$
_		4770 ,, 5010		6	$\frac{5_{\frac{1}{2}}}{5_{\frac{1}{2}}}$	71/2	7		120	$\overline{1_{16}^2}$	77		21	83	1	21	60	6	60	5
_		5010 ,, 5260		$6\frac{1}{4}$	$5\frac{3}{4}$	8	$7\frac{1}{4}$	- T	3	$1\frac{2}{16}$			21	83	1	21	60	6	60	5
		5260 ,, 5570			6	81	$7\frac{1}{2}$				77		21	83		21	60	6	60	5
-	-	5570 ,, 5900	3	$6\frac{3}{4}$	$6\frac{1}{4}$	$8\frac{1}{2}$	8	$3\frac{1}{2}$	120	$1\frac{3}{16}$	86	3	12	93	0	12	60	7	60	5

† The equipment for Tug Steamers of a larger size than the Trawlers provided for by the above Table shall be the same as for ordinary seagoing vessels.

The Anchors and Chains to be tested at a Public Testing Machine in accordance with the statutory tests.

 $\hfill \odot$ The tests of Anchors in this Table are approximate tests ; or as near as can be expressed in tons and aliquot part of tons.

(a) By Section 50 of the Rules for the Building and Classification of Steel Vessels, it is provided that the equipment is to be regulated by the number produced by the sum of the measurements in feet of the greatest moulded breadth of the vessel and the depth from the upper part of keel to the top of the upper deck beams at side at the middle of the length multiplied by the length of the vessel. In awning or shelter deck and part awning deck vessels the measurement of depth defined above is to be taken to the deck next below the awning or shelter deck, provided the height between the decks does not exceed 8 feet. If the 'tween deck height exceeds 8 feet the measurement is to be taken to a point 8 feet below the awning or shelter deck. In turret deck vessels to the normal beam line at base of turret. beam line at base of turret.

For a sailing vessel with a poop, bridge, top-gallant forecastle, or a raised quarter-deck, the equipment number is to be increased *one-fifteenth* beyond that which it would be if she were flush-decked.

For a steam vessel having erections on deck, the number obtained by the first clause of this paragraph is to be increased as follows:—

For a raised quarter deck, add the product of the height and length in feet of the erection.

For an awning or shelter deck, part awning deck, poop, bridge or forecastle add three-fourths the product of the height and length in feet of each erection, eight feet being taken as the maximum height for awning, or shelter deck, or part awning deck erections.

For deck houses or other erections not extending to the side, but exceeding either in length or breadth half the rule breadth of the vessel, add one-half the product of the height and length in feet of such erections.

Where erections are fitted upon erections, the equipment number is to be correspondingly increased.

To entitle vessels classed A "For Channel Purposes," to the Figure I, the equipment of Anchors and Chain Cables, etc., should be as required by Table 31, with the exception that not more than two Bower Anchors and one Stream Anchor need be supplied, the first Bower Anchor should be of the full weight required by the Table, and the second Bower may be 15 per cent. lighter. This rule, however, applies only to vessels intended for short passages. In vessels classed "For Channel Purposes," which are intended for longer voyages, such as the Queenboro' and Flushing, the Channel Islands or the Irish Sea service, the equipment must be in accordance with the requirements of Table 31.

(b) In order to meet the requirements of different trades, the weight of Anchors as given in the Table may be modified as under:

Where two Bower Anchors are required, one of them may be 7½ per cent. lighter than the weight set forth in the Table, provided the collective weight of the two Anchors is equal to that given in the Table, provided the collective weight of the three Bower Anchors are required, one of them may be 15 per cent., and another 7½ per cent. lighter than the weight set forth in the Table, provided the collective weight of the three Anchors is equal to that given in Table. Where it may be desired by the Owners the Bower Anchors may be of equal weight, provided the collective weight be not less than required by the Table.

For sailing vessels: in no case may the best Bower Anchor be lighter than prescribed in the Table, nor the third Bower be lighter than is allowed by this footnote.

All Anchor Stocks must be of acknowledged and approved description, and be one-fourth the weight of the Anchor given in the Table.

The heads of Stockless Anchors should not be less than three-fifths of the total weight of the Anchor.

weight of the Anchor.

(c) Stockless Stream and Kedge Anchors.—In the case of Stockless Stream and Kedge Anchors, an addition to the weight specified in this Table must be made of one-fourth to compensate for the deficiency in weight consequent on the absence of Stock.

(d) All Anchors, including Stream and Kedge Anchors exceeding lestbs, in weight, including Stock, to be tested according to the requirements of the Act of Parliament and the Certificates of Test produced.

(a) The Chain Cables and Stream Chains to be tested in all cases according to the

(e) The Chain Cables and Stream Chains to be tested in all cases according to the requirements of the Act of Parliament, and the Certificates of Test produced.

(1) There should be included in the weights, 2 End Shackles to each Cable; that is 4 for each outfit, which contains two Cables.

(g) There should be included in the weights, 2 End Shackles to each Stream Chain (h) Unstudded close-link Chains will be admitted as Cables, if proved two-thirds the Test required for Stud-link Chains for the tensile strain, and 100 per cent. above the tensile strain for the breaking strain.

(i) When steel wire Towlines or Hawsers are adopted, see notes (i) below.

. Where a departure from the requirements of this Table is proposed by an Owner the same should be submitted in the first place for the consideration of the

N.B.—The Italic letters preceding the Equipment Numbers correspond with letters printed in the seventh column in the List of Steam Vessels in the Register Book to indicate the Equipment Numbers of vessels per this Table.

(i) STEEL WIRE TOWLINES, HAWSERS AND WARPS.

(i) When steel wire towlines, hawsers, or warps are adopted, a short length of each of the wires composing the towlines, &c., will be required, after being galvanized, to withstand a tensile stress equivalent to that set forth in Table 31, and the aggregate strength of the wires must not be less than 10 per cent. in excess of that stress.

Each wire will be required to be capable of being twisted around itself not less than eight times, and of being untwisted and straightened without breaking.

Each manufacturer to be required to provide on his premises machines suitable for satisfactorily making the foregoing tests, and the works to be at all times open to the inspection of the Society's Surveyors, who are to be empowered to retest any hawser or towline for which a certificate has been issued by the manufacturer.

Printed Forms of Certificates, approved by the Committee, to be given by the Manufacturers of Steel Wire Hawsers, will be supplied to them upon application to the Secretary.

SPECIAL FLEXIBLE STEEL WIRE ROPE.

When an Owner prefers to substitute special flexible steel wire ropes for steel wire rope of ordinary make, the sizes may be reduced in accordance with the following Table, provided each flexible rope be formed of six strands with 24 wires in each strand, and that the diameter of each wire is 5th of the circumference of the rope, and the ropes are capable of withstanding the breaking tests shown in the Table:—

WIRE	LE STEEL ROPE. reaking Test.	CORRE- SPONDING SIZES RE- QUIRED BY TABLE 31.	FLEXI WII Size. I	CORRESPONDING SIZES REQUIRED BY TABLE 31.	
Inches.	Tons.	Inches.	Inches.	Tons.	Inches.
13/4	8.9	2	31/2	35.5	41/4
2	11.7	21/4	3 3 4	41.0	4½
21/2	18.2	23/4	44	52.5	434
$2\frac{1}{2}$	18.2	3	4 1/2	59.0	5
$2\frac{3}{4}$	22.0	31/4	$4\frac{3}{4}$	65.5	$5\frac{1}{4}$
3	26.2	31/2	5	73.0	51/2
31/4	30.7	334	$5\frac{1}{2}$	88.0	6
312	35.2	4	$6\frac{1}{4}$	114.0	7

RENEWAL OF CHAIN CABLES WHEN WORN.

When any length of a Chain Cable is worn so that the mean diameter at its most worn part is reduced to the size given in the following Table it is to be renewed.

Size of Chain Cable originally.	Should be renewed when worn to	Size of Chain Cable originally.	Should be renewed when worn to	Size of Chain Cable originally.	Should be renewed when worn to	Size of Chain Cable originally.	Should be renewed when worn to
Diameter in inches.	Mean diameter in inches.	Diameter in inches.	Mean diameter in inches.	Diameter in inches.	Mean diameter in inches.	Diameter in inches.	Mean diameter in inches.
11	2 O 3 2	$1\frac{4}{16}$	$1\frac{2}{16}$	$1\frac{1}{16}$	$1\frac{10}{16}$	$2\frac{6}{16}$	$2\frac{2}{16}$
$\frac{12}{16}$	$\frac{2}{3}\frac{1}{2}$	1 5 1 6	$1\frac{3}{16}$	$1\frac{14}{16}$	1116	276	$2\frac{3}{16}$
13	$\frac{2}{3}\frac{3}{2}$	$1\frac{6}{16}$	$1\frac{7}{32}$	$1\frac{15}{16}$	$1\frac{2}{3}\frac{3}{2}$	$2\frac{8}{16}$	$2\frac{4}{16}$
$\frac{14}{16}$	$\frac{25}{32}$	$1\frac{7}{16}$	$1\frac{9}{32}$	2	$1\frac{25}{32}$	$2\frac{9}{16}$	$2\frac{9}{32}$
15 16	$\frac{27}{32}$	1 8 1 6	$1\frac{1}{3}\frac{1}{2}$	$2\frac{1}{16}$	$1\frac{27}{32}$	210	$2\frac{1}{3}\frac{1}{2}$
1	$\frac{29}{32}$	$1\frac{9}{16}$	$1\frac{1}{3}\frac{3}{2}$	$2\frac{2}{16}$	$1\frac{2}{3}\frac{9}{2}$	$2\frac{1}{16}$	$2\frac{13}{32}$
$1\frac{1}{16}$	15 16	110	$1\frac{15}{32}$	$2\frac{3}{16}$	$1\frac{3}{3}\frac{1}{2}$	$2\frac{12}{6}$	$2\frac{1}{3}\frac{5}{2}$
1,2	1	111	18/16	$2\frac{4}{16}$	2	$2\frac{1}{16}$	$2\frac{17}{32}$
$1\frac{3}{16}$	$1\frac{1}{16}$	$1\frac{12}{16}$	1 9 16	$2\frac{5}{16}$	$2\frac{1}{16}$	$2\frac{14}{16}$	$2\frac{9}{16}$

Extract from the Rules for Wood and Composite Vessels, Section 32.

Tonnage for Regulating the Scantlings and Equipment (as regards Anchors, Chains, &c.).

In flush-decked vessels having either one, two or three decks (not being spar or awning-decked), the tonnage under the upper deck, without abatement of the tonnage of the space for the crew, or for the propelling power of steam vessels, is to regulate all the scantlings of the hull, and also the equipment of the vessel, as regards anchors, chains, warps, &c.

† In vessels having a raised quarter deck, or a poop, or top-gallant forecastle, or deck houses, or awning-deck, or spar deck, the total tonnage below the tonnage deck is to regulate the scantlings of the hull, but the register tonnage, as cut on the main beam of sailing vessels and of steam vessels, with the addition of the tonnage of the space required for propelling power, is to regulate the equipment.

But in vessels where the tonnage of the erections above the tonnage deck is less than that allowed for crew space, then the difference between the tonnage of these erections and the tonnage of the space allowed for crew is to be added to the register tonnage, cut on the main beam, for the tonnage that is to regulate the equipment.

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CAST STEEL ANCHORS.

All Cast Steel Anchors intended for vessels classed or proposed to be classed in the Society's Register Book must, in addition to undergoing the statutory tests, be subjected to the percussive, hammering, and bending tests recommended in the report of the Committee appointed by the Board of Trade to consider the question of tests of Cast Steel Anchors.

These tests, which are hereunder set forth, must be carefully and completely made in the presence and to the satisfaction of officers appointed by the Committee, viz.:—

PERCUSSIVE TEST.

1. Anchors, or when anchors are made of more than one piece, each piece shall be subject to this test, as follows:—

The anchor or piece shall be given weight. GIVEN HEIGHT. raised the given height for the given weight and shall be dropped on an

15 cwt. and below - 15 feet. iron slab.
Above 15 cwt. - 12 feet. The

The given height means that the lowest part of the anchor or piece

when suspended shall be at least the given height above the iron slab to which it is to be dropped.

2. An anchor of the Admiralty pattern shall first be raised vertically to the given height with its shanks and arms in a horizontal position, and shall be let fall from that height.

3. It shall then be raised a second time to the given height, and shall be suspended with the crown downwards. Two iron blocks shall be placed underneath it, and it shall be let fall from this position so that one of the blocks receives it on the middle of one arm, and the other block receives it on the middle of the other arm.

4. The slab for the horizontal test shall be of steel or iron, well laid on a solid concrete foundation to the satisfaction of the inspector.

5. If the slab on which the anchor falls is broken, the test shall be repeated until a slab is made that does not break.

6. The blocks for the vertical test shall be solid, and shall be of sufficient height to prevent the crown of the anchor from touching the slab, and shall be otherwise to the satisfaction of the inspector.

HAMMERING TEST.

7. When the percussive test has been passed successfully, to the satisfaction of the inspector, the anchor or piece shall be slung and freely

put to a hammering test as follows, that is to say, it shall be well hammered over its parts with a sledge hammer weighing not less than 7 lbs., and shall be required to give under this treatment such a clear ring in all its parts as shall satisfy the inspector that the casting is sound, and without flaws existing, either originally or developed as the result of the application of the preceding percussive tests.

BENDING TEST.

8. Cast steel may be passed as sufficiently ductile for anchors when a piece of each casting, 8 inches in length, is cut from the casting, turned to 1 inch in diameter, and is then bent cold by hammering through an angle of 90 degrees over a radius of $1\frac{1}{2}$ inches, without showing signs of flaw or fracture.

9. There must be a piece cast on each cast steel anchor, or on each portion of such anchor when it is made of more than one casting, and such piece must be of sufficient size to enable one test piece of the size before stated to be cut out of it, or it may be (at the discretion of the manufacturer) of sufficient size to enable four test pieces to be cut out of it. If it is only of sufficient size to enable one test piece to be cut out of it, that piece shall be subjected to the bending test named in paragraph 8, and, if it fails to withstand it, the casting is to be condemned.

If the piece is large enough to enable four test pieces to be cut out of it, these four test pieces shall be disposed of as follows, that is to say, one of them shall be turned in a lather to 1 inch in diameter for a length of 8 inches, and bent cold through an angle of 90 degrees over a radius of $1\frac{1}{2}$ inches, and if it withstands this test without flaw or fracture, shall be deemed to have withstood a satisfactory test for ductility. If the one test piece does not pass this test, all or any of the other three test pieces may be tested in a similar manner, and if any one of the four test pieces passes this test, the anchor or part of the anchor, as the case may be, shall be deemed so far satisfactory.

ANNEALING.

10. Each anchor must be properly and sufficiently annealed, and when so annealed, shall be stamped "annealed steel." Annealing is not to be regarded as proper, or efficient, unless the process extends from three days for small anchors, up to six days for large ones.

PROVING ESTABLISHMENTS.

The following Proving Establishments are recognised by the Committee of Lloyd's Register for the Testing of Anchors and Chains while licensed by the Board of Trade for that purpose:—

NETHERTON—Lloyd's Proving House	.Superintendent,	Mr. H. Green.
TIPTON—Lloyd's Proving House	. ditto	Mr. C. E. Perrins.
Low Walker—Lloyd's Proving House	. ditto	Mr. A. Green.
Chester (Saltney)—Lloyd's Proving House	. ditto	Mr. H. T. Welford.
GLASGOW—Lloyd's Proving House	. ditto	Mr. E. Seedhouse.
Cardiff—Lloyd's Proving House	. ditto	Mr. G. W. Penn.
SUNDERLAND—Lloyd's Proving House	. ditto	Mr. A. Green.
CRADLEY HEATH—Lloyd's Proving House	. ditto	Mr. S. C. Paul.

N.B.—Vessels supplied with Anchors and Chain Cables tested at any of the Proving Establishments in the above list, will have the notation of "Lloyd's A. & C.P." in the Register Book, signifying that the Anchors and Chain Cables have been tested at a machine under the control of the Committee of Lloyd's Register of Shipping.

The following Machines have been recognised by the Committee for the testing of Anchors and Chain Cables supplied to foreign owned vessels (see Section 50 of the Rules):—

AUSTRIA Government Establishment at Pola. SWEDEN Government Establishment at Kong niska Högskolan, Stockholm. """ Aktiengesellschaft Stahlwerke Weissenfels UNITED STATES American Steel Casting Co., Ches	
	ter. Pa.
	ter. Pa.
", Aktiengesellschaft Stahlwerke Weissenfels (for the testing of Small Chains only). UNITED STATES American Steel Casting Co., Ches (for the testing of Anchors only)	
BELGIUM The Antwerp Engineering Co., Société Anonyme, Rue des Indes, Antwerp. ,, Baldt Anchor Co., Chester, Pa. testing of Anchors only).	
Société Anonyme de Clouteries Mécaniques, Fontaine l'Evêque (for the testing of Bradlee & Co.'s Works, Philadelphi	
Small Chains only). ,, Cape Ann Anchor Works, Glouceste	r, Mass.
" Société Anonyme des Fabriques de Chaînes & " " J. B. Carr Co., Troy, N.Y.	
Pièces de Forge de Heppignies, près ,, Columbus Chain Co., Columbus, Oh	
" Société Anonyme des Usines Wattelar- adelphia, Pa.	
DENMARK Government Establishment at Copenhagen.)hio.
,, ,, Johes & Laughin Steel Co., Pittsb	urg, Pa.
France E. Turbot, Anzin (Nord). ,, Lebanon Chain Works, Lebanon, P	a.
,,	urnham,
" Dorémieux, Fils et Cie., St. Amand (Nord). " " J. McKay & Co.'s Iron City Chain McKees Rocks, near Pittsburg, P	
" Marrel Frères, Capelette, Marseilles. " Monongahela Iron and Steel Co., Pi	
,, M. Hemet, Havre.	
,, Mathieu Vivin & Louis Pierens, St. Amand- les-Eaux (Nord). ,, The Seaboard Steel Castings Co., Pa. (for the testing of Anchors of	
GERMANY A. Borsig, Berg und Huttenverwaltung Borsigwerk, Borsigwerk, Oberschlesien. , , Seneca Chain Co., Kent, Ohio. The Standard Chain Co. Columbus	
Duishunger Magahinanhan Alrian Coroll ", ", The Standard Chain Co., Columbus	
schaft (vormals Bechem & Keetmann). " " weither chain & from Co., Lebanor	
Duisburg. ,, ,, West End Rolling Mills, Lebanon,	
Holland Koninklijke Nederlandsche Grofsmederij, , , Whitehill Chain Works, Whitehill, boro, N.J.	Fields-
" Nederlandsche Ketting Fabriek, Schiedam. , " Woodhouse Chain Works, Trenton,	N.J.

By order of the Committee,

*

WEB FRAMES and STRINGERS.

TABLE 32.

(See continuation.)

-	-						MANAGE OF MANAGE OF THE PARTY.		-	-	-			1000	Julitinua	
		DEPTH	(d) AT M	IDDLE OF	LENGTH	FROM TO	OP OF ORI	DINARY I	FLOORS AT	CENTRE	TO TOP	OF BEAMS	S AT SID	E OF TAN	K DECK.	
TRANS-	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.	feet.
VERSE	11 and	12 and	13 and	14 and	15 and	16 and	17 and	18 and	19 and	20 and	21 and	22 and	23 and	24 and	25 and	26 and
NUMBER.	under 12	under 13	under 14	under 15	under 16	under 17	under 18	under 19	under 20	under 21	under 22	under 23	under 24	under 25	under 26	under 27
B+D.		10														
	<		TWO	SIDE STRI	NGERS		>	<	THREE	SIDE STI	RINGERS	>	<f< td=""><td>OUR SIDE</td><td>STRINGE</td><td>RS></td></f<>	OUR SIDE	STRINGE	RS>
feet.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.	inches.
45 and 48	12 × ·2	$6 \mid 13 \times \cdot 26 \mid$	$13 \times \cdot 28$	13 × ·30	14 × ·30	14 × ·32	$14 \times \cdot 34$									
48 and solution an	13 × ·2	3 13 × ⋅28	13 × ·30	14 × ·30	14 × ·32	14 × ·34	14 × ·36	15 × ·36	3							
$51_{ m under}^{ m and} 54$	13 × ·28	8 13 × ·30	14 × ·30	14 × ·32	14 × ·34	14 × ·36	15 × ⋅36	16 × ·36	$316 \times \cdot 38$							
$54_{ m under}^{ m and} 57$	13 × ·30	14 × ·30	14 × ·32	14 × ·34	14 × ·36	15 × ·36	16 × ·36	16 × ·38	17 × ⋅38	18 × ·38	-					
57 and 60 under 60	14 × ·30	14 × ·32	14 × ·34	14 × ·36	15 × ·36	16 × ·36	16 × ⋅38	17 × ⋅38	18 × ·38	18 × ·40	19 × ·40	20 × ·42				
60 and 63	14 × ·35	214 × ·34	14 × ·36	15 × ·36	16 × ·36	16 × ·38	17 × ·38	18 × ⋅38	18 × ·40	19 × ·40	20 × ·40	$21 \times \cdot 42$	22 × ·44	24 × ·44		
33 and under 66	14 × ·34	114 × ⋅36	15 × ·36	16 × ·36	16 × ·38	17 × ⋅38	18 × ·38	18 × ·40	19 × ·40	20 × ·40	$21 \times \cdot 40$	$22 \times \cdot 42$	$23 \times \cdot 44$	$24 \times \cdot 46$	$26 \times \cdot 46$	$27 \times \cdot 48$
36 and under 69		15 × ·36	16 × ·36	16 × ·38	17 × ·38	18 × ⋅38	$18 \times \cdot 40$	19 × ·40	20 × ·40	20 × ·42	21 × ·42	$22 \times \cdot 44$	$24 \times \cdot 44$	$25 \times \cdot 46$	26 × ·48	28 × ·48
39 under 72			16 × ·38	$17 \times \cdot 38$	18 × ⋅38	$18 \times \cdot 40$	$19 \times \cdot 40$	20 × ·40	20 × ·42	21 × ·42	22 × ·42	$23 \times \cdot 44$	$24 \times \cdot 46$	$26 \times \cdot 46$	$27 \times \cdot 48$	28 × ·50
72 and 75				18 × ⋅38	18 × ·40	19 × ·40	20 × ·40	$20 \times \cdot 42$	$21 \times \cdot 42$	$22 \times \cdot 42$	$23 \times \cdot 425$	$24 \times \cdot 44$	$25 \times \cdot 46$	$26 \times \cdot 48$	28 × ·48	29 × ·50
75 and 78 under 78					19 × ·40	20 × ·40	20 × ·42	$21 \times \cdot 42$	22 × ·42	22 × ·44	$23 \times \cdot 44$	24 × ·46	26 × ·46	27 × ·48	28 × ·50	30 × ·50
78 and 81						$20 \times \cdot 42$	$21 \times \cdot 42$	$22 \times \cdot 42$	22 × ·44	23 × ·44	24 × ·44 2	$25 \times \cdot 46$	$26 \times \cdot 48$	28 × ·48	29 × · 50	30 × ·52
31 and under 84							22 × ·42	22 × ·44	23 × ·44	24 × ·44	$25 \times \cdot 44$	26 × ·46	$27 \times \cdot 48$	28 × ·50	30 × · 50	31 × ·52
34 and 87							2	23 × ·44	24 × ·44	24 × ·46	$25 \times \cdot 46$	26 × ·48	28 × ·48	29 × ·50	30 × ·52	32 × ·52
37 and under 90									$24 \times \cdot 46$	25 × ·46	$26 \times \cdot 46$	$27 \times \cdot 48$	28 × ·50	30 × ·50	31 × ·52	$32 \times \cdot 54$
90 and 93									2	26 × ·48	$27 \times \cdot 48$	28 × ·50	30 × ·50	31 × ·52	32 × ·54	34 × ·54
93 and 96											29 × ·48 3	80 × ·50	$31 \times \cdot 52$	$32 \times \cdot 54$	$34 \times \cdot 543$	55 × ·56
96 and under 99											3	81 × ·52	32 × ·54	34 × ·54	$35 \times .563$	6 × ·58

The stringers are to be of the same dimensions as the web frames and are to be attached to the outside plating by double angles for a length of three frame spaces on each side of the bulkheads.

The web frames are to be spaced not more than four frame spaces apart.

The web frames are to be attached to the outside plating by double angles where their depth is 24 inches or above.

INTERMEDIATE FRAMES, FACE ANGLES, &c.

TABLE 32.

(Concluded.)

		INT	TERMEDIATE FRA	MES.	ANGLES ATTACHING WEB FRAMES.		BUT	T STRA	APS FOI	R STRIN	NGER	WEB 'TWI	FRAMEEN DE	ES IN
TRANS-	FRAME				SIDE STRINGERS AND KEELSONS TO OUTSIDE PLAT-	D	imensio	ns.	Rivets.		Depth.			
VERSE NUMBER. B+D.	SPACING	Built	Framing.	Bulb Angles.	ING; DOUBLE FACE ANGLES TO WEB FRAMES AND STRINGERS; AND	ANGLES TO WEB FRAMES AND SIDE STRINGERS.	Length.	Breadth,	Thickness,	Number in Straps and Strin- ger Face	Number in Straps and Web Frame Face	At Heel.	At Head.	Thick ness.
		Frames*	Reversed Frames.							Angles.				
$45_{ m under}^{ m feet.}48$	inches. $22\frac{1}{2}$	$3\frac{1}{2} \times 3 \times 30$	$2\frac{1}{2} \times 2\frac{1}{2} \times 30$	inches.	$3 \times 3 \times 308$	$5 \times 3 \times 48$	inches.	inches.	inches.	16	4	inches.	inches.	inches
$48_{ m under}^{ m and} 51$	$22\frac{1}{2}$	$3\frac{1}{2} \times 3 \times 30$	$3 \times 2\frac{1}{2} \times 30$		$3 \times 3 \times 30$	5 ×3 ×·48	22	22	27	27	22			
$51_{ m under}^{ m and} 54$	23	$3\frac{1}{2} \times 3 \times 30$	3 ×3 ×·30		$3 \times 3 \times 325$	$5 \times 3 \times 50$	22	22	"	27	27			
$54_{ m under}^{ m and}57$	23	4 ×3 ×·30	$3 \times 3 \times 30$		$3 \times 3 \times 345$	$5 \times 3 \times 52$	22	27	.48	27	22	15	15	.34
$57_{ m under}^{ m and}60$	$23\frac{1}{2}$	$4\frac{1}{2} \times 3 \times 30$	$3 \times 3 \times 30$	$5\frac{1}{2} \times 3 \times 36$	$3 \times 3 \times 36$	$5 \times 3\frac{1}{2} \times 52$	42	11	"	20	6	15	15	.34
$60_{\mathrm{under}}^{\mathrm{and}}63$	$23\frac{1}{2}$	$4\frac{1}{2} \times 3 \times 32$	$3 \times 3 \times 32$	$5\frac{1}{2} \times 3 \times 38$	$3\frac{1}{2} \times 3 \times 36$	$5 \times 3\frac{1}{2} \times 54$	27	22	.50	27	22	15	15	.36
$63_{\mathrm{under}}^{\mathrm{and}}66$	24	$5 \times 3 \times 32$	$3 \times 3 \times 32$	6 ×3 ×·38	$3\frac{1}{2} \times 3 \times 386$	$3 \times 3\frac{1}{2} \times 54$	"	22	27	27	27	18	15	.36
$66_{\mathrm{under}}^{\mathrm{and}}69$	24	$5 \times 3 \times 34$	$3 \times 3 \times 34$	$6 \times 3 \times 40$	$3\frac{1}{2} \times 3 \times 406$	$3 \times 3\frac{1}{2} \times 56$	27	22	.52	27	27	21	18	.38
$69_{\mathrm{under}}^{\mathrm{\ and\ }}72$	$24\frac{1}{2}$	$5\frac{1}{2} \times 3\frac{1}{2} \times 34$	$3 \times 3 \times 34$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$3\frac{1}{2} \times 3\frac{1}{2} \times 40$	$3\frac{1}{2} \times 3\frac{1}{2} \times 58$	45	12	27	27	22	24	18	.38
$72_{ m under}^{ m and}75$	$24\frac{1}{2}$	$5\frac{1}{2} \times 3\frac{1}{2} \times 34$	$3\frac{1}{2} \times 3 \times 34$	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	$3\frac{1}{2} \times 3\frac{1}{2} \times 60$	27	22	.54	27	27	27	21	.38
$75_{\mathrm{under}}^{\mathrm{and}}78$	25	$5\frac{1}{2} \times 3\frac{1}{2} \times 36$	$3\frac{1}{2} \times 3 \times 36$	$6\frac{1}{2} \times 3\frac{1}{2} \times 42$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$7 \times 3\frac{1}{2} \times 60$	22	"	27	22	22	30	21	•40
$78_{\mathrm{under}}^{\mathrm{and}}81$	25	$6 \times 3\frac{1}{2} \times 36$	$3\frac{1}{2} \times 3 \times 36$	$7 \times 3\frac{1}{2} \times 42$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	$7 \times 3\frac{1}{2} \times \cdot 62$	27	22	.56	22	22	30	21	•40
$81_{\mathrm{under}}^{\mathrm{and}}84$	$25\frac{1}{2}$	$6 \times 3\frac{1}{2} \times 38$	$3\frac{1}{2} \times 3 \times 38$	$7 \times 3\frac{1}{2} \times 44$	$3\frac{1}{2} \times 3\frac{1}{2} \times 48$	$7 \times 3\frac{1}{2} \times \cdot 64$	27	22	27	27	27	33	21	.42
$84_{ m under}^{ m and}87$	$25\frac{1}{2}$	$6\frac{1}{2} \times 3\frac{1}{2} \times 38$	$3\frac{1}{2} \times 3 \times 38$	$7\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	$3\frac{1}{2} \times 3\frac{1}{2} \times 50$	$7 \times 3\frac{1}{2} \times 66$	27	27	.58	22	27	33	21	.42
$87_{\mathrm{under}}^{\mathrm{and}}90$	26	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$3\frac{1}{2} \times 3 \times 40$	$7\frac{1}{2} \times 3\frac{1}{2} \times 46$	$3\frac{1}{2} \times 3\frac{1}{2} \times 52$	$7 \times 3\frac{1}{2} \times 68$	27	27	27	"	22	36	24	•44
$90_{\mathrm{under}}^{\mathrm{and}}93$	26	$7 \times 3\frac{1}{2} \times \cdot 40$	$3\frac{1}{2} \times 3 \times 40$	$8 \times 3\frac{1}{2} \times 46$	$4 \times 3\frac{1}{2} \times 52$	$7 \times 3\frac{1}{2} \times \cdot 72$	27	"	.60	"	27	36	24	•44
$93_{\mathrm{under}}^{\mathrm{and}}96$	$26\frac{1}{2}$	$7 \times 3\frac{1}{2} \times \cdot 42$	$3\frac{1}{2} \times 3 \times 42$	$8 \times 3\frac{1}{2} \times 48$	$4 \times 3\frac{1}{2} \times 547$	$7 \times 3\frac{1}{2} \times 76$	"	"	22	22	27	39	24	.46
$96_{\mathrm{under}}^{\mathrm{and}}99$	$26\frac{1}{2}$	$7 \times 3\frac{1}{2} \times 42$	$3\frac{1}{2} \times 3\frac{1}{2} \times 42$	$8\frac{1}{2} \times 3\frac{1}{2} \times 48$	$4 \times 3\frac{1}{2} \times 567$	$7 \times 3\frac{1}{2} \times \cdot 80$	27	22	.62	22	22	39	24	.46

*The frames in the 'tween decks, may be of angles '06 of an inch thicker than required by the Table, in which case the reversed frames may be dispensed with.

†The reversed frame at upper edge of floor plates to be of the dimensions required for double face angles on webs.

FLOOR PLATES.

TABLE 33.

TRANSVERSE		THICKNESS. *			TRANSVERSE		THICKNESS. *	
NUMBER. B + D	ER. DEPTH AT FOR NUMBER.			DEPTH AT CENTRE.	For $\frac{3}{5}$ length Amidships.	At Ends.		
feet. 45 and under 46	inches.	inches.	inches.		feet. 68 and under 70	inches.	inches.	inches.
46 and 47	18	·34	.30	6 8 3	70 and under 72	29	.46	.38
47 and under 48	18	.36	·32	8.1	72 and vander 74	30	.46	.38
48 and 49	19	.36	·32	- 81	74 and 176	30	•48	.38
49 and under 50	20	.36	32		76 and under 78	31	·48	.38
50 and under 51	20	.38	•34		78 and under 80	32	•48	.38
51 and under 52	21	.38	·34	6 8	80 and under 82	32	.50	•40
52 and under 53	22	.38	·34	8	82 and under 84	33	.50	•40
53 and under 54	22	•40	•34		84 and number 86	34	.50	•40
54 and 55	23	·40	•34		86 and under 88	35	.50	•40
55 and under 56	24	•40	·34		88 and under 90	35	.52	•40
56 and 58	24	•42	.36		90 and under 92	36	.52	•40
58 and dunder 60	25	•42	•36		92 and under 94	37	.52	•40
60 and under 62	26	•42	.36		94 and under 96	38	.52	•40
62 and under 64	26	•44	.36	1	96 and under 98	38	.54	•42
64 and under 66	27	•44	.36	18	98 and under 100	39	.54	.42
66 and 68	28	•44	.36		the to st ye	i dibibeasev		Colte

^{*} In the engine space of steam vessels the floors are to be '04 of an inch thicker, and in the boiler space '10 of an inch thicker than required by the Table.

FLAT KEEL ANGLES, and SIDE and BILGE KEELSONS. TABLE 34.

LONGITUDINAL	FLAT KEEL AND	HES.	SIDE AND BILGE KEELSONS.					
NUMBER.	For $\frac{1}{2}$ ength	Thickness	For $\frac{1}{2}$ length	Thickness	Intercostal Plates.	Angles on Vertical Plate.		
L × (B + D)	Amidships.	at Ends.	Amidships.	at Ends.		For $\frac{1}{2}$ length Amidships.	Thickness at Ends.	
	inches.	inches.	inches.	inches.	inches.	inches.	inches.	
7000 and under 7600	$3\frac{1}{2} \times 3\frac{1}{2} \times .38$.38	Double Angles, $3\frac{1}{2} \times 3 \times 34$.34	.32			
7600 and 8200	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$.38	$4 \times 3 \times 34$	•34	.32			
8200 and under 8800	$4 \times 4 \times \cdot 40$.38	$4 \times 3 \times 34$.34	.32	x 8 x 10 00 00.	198- 11	
8800 and 9400	$4 \times 4 \times \cdot 40$.38	$4 \times 3 \times 36$	•34	•34	I was to the trans		
9400 and 10000	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 40$.38	$4 \times 3 \times 36$	·34	-34			
10000 and 10600	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 40$.38	$4\frac{1}{2} \times 3 \times 36$.34	·34			
10600 and 11800	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 42$	•40	$4\frac{1}{2} \times 3\frac{1}{2} \times .36$.34	.36			
11800 and under 12400	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 42$	•40	$5 \times 3\frac{1}{2} \times 36$.34	.36			
12400 and under 13000	$\frac{1}{4\frac{1}{2}} \times 4\frac{1}{2} \times \cdot 42$	•40	$5 \times 3\frac{1}{2} \times \cdot 38$.36	.38			
13000 and 14200	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 44$	•42	$5 \times 3\frac{1}{2} \times \cdot 40$.36	.38			
14200 and 15400	$\frac{1}{4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 44}$	•42	$5\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$.36	.38	X II X graft day to make	100	
15400 and 16000	$\frac{1}{4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 46}$	•44	$5\frac{1}{2} \times 3\frac{1}{2} \times {}^{\cdot}42$.36	.38	NE A TOUR THE	7 8 4 1	
16000 and 16600	$\frac{1}{4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 46}$	•44	$6 \times 3\frac{1}{2} \times \cdot 42$	•36	•40			
16600 and 17200	$5 \times 5 \times \cdot 46$	•44	$6 \times 3\frac{1}{2} \times \cdot 42$.36	•40			
17200 and 18000	5 ×5 × ·48	•46	Double Bulb Angles. $7 \times 3\frac{1}{2} \times 42$	•40	•40	x 2 X 4 7 100 80	14- 21	
18000 and 19000	$5 \times 5 \times .50$	•46	$8 \times 3\frac{1}{2} \times \cdot 46$	•44	•40			
19000 and 20000	$5 \times 5 \times .50$	•46	$9 \times 3\frac{1}{2} \times .50$	•46	•40			
20000 and under 21000	$5 \times 5 \times .52$	•48	$10 \times 3\frac{1}{2} \times .54$	•48	•40	× 4 × 4 × 4 × 4		
21000 and under 22000	$5 \times 5 \times .54$.50	Vertical Plate, 11 × ·50	and Four	Angles.	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$.38	
22000 and under 24000	$5 \times 5 \times 54$.50	$12 \times .52$	•42	•42	$\frac{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46}{6 \times 3 \times 3 \times 3}$.38	
24000 and under 26000	$5 \times 5 \times .56$.52	$13 \times .54$	•44	•42	$6\frac{1}{2} \times 3\frac{1}{2} \times .46$.38	
26000 and under 28000	$5 \times 5 \times .56$.52	$14 \times .56$	•46	•42	$\frac{6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48}{6 \times 3 \times 3 \times 3}$.38	
28000 and under 30000	$5 \times 5 \times .58$	•54	15 × ·58	•48	•42	$6\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$.38	
30000 and under 32000	$5 \times 5 \times .58$.54	16 × ·60	.50	•42	$6\frac{1}{2} \times 3\frac{1}{2} \times .50$	•40	
32000 and under 34000	$5 \times 5 \times 60$.54	17 × ·62	.52	•42	$6\frac{1}{2} \times 3\frac{1}{2} \times .50$	· ·40	
34000 and 36000	$5 \times 5 \times .60$.54	18 × ·64	.54	•44	$7 \times 3\frac{1}{2} \times .50$.40	
36000 and under 39000	$5 \times 5 \times .60$	•54	19 × ·66	.56	•44	$7 \times 3\frac{1}{2} \times .50$	•40	
39000 and 42000	$6 \times 6 \times .60$	•54	20 × ·68	.58	•44	$7 \times 3\frac{1}{2} \times .50$	•40	
42000 and under 46000	$6 \times 6 \times .60$	•54	$21 \times .70$.60	•44	$7 \times 3\frac{1}{2} \times .50$	•40	
46000 and 50000	$6 \times 6 \times .60$	•54	22 × ·72	.62	•44	$7 \times 3\frac{1}{2} \times .50$	•40	

Where the breadth of the vessel is under 50 feet, two keelsons of the dimensions required by the Table are to be fitted on each side. Where the breadth is 50 feet and under 64 feet, three keelsons are to be fitted on each side, in which case the depth of the vertical plates may be one-fourth less than given in the Table.

The keelsons required by the above Table are, so far as is practicable, to extend throughout the oil compartments and machinery space.

BULKHEADS.

TABLE 35.

DEPTH FROM TOP OF FLOORS TO TOP OF BEAMS AT	THICKNESS OF BULKHEAD PLATING. Below Tank Deck. In		VERTICAL STIFFENING BARS. **		HORIZONTAL GIRDERS BELOW TANK DECK.					
CENTRE OF TANK DECK.*	At Floor.	At Tank Deck.	Expansion Trunk.	Bulb Angles below Tank Deck.	Angles in Expansion Trunk.	1st (at bottom).	2nd.	3rd.	4th.	HEADS. DEPTH AT HEEL.
feet. 12 and under 13	inches.	inches.		inches. $5\frac{1}{2} \times 3 \times \cdot 34$	inches. $5 \times 3 \times \cdot 30$	$\begin{array}{c} \text{inches.} \\ \text{Channel.} \\ 9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \end{array}$	$\begin{array}{c} \text{inches.} \\ \text{Channel.} \\ 9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \end{array}$	inches. Channel.	inches. Channel.	inches.
13 and under 14	•36	•32	•30	$5\frac{1}{2} \times 3 \times \cdot 36$	$5 \times 3 \times \cdot 32$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$9 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	x 4x 5 000		18
14 and under 15	•36	.32	•30	$5\frac{1}{2} \times 3 \times \cdot 38$	$5 \times 3 \times \cdot 32$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$			20
15 and under 16	•38	•34	•32	$6 \times 3 \times \cdot 38$	$5 \times 3 \times \cdot 34$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$10 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	2 14 x (2 + 1) ms	1000	22
16 and under 17	•38	•34	-32	$6 \times 3 \times \cdot 40$	$5 \times 3 \times \cdot 34$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	* [b x 484] 008		24
17 and under 18	•40	•34	.32	$6\frac{1}{2} \times 3 \times \cdot 40$	$5 \times 3 \times \cdot 36$	$15 \times 4 \times 4 \times \cdot 52$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$			26
18 and under 19	•40	•36	•34	$6\frac{1}{2} \times 3 \times \cdot 42$	$5 \times 3 \times \cdot 36$	$15 \times 4 \times 4 \times \cdot 52$	$15 \times 4 \times 4 \times \cdot 52$	×11-×11-1 00s	T 000001	28
19 and under 20	•42	.36	•34	$6\frac{1}{2} \times 3 \times \cdot 42$	$5 \times 3 \times \cdot 38$	$15 \times 4 \times 4 \times \cdot 52$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	11200	30
20 and under 21	•42	•36	•34	$7 \times 3 \times \cdot 42$	5 × 3 × · 38	$15 \times 4 \times 4 \times \cdot 52$	$15 \times 4 \times 4 \times \cdot 52$	$12 \times 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$		32
21 and under 22	•44	•38	.36	$7 \times 3 \times \cdot 44$	$5 \times 3 \times \cdot 40$	$15 \times 4 \times 4 \times \cdot 52$	$15 \times 4 \times 4 \times \cdot 52$	$15 \times 4 \times 4 \times \cdot 52$		34
22 and under 23	•44	•38	•36	$7\frac{1}{2} \times 3 \times \cdot 44$	5 × 3 × ·40	Plate. 20 × ·40	$15 \times 4 \times 4 \times \cdot 52$	$15 \times 4 \times 4 \times \cdot 52$	Figure 1	36
23 and under 24	•44	.38	•36	$7\frac{1}{2} \times 3 \times \cdot 46$	$5\frac{1}{2} \times 3 \times \cdot 40$	22 × ·40	Plate. 20 × •40	$15 \times 4 \times 4 \times \cdot 52$		38
24 and under 25	•46	•40	•38	$7\frac{1}{2} \times 3 \times \cdot 46$	$5\frac{1}{2} \times 3 \times \cdot 40$	22 × ·40	20 × ·40	$15 \times 4 \times 4 \times \cdot 52$	$15 \times 4 \times 4 \times \cdot 52$	40
25 and under 26	.46	•40	.38	8 × 3 × ·46	$5\frac{1}{2} \times 3 \times \cdot 40$	$24 \times \cdot 42$	22 × ·40	Plate. 20 × ·40	$15 \times 4 \times 4 \times \cdot 52$	Two frame spaces.
26 and under 27	•46	•40	•38	8 × 3 × ·48	$5\frac{1}{2} \times 3 \times \cdot 40$	26 × ·44	24 × ·44	22 × ·42	Plate. 20 × ·40	22
27 and under 28	.48	•42	•40	$8\frac{1}{2} \times 3 \times \cdot 48$	$5\frac{1}{2} \times 3 \times \cdot 40$	28 × ·46	26·× ·44	$24 \times \cdot 42$	21 × ·40	27
28 and under 29	.48	•42	•40	$8\frac{1}{2} \times 3 \times \cdot 50$	$5\frac{1}{2} \times 3 \times \cdot 40$	30 × ·46	27 × ·44	$25 \times \cdot 42$	22 × ·40	- 27
29 and under 30	.48	•42	•40	$8\frac{1}{2} \times 3 \times .52$	$5\frac{1}{2} \times 3 \times \cdot 40$	32 × ·48	29 × ·46	26 × ·42	23 × ·40	22
30 and under 31	.50	•44	•42	$9 \times 3 \times \cdot 52$	$5\frac{1}{2} \times 3 \times \cdot 40$	34 × ·48	30 × ·46	27 × ·44	24 × ·40	22
31 and under 32	•50	•44	•42	$9 \times 3 \times \cdot 54$	$5\frac{1}{2} \times 3 \times \cdot 40$	36 × ·50	32 × ·48	29 × ·44	25 × ·40	22
32 and under 33	•50	•44	•42	9 × 3 × · 56	$5\frac{1}{2} \times 3 \times \cdot 40$	38 × ·50	34 × ·48	30 × ⋅44	26 × ·40	22

^{*} The depth is to be measured at the middle of the length of the vessel except for the thickness of bottom part of bulkhead pl ing, vertical stiffeners and horizontal girders below tank deck in which cases the depth is to be measured at the bulkheads.

less than that of the floors at centre, and that at the head not less than two-thirds that at the heel.

^{**} The vertical stiffeners on the middle line bulkheads are to be spaced as required for the frames of the vessel and those on the transverse bulkheads are also to be spaced as required for the frames, but are in no case to be more than 24 inches apart centre to centre.

Web plates are to be fitted to the middle line bulkheads opposite the web frames at the side of the vessel. Their thickness is to be as required for the plating of the lower part of the bulkhead, and the depth at the heel is not to be

[†] Two web plates are to be fitted to the transverse bulkheads on each side of the middle line where the breadth is less than 50 feet, and three where the breadth is 50 feet and under 64 feet. The web plates are to be of the thickness required for the plating of the lower part of the bulkhead. Their depth at heel is to be as given in the Table, and the depth at head equal to one frame space, but need not exceed that required at the heel.

Where the horizontal girders on bulkheads are formed of plates they are to have a bulb angle face bar of the dimensions required for the vertical stiffeners.

EXPANSION TRUNKS and BULKHEAD BOUNDARY BARS.

TABLE 36.

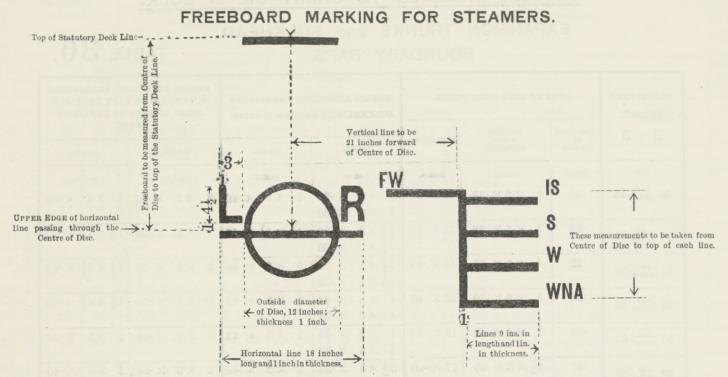
TRANSVERSE	SIDE	S OF EXPANSION T	RUNK.		ING TRANSVERSE	ANGLES ATTACHING TRANSVERSE BULKHEADS TO TANK DECK AND SIDES AND TOP OF EXPANSION TRUNK.			
B + D	Thickness of Plating.	Vertical Angle Stiffeners.	Web Plates.	Double,	Single.	Double.	Single.		
feet.	inches.	inches.	inches.	inches.	inches.	inches.	inches.		
45 and under 48	•30	$5 \times 3 \times \cdot 38$	12 × ·36	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 × 4 × ·40	3 × 3 × ·30	$4 \times 4 \times \cdot 40$		
48 and under 51	•32	5 × 3 × ·38	13 × ·38	$ \begin{array}{cccc} 3\frac{1}{2} \times 3 & \times \cdot 30 \\ 3\frac{1}{2} \times 3 & \times \cdot 30 \end{array} $	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 40$	3 × 3 × ·30	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 40$		
51 and under 54	•32	$5 \times 3 \times \cdot 40$	14 × ·40	$\begin{array}{cccc} 3\frac{1}{2} \times 3 & \times \cdot 32 \\ 3\frac{1}{2} \times 3 & \times \cdot 32 \end{array}$	5 × 5 × ·40	3 × 3 × ·32	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 40$		
54 and under 57	•34	5 × 3 × ·40	$\boxed{15 \times \cdot 40}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5 × 5 × ·42	3 × 3 × ·34	$4\frac{1}{2} \times 4\frac{1}{2} \times \cdot 40$		
57 and under 60	•34	$5 \times 3 \times \cdot 40$	16 × ·40	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 × 5 × ·42	3 × 3 × · 36	5 × 5 × ·40		
60 and under 63	•36	$5\frac{1}{2} \times 3 \times \cdot 40$	17 × ·40	$\begin{array}{cccc} 5\frac{1}{2} \times 3 & \times \cdot 36 \\ 3 & \times 3 & \times \cdot 36 \end{array}$	5 × 5 × ·44	3 × 3 × · 36	$5 \times 5 \times \cdot 40$		
63 and under 66	•36	$5\frac{1}{2} \times 3 \times \cdot 40$	18 × ·40	$\begin{array}{cccc} 5\frac{1}{2} \times 3 & \times \cdot 38 \\ 3 & \times 3 & \times \cdot 38 \end{array}$	$5 \times 5 \times \cdot 44$	3 ×3 × 38	$5 \times 5 \times \cdot 42$		
66 and 69	•38	$5\frac{1}{2} \times 3 \times \cdot 40$	18 × ·40	$5\frac{1}{2} \times 3 \times \cdot 40$ $3 \times 3 \times \cdot 40$	$5 \times 5 \times \cdot 46$	$3 \times 3 \times \cdot 40$	$5 \times 5 \times \cdot 42$		
69 and under 72	•38	$5\frac{1}{2} \times 3 \times \cdot 40$	19 × ·40	$ \begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 40 \\ 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40 \end{array} $	5 × 5 × ·48	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 40$	$5 \times 5 \times \cdot 44$		
72 and under 75	•40	6 × 3 × ·40	20 × ·40	$ \begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 42 \\ 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42 \end{array} $	$5 \times 5 \times 50$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 42$	5 × 5 × ·44		
75 and under 78	•40	6 × 3 × ·40	21 × ·40	$ \begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 44 \\ 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44 \end{array} $	5 × 5 × ·50	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 44$	5 × 5 × ·46		
78 and under 81	•40	6 × 3 × ·40	22 × ·40	$ \begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 46 \\ 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46 \end{array} $	6 × 6 × ·50	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 46$	5 × 5 × ·46		
81 and under 84	•42	$6\frac{1}{2} \times 3 \times \cdot 40$	23 × ·40	$ \begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 48 \\ 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48 \end{array} $	6 × 6 × ·50	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 48$	5 × 5 × ·48		
84 and under 87	•42	$6\frac{1}{2} \times 3 \times \cdot 40$	$24 \times \cdot 40$	$ \begin{array}{c} 6 \times 3\frac{1}{2} \times \cdot 50 \\ 3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50 \end{array} $	6 × 6 × ·50	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	5 × 5 × ·50		
87 and under 90	•42	$6\frac{1}{2} \times 3 \times \cdot 40$	24 × ·40		$6 \times 6 \times \cdot 52$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	6 × 6 × · 50		
90 and under 93	•44	$6\frac{1}{2} \times 3 \times \cdot 40$	$25 \times \cdot 40$		6 × 6 × ·52	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	6 × 6 × ·50		
93 and under 96	•44	$6\frac{1}{2} \times 3 \times \cdot 40$	25 × ·40		$6 \times 6 \times \cdot 54$	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	6 × 6 × ·50		
96 and 99	•44	$6\frac{1}{2} \times 3 \times \cdot 40$	26 × ·40		6 × 6 × · 56	$3\frac{1}{2} \times 3\frac{1}{2} \times \cdot 50$	$6 \times 6 \times \cdot 52$		

LLOYD'S REGISTER OF BRITISH AND FOREIGN SHIPPING, LONDON,-17th June, 1909.

ASSIGNMENT OF FREEBOARD.

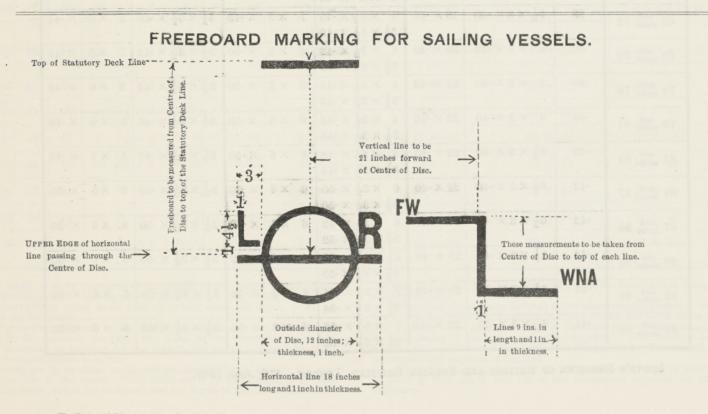
Under the Merchant Shipping Act, 1894, the Committee of Lloyd's Register are empowered to assign freeboards to British Vessels as required by the Act. Forms of application for the assignment of freeboard can be obtained from the London, or other, offices of the Society.

The mode of Marking, approved by the Board of Trade, is as follows:-



The Centre of Disc to be placed on both sides of vessel amidships, i.e., at the middle of the length of the load water line. Vessels are to be marked with such of the horizontal lines are as applicable to the nature of their employment. In accordance with the regulations made by the Board of Trade, the discs and lines must be permanently marked by centre punch marks or cutting, and the particulars given in the Certificate are to be entered in the official log.

N.B.—It is a condition on which an awning or shelter deck or partial awning deck vessel is classed in the Society's Register Book that the Freeboard assigned shall be marked on the vessel's sides as above prescribed; and, under the provisions of Section 44 of the Society's Rules for Steel Ships. If the vessel proceed to sea with a less freeboard than that approved by the Committee, or if the freeboard mark be placed higher than the position assigned by the Committee, the vessel will be liable to have her class expunged from the Register Book.



The Centre of Disc to be placed on both sides of vessel amidships, i.e., at the middle of the length of the load line. Coasting vessels are required to be marked with only the maximum load line in fresh water. In accordance with the regulations made by the Board of Trade, the disc and lines must be permanently marked by centre punch marks or outling and the particulars given in the Certificate are to be entered in the official log.



